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**COMPARATIVE PERFORMANCE OF HIGH  
EFFICIENCY SHIP PROPULSION SYSTEMS  
FOR DESTROYER HULL TYPES. VOLUME II.  
APPENDICES**

**Alan J. Stewart**

**Bradford Computer and Systems, Incorporated**

**Prepared for:**

**Office of Naval Research  
Advanced Research Projects Agency**

**6 December 1974**

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VOLUME II  
APPENDICES

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Alan J. Stewart

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# COMPARATIVE PERFORMANCE OF HIGH EFFICIENCY SHIP PROPULSION SYSTEMS FOR DESTROYER HULL TYPES

**VOLUME II**

## APPENDICES

By

Alan J. Stewart

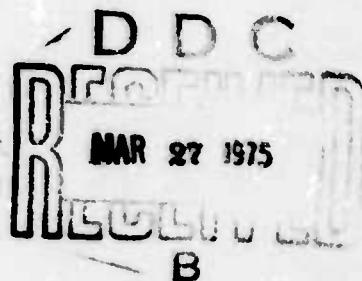
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## APPENDIX A - MATH MODELS

This appendix contains the math models used in computer simulation of the systems.

### A.1 TURBINE MATH MODELS

The gas turbines were modeled using the following expression for fuel rate: (1)

$$W_F = \frac{Q_T + W_1 + W_2 S_T}{W_3 - W_4 S_T} \quad (A1)$$

Where:  $W_F$  = Fuel Rate (lb/hr)

$Q_T$  = Turbine Torque (lb - ft)

$S_T$  = Turbine Speed (rpm)

$W_1$ ,  $W_2$ ,  $W_3$  and  $W_4$  are constants characterizing the turbine.

The following constraints were imposed:

$Q_T \leq Q_{MAX}$  Where  $Q_{MAX}$  = Max. allowable steady-state torque

$S_T \leq S_{MAX}$  Where  $S_{MAX}$  = Max. allowable steady-state rpm

$W_{MIN} \leq W_F \leq W_{MAX}$  Where  $W_{MIN}$  = Min. allowable (idle)/fuel rate

$W_{MAX}$  = Max. allowable fuel rate

The turbine power is:

$$P_T = 1.904 \times 10^{-4} S_T Q_T \quad (A2)$$

Where:  $P_T$  = Turbine shaft horsepower

---

(1) Expressions developed by NSRDC, Annapolis.

Specific Fuel Consumption is:

$$SFC = W_F / P_T \text{ (lb/hp - hr)} \quad (A3)$$

The maximum available turbine power occurs at  $W_F = W_{MAX}$  and a turbine speed,  $s_0$ ; at this point:

$$Q_0 = \frac{W_3 W_{MAX} - W_1}{2}$$

$$s_0 = \frac{W_3 W_{MAX} - W_1}{2 (W_4 W_F + W_2)} = \frac{Q_0}{W_4 W_F + W_2}$$

$$P_{MAX} = 1.904 \times 10^{-4} s_0 Q_0$$

$$SFC_{MIN} = W_{MAX} / P_{MAX}$$

In order to compare turbine performance at various operating points, a turbine figure-of-merit was defined as:

$$FOM = SFC_{MIN} / SFC \quad (A4)$$

For any given power,  $P_T$ , there will be an optimum Speed,  $s_{TO}$ , which minimizes the fuel rate (and SPC), given by:

$$s_{TO} = \sqrt{\left(\beta W_4 P_T\right)^2 + \beta W_3 P_T} - \beta W_4 P_T \quad (A5)$$

$$\text{Where } \beta = \frac{5252}{W_1 W_4 + W_2 W_3}$$

For a given fuel rate,  $W_F$ , the maximum power and associated speed and torque may be expressed by:

$$S_{T0} = \rho / 2\sigma$$

$$Q_{T0} = \rho / 2$$

$$P_{T0} = 1.904 \times 10^{-4} \rho^2 / 4\sigma$$

$$\text{Where: } \rho = W_3 W_F - W_1$$

$$\sigma = W_4 W_F + W_2$$

With the fuel rate fixed, power may then be expressed as a function of the speed:

$$\frac{P_T}{P_{T0}} = \left( 2 - \frac{S_T}{S_{T0}} \right) \left( \frac{S_T}{S_{T0}} \right); W_F \text{ constant.} \quad (\text{A6})$$

This behavior is shown in figure A1.

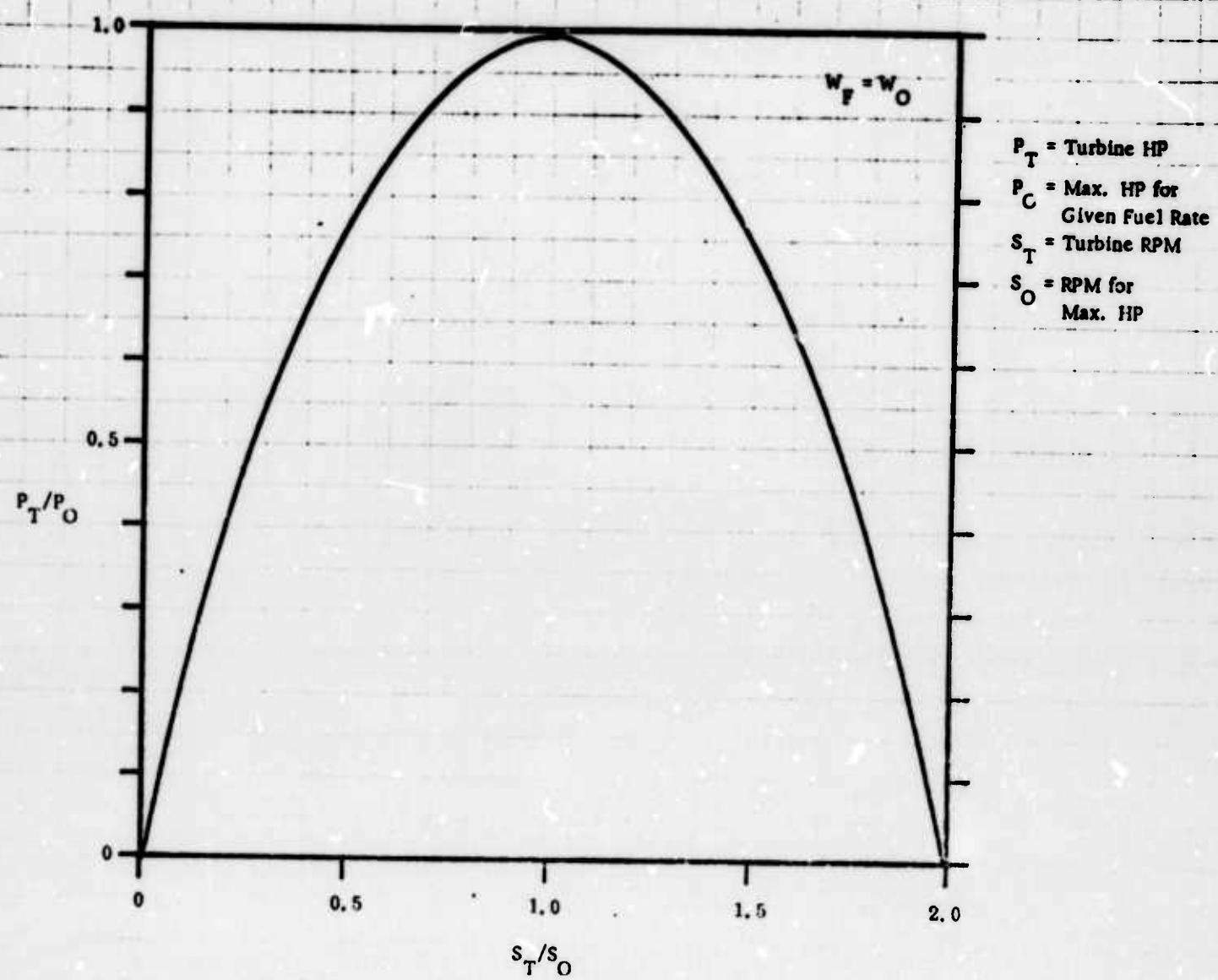


Figure A-1. Power vs. Speed for fixed Fuel Rate

### A.1.1 Main (LM - 2500) Turbine

Constants used for the LM - 2500 turbine were as follows<sup>(1)</sup>:

$$W_1 = 6600$$

$$W_3 = 9.143$$

$$W_2 = 1.05$$

$$W_4 = 1.143 \times 10^{-3}$$

$$W_{MIN} = 1100 \text{ lb/hr}$$

$$W_{MAX} = 8400 \text{ lb/hr}$$

$$Q_{MAX} = 60,000 \text{ lb-ft}$$

$$S_{MAX} = 3600 \text{ rpm}$$

These values result in optimum operating speeds vs. power and corresponding FOM and fuel rate values, as shown in figure A2. Maximum power is 22,024 hp at 3295 rpm, with an SFC of 0.3814 lb/hp-hr (FOM = 1.0).

A performance map showing power and SFC vs. shaft speed is shown in figure A3. The effect on fuel consumption of operating the turbine at other than the optimum speed,  $S_{T0}$  (shown by a dash-dotted line) may be seen on the figure. For example, at 10,000 hp:

<u>Speed</u>	<u>Fuel Rate</u>	<u>SFC</u>	<u>% Increase in Fuel</u>
2000 rpm	5099 lb/hr	0.510	7.1
2840 rpm <sup>(2)</sup>	4760 lb/hr	0.476	0
3600 rpm	4966 lb/hr	0.497	4.3

(1) Based on NSRDC, Annapolis values developed for superconductive drive system studies; the values used (with the possible exception of  $W_{MIN}$ ) should not vary significantly for 20,000 hp turbines other than the LM-2500; while the study results for each configuration depend on the specific constants, comparative results between configurations are not highly sensitive to the choice of constants.

(2) Optimum speed.

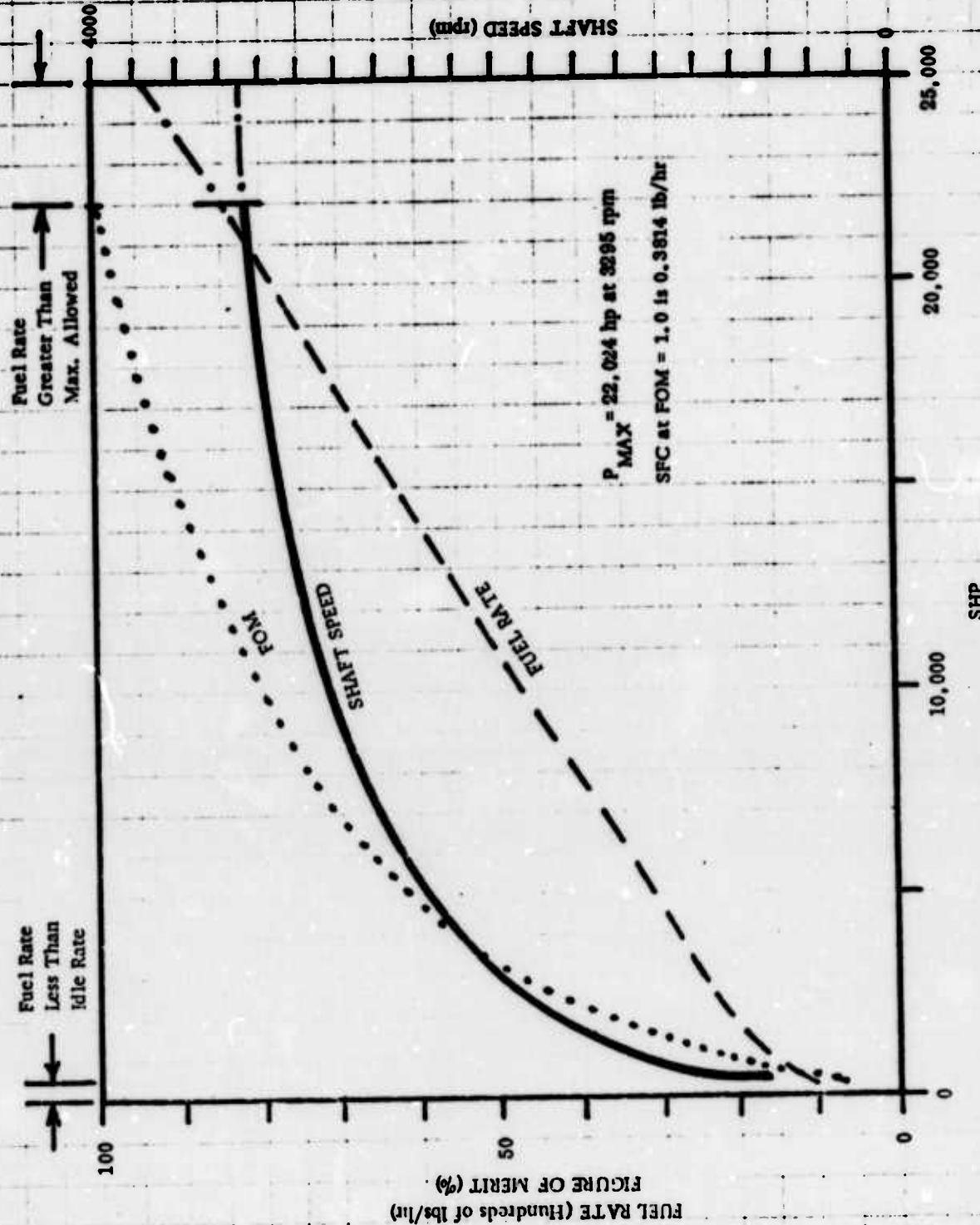


Figure A-2. LM-2500 Turbine Model - Optimum Operating Conditions

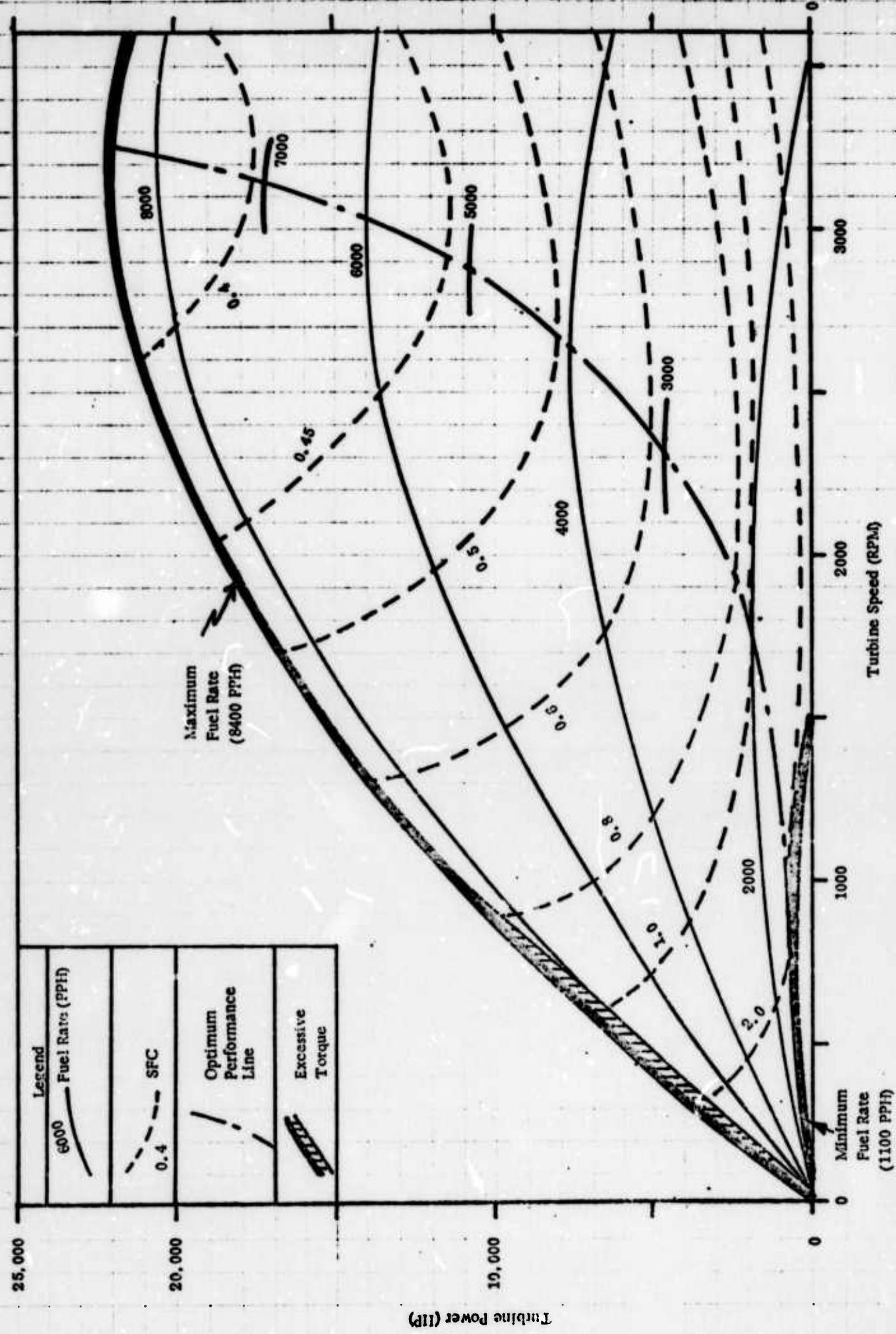


Figure A-3. LM-2500 Turbine Model - Power and SFC vs. Speed

### A.1.2 Cruise (Garrett GTPF990) Turbine

The following constants were used<sup>(1)</sup>:

$$W_1 = 750$$

$$W_3 = 3.35$$

$$W_2 = 0.06$$

$$W_4 = 19 \times 10^{-5}$$

$$W_{MIN} = 360 \text{ lb/hr}$$

$$W_{MAX} = 2700 \text{ lb/hr}$$

$$Q_{MAX} = 7500 \text{ lb-ft}$$

$$S_{MAX} = 7200 \text{ rpm} \quad (2)$$

Resulting optimum performance points are shown in figure A4, and performance as a function of power and speed are shown in figure A5.

Maximum power is 5716 hp at 7200 rpm<sup>(3)</sup> with an SFC of 0.4724 (FOM = 1.0).

### A.1.3 Adjusted FOM

The figure-of-merit expresses the turbine efficiency as a percent of its optimum SFC. The SFC, in turn, may be related to the thermal efficiency of the turbine.

- 
- (1) Based on NSRDC-Annapolis superconducting propulsion study values (characteristic of 5,000 hp turbines; see footnote<sup>(1)</sup> on page A-5).
  - (2) 7200 rpm is the power assembly speed; the standard Navy version has a built-in 2-1 gear reduction to 3600 rpm. Ref: Gas Turbine World, September 1974, p. 12.
  - (3) Performance is limited by the 7200 rpm shaft speed limit; if there were no speed limitation, optimum speed would be 7238 rpm with no change in the SFC (SFC = 0.4724).

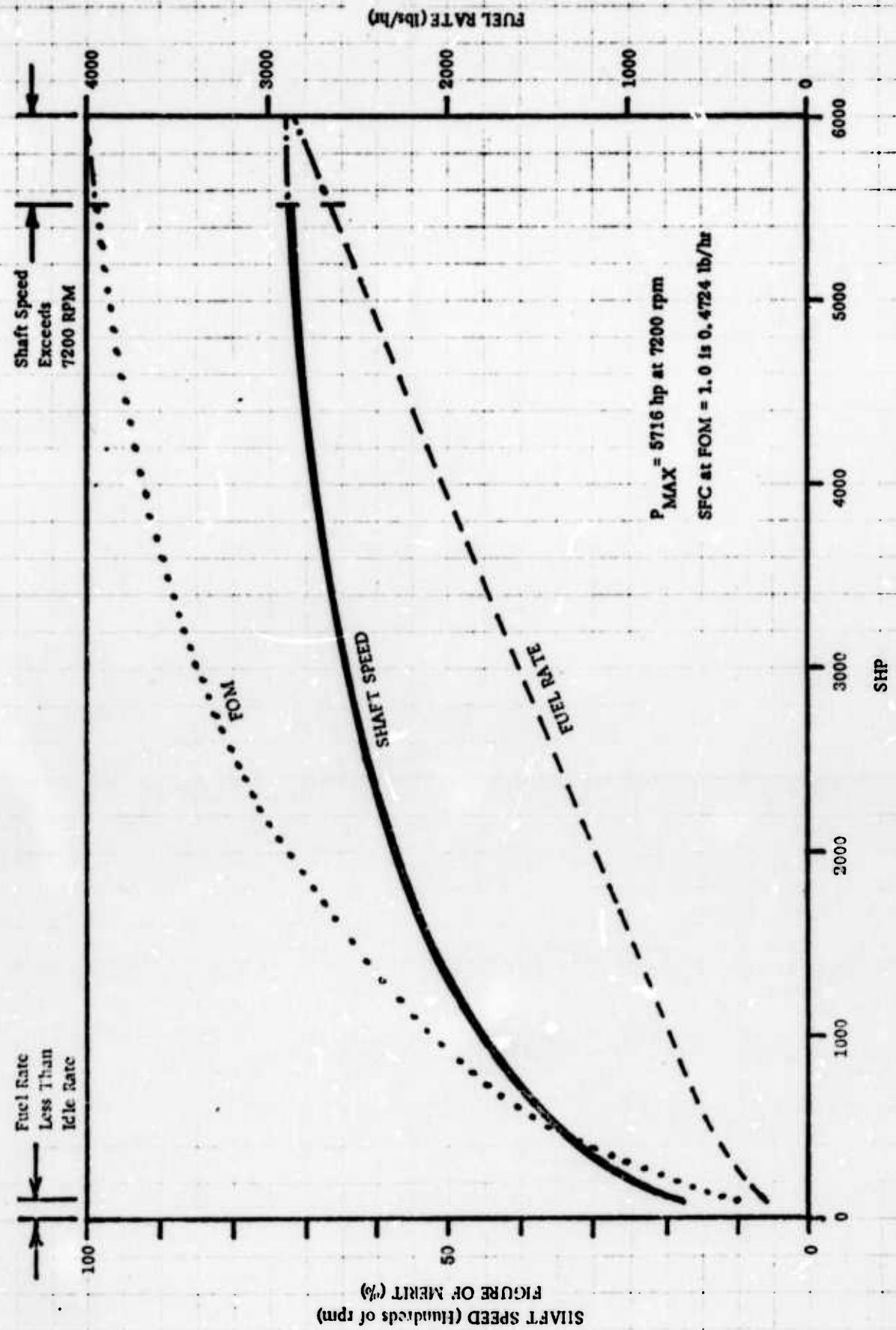


Figure A-4. Garrett 990 Turbine Model - Optimum Operating Conditions

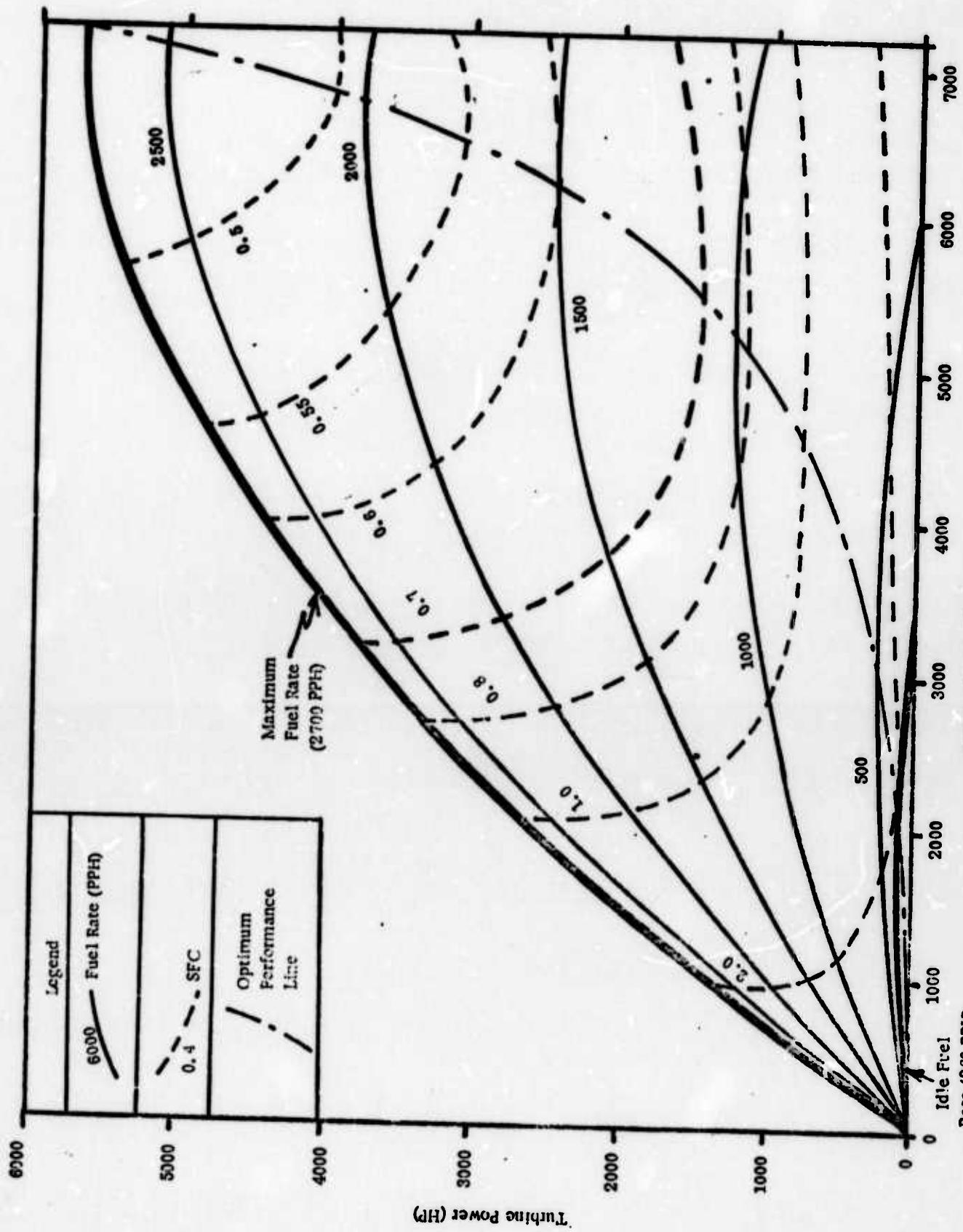


Figure A-5. Garrett S30 Turbine Model - Power and SFC Vs. Speed

Taking the gross heat of combustion of Navy distillate fuel as 19,300 btu/lb<sup>(1)</sup> and using 2545 btu/hp-hr gives a value of 0.1319 lbs of fuel/hp-hr for 100% conversion efficiency. For the two turbines:

	<u>Min. SFC</u>	<u>Max. Thermal Eff.</u>
Main	0.3814	0.3457
Cruise	0.4724	0.2791

and:

$$\text{Thermal Eff.} = \text{FOM} \times (\text{Max. thermal eff.})$$

The use of FOM, frees the analysis from fuel type and is used in the system analysis. In order to compare the two turbines on a common basis, the cruise turbine FOM is adjusted to account for its reduced thermal efficiency whenever comparisons are made between turbines. The adjusted cruise FOM is:

$$\text{Adjusted Cruise FOM} = \frac{\text{Main SFC}_{\text{Min}}}{\text{Cruise SFC}_{\text{Min}}} \times \text{FOM} = 0.8074 \times \text{FOM.} \quad (\text{A7})$$

For the adjusted cruise FOM:

$$\text{Thermal Eff.} = (\text{Adj. FOM}) \times (\text{Max. thermal eff. for main turbine})$$

---

(1) R.J. Gauthey and J.P. DeTolla, "The Energy Crises and Naval Ship Research and Development," Naval Engineers Journal, 86, June 1974, p. 101.

## A.2 PROPELLER MATH MODEL

In order to obtain a reasonable estimate of propeller performance, the behavior of thrust and torque coefficients for a standard propeller series<sup>(1)</sup> were linearized and modeled as follows:

$$C_T = T_M \left( 1 - \frac{J}{T_0} \right) \quad (A8)$$

$$C_Q = Q_M \left( 1 - \frac{J}{Q_0} \right) \quad (A9)$$

$$\begin{aligned} T_M &= T_{M1} + T_{M2} R + T_{M3} R^2 \\ T_0 &= T_{01} + T_{02} R + T_{03} R^2 \end{aligned} \quad \left. \begin{array}{l} \\ \end{array} \right\} \quad (A11)$$

$$Q_M = Q_{M1} + Q_{M2} \sin [Q_{M3} (R - Rx)]$$

$$Q_0 = Q_{01} + Q_{02} R + Q_{03} R^2$$

Where:  $C_T$  = Thrust coefficient

$C_Q$  = Torque coefficient

$J$  = Advance coefficient

$T_M$  = Value of  $C_T$  at  $J = 0$

$T_0$  = Value of  $J$  at  $C_T = 0$

$Q_M$  = Value of  $C_Q$  at  $J = 0$

---

(1) T.P. O'Brien, The Design of Marine Screw Propellers, Hutchison Scientific and Technical Publishers, London. Gawn standard screw series (pp. 88-92) was used to obtain the model form.

(Cont'd)

$$Q_0 = \text{Value of } J \text{ at } C_Q = 0$$

R = Pitch to Diameter (P/D) ratio

$$T_{M1}, T_{M2}, T_{M3}, T_{01}, T_{02}, T_{03}, Q_{M1}, Q_{M2},$$

$Q_{M3}$ ,  $Q_{01}$ ,  $Q_{02}$ ,  $Q_{03}$  and RX are constants

characterizing the propeller.

The following standard relationships are used:

$$J = \frac{V}{nD} = 101.3 \frac{V}{SD}$$

$$T = e n^2 D^4 C_T$$

$$Q = e n^2 D^5 C_Q$$

$$\eta_p = \frac{J}{2\pi} \cdot \frac{C_T}{C_Q}$$

Where:  $V$  = Ship speed in fps

$V$  = Ship speed in knots

$n$  = Propeller speed in rev/sec

$S$  = Propeller speed in rpm

$D$  = Propeller diameter in feet

$e$  = Water density in slugs/ft<sup>3</sup>

$T$  = Thrust in lbs

$Q$  = Torque in lb - ft

$\eta_p$  = Propeller efficiency

} (A12)

**Maximum propeller efficiency occurs at:**

$$J = Q_0 \left[ 1 - \sqrt{1 - \frac{T_0}{Q_0}} \right] \quad (J \text{ for max } \eta_p). \quad (\text{A13})$$

The relationships between  $J$ ,  $C_T$ ,  $C_Q$ ,  $T_0$ ,  $T_M$ ,  $Q_0$ ,  $Q_M$ , and  $N$  are shown in figure A6.

For the propeller model used in the study the following values were used:

$$T_{01} = 0.0500 \qquad Q_{01} = 0.4550$$

$$T_{02} = 1.0130 \qquad Q_{02} = 0.5470$$

$$T_{03} = 0.0060 \qquad Q_{03} = 0.1577$$

$$T_{M1} = -0.2600 \qquad Q_{M1} = 0.1830$$

$$T_{M2} = 1.0000 \qquad Q_{M2} = 0.1633$$

$$T_{M3} = -0.1800 \qquad Q_{M3} = 1.5160$$

$$D = 17 \text{ ft} \qquad R_X = 1.4250$$

$$\rho = 1.9905 \text{ slugs/ft}^3.$$

These values were selected to:

- a. Match the general characteristics of the Gawn standard screw series in terms of relative efficiencies at various pitches.
- b. Provide approximately 72 to 73% efficiency under actual operation (selected arbitrarily as a reasonable efficiency).

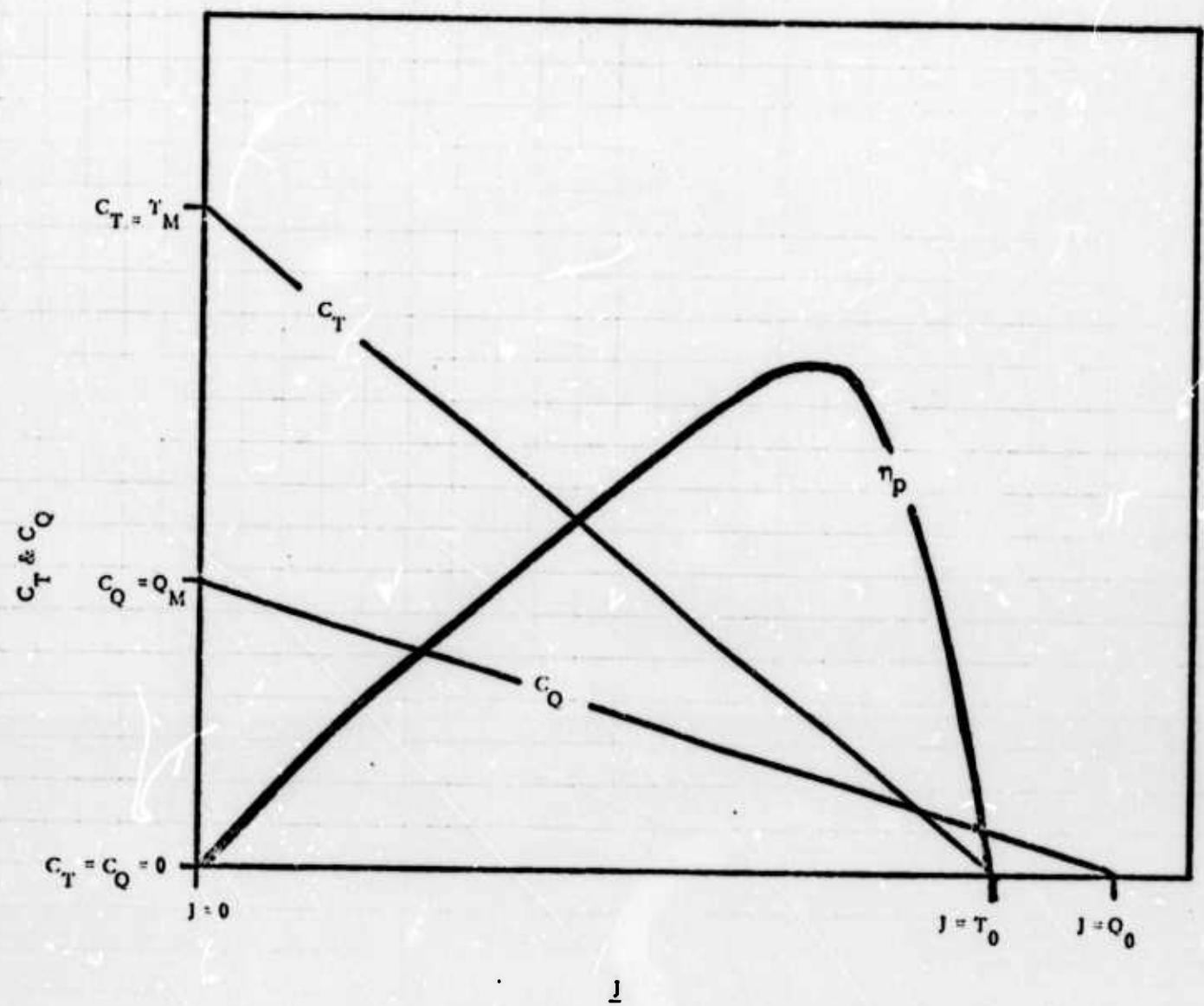


Figure A-6. Propeller Relationships

The values given for c and D provide the following characteristics:

$$J = 5.961 \frac{V}{S} \quad (A14)$$

$$T = 46.18C_T \cdot S^2 \quad (A15)$$

$$Q = 785.1C_Q \cdot S^2 \quad (A16)$$

The values given for  $T_{M1}$ ,  $T_{M2}$ , etc. give the values shown in  
table A1.

Table A-1  
Propeller Characteristics vs P/D

<u>P/D</u>	<u>T<sub>M</sub></u>	<u>T<sub>0</sub></u>	<u>Q<sub>M</sub></u>	<u>Q<sub>0</sub></u>	<u>J</u>	<u>Maximum Efficiency</u> <u><math>\eta_p</math></u>
0.2735	0.0000	0.3275	0.02219	0.6164	0.1944	0.0000
0.3000	0.0238	0.3544	0.02118	0.6333	0.2131	0.0229
0.4000	0.1112	0.4562	0.01972	0.6990	0.2870	0.1620
0.5000	0.1950	0.5580	0.02201	0.7679	0.3664	0.3392
0.6000	0.2752	0.6600	0.02799	0.8400	0.4511	0.4825
0.7000	0.3518	0.7620	0.03753	0.9152	0.5408	0.5720
0.8000	0.4248	0.8642	0.05041	0.9935	0.6351	0.6260
0.9000	0.4942	0.9666	0.06632	1.0750	0.7335	0.6602
1.0000	0.5600	1.0690	0.08492	1.1597	0.8354	0.6852
1.1000	0.6222	1.1716	0.10576	1.2475	0.9397	0.7057
1.2000	0.6808	1.2742	0.12837	1.3385	1.0452	0.7237
1.3000	0.7358	1.3770	0.15224	1.4326	1.1504	0.7393
1.4000	0.7872	1.4800	0.17681	1.5299	1.2535	0.7523
1.5000	0.8350	1.5830	0.20153	1.6303	1.3525	0.7621
1.6000	0.8792	1.6862	0.22582	1.7339	1.4462	0.7686
1.7000	0.9198	1.7894	0.24912	1.8407	1.5336	0.7724
1.8000	0.9558	1.8929	0.27092	1.9505	1.6150	0.7746
1.9000	0.9902	1.9964	0.29069	2.0636	1.6911	0.7766
2.000	1.0200	2.1000	0.30799	2.1798	1.7627	0.7799

### A.3 SHIP DRAG MODEL.

The ship's drag characteristics were modeled as follows:

$$EHP = C_D \cdot V^3 \quad (A17)$$

$$C_D = C_{D0} \text{ for } V \leq 27 \text{ knots} \quad (A18)$$

$$C_D = C_{D0} \frac{V - C_2}{V_x - C_2} \text{ for } V \geq 27 \text{ knots}$$

$$D_S = \left( \frac{3600 \text{ sec/hr}}{6080 \text{ ft/mile}} \right) \cdot (550 \text{ lb-ft/sec/hp}) \cdot \frac{EHP}{V} \quad (A19)$$
$$= 325.7 C_D V^2$$

Where: EHP = Effective horsepower

V = Speed in knots

$C_{D0}$ ,  $C_2$  and  $V_x$  are drag constants.

This form was chosen to approximate a  $V^2$  dependence on drag at lower speeds with drag increasing faster in the 30-knot region. Values were chosen for the three constants of:

$$C_{D0} = 1.4 \text{ hp/(kt)}^3$$

$$C_2 = 5 \text{ knots}$$

$$V_x = 27 \text{ knots}$$

The resultant drag/power profile is given in table A2.

Table A-3  
Ship Drag Characteristics

<u>Speed (kts)</u>	<u>Drag (lbs)</u>	<u>Effective Hp</u>	<u>Speed (kts)</u>	<u>Drag (lbs)</u>	<u>Effective Hp</u>
1.0	456.	1.40	19.0	164587.	9602.59
2.0	1824.	11.20	20.0	182368.	11199.99
3.0	4103.	37.80	21.0	201061.	12965.39
4.0	7295.	89.60	22.0	220666.	14907.19
5.0	11398.	175.00	23.0	241182.	17033.79
6.0	16413.	302.40	24.0	262610.	19353.59
7.0	22340.	480.20	25.0	284951.	21874.98
8.0	29179.	716.80	26.0	308202.	24606.38
9.0	36930.	1020.60	27.0	332368.	27556.19
10.0	45592.	1400.00	28.0	373689.	32129.70
11.0	55166.	1863.40	29.0	418286.	37248.61
12.0	65653.	2419.20	30.0	466282.	42954.48
13.0	77051.	3075.80	31.0	517801.	49290.50
14.0	89360.	3841.60	32.0	572968.	56301.31
15.0	102582.	4725.00	33.0	631906.	64033.13
16.0	116716.	5734.40	34.0	694740.	72533.63
17.0	131761.	6878.19	35.0	761594.	81852.19
18.0	147718.	8164.79	36.0	832594.	92039.44

## A.4 TURBINE-PROPELLER- DRAG PERFORMANCE RELATIONSHIPS

### A.4.1 Propeller/Drag Performance

The maximum propeller efficiencies given in table A1 cannot be attained unless the advance coefficient  $J$  is at the proper value. However, under steady-state operating conditions, the value of  $J$  is fixed by the relationship between propeller thrust coefficient and ship's drag, since the total propeller thrust must equal the drag at steady-state.

From A.2 and A.3:

$$T = 46.18 C_T S^2 \quad (A15)$$

$$D_S = 325.7 C_D V^2 \quad (A19)$$

$$J = 5.961 V/S \quad (A14)$$

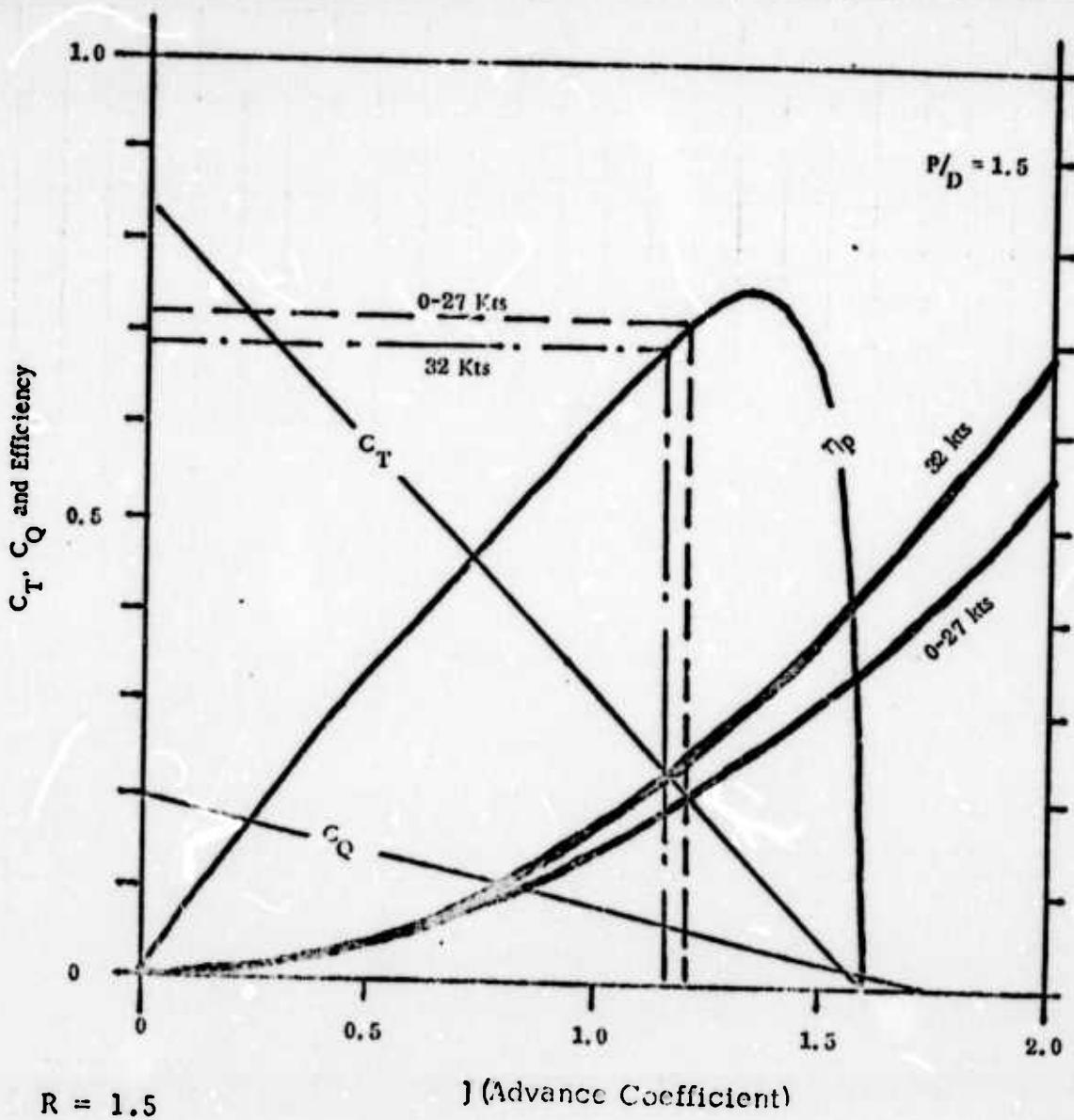
Combining ( $D_S = 2T$ ):

$$C_T = 9.921 \times 10^{-2} C_D J^2$$

while, from A2:

$$C_T = T_M \left( 1 - \frac{1}{T_0} \right) \quad (A8)$$

Figure A7 shows the resulting operating points for a P/D ratio of 1.5. Operating efficiencies and advance coefficient,  $J$ , are given versus P/D ratio in table A3 and figure A8. For speeds up to 27 knots, maximum possible operating efficiency is 72.8% at a P/D ratio of 1.38; at 32 knots maximum efficiency is 71.3% at a 1.29 P/D ratio.



$$R = 1.5$$

$J$  (Advance Coefficient)

$$T_M = 0.8350 \quad Q_M = 0.2015$$

$$T_0 = 1.5830 \quad Q_0 = 1.6303$$

For Maximum  $\eta_p$ :

$$J = 1.353$$

$$\eta_p = 76.2\%$$

Operating Point for 0-27 kts:

$$J = 1.202$$

$$\eta = 72.6\%$$

$$C_T = 0.2010$$

$$C_Q = 0.05294$$

Operating Point for 32 kts:

$$J = 1.153$$

$$\eta = 70.6\%$$

$$C_T = 0.2268$$

$$C_Q = 0.05899$$

Figure A-7. Propeller Operation With  $P/D = 1.5$

<u>P/D Ratio</u>	<u>Maximum Propeller Efficiency</u>	<u>Operating Propeller Efficiency</u> <sup>(1)</sup>	<u>Advance Coefficient (j)</u> <sup>(1)</sup>
0.2735	0	0	0
0.3	0.023	0.022 - 0.023	0.238 - 0.225
0.4	0.162	0.129 - 0.138	0.375 - 0.364
0.5	0.339	0.269 - 0.289	0.469 - 0.456
0.6	0.483	0.404 - 0.430	0.557 - 0.541
0.7	0.573	0.510 - 0.534	0.637 - 0.620
0.8	0.626	0.587 - 0.607	0.718 - 0.696
0.9	0.660	0.643 - 0.655	0.795 - 0.769
1.0	0.685	0.681 - 0.685	0.869 - 0.841
1.1	0.706	0.706 - 0.703	0.940 - 0.909
1.2	0.724	0.720 - 0.711	1.009 - 0.972
1.3	0.739	0.727 - 0.713	1.076 - 1.037
1.4	0.752	0.726 - 0.710	1.140 - 1.095
1.5	0.762	0.726 - 0.706	1.202 - 1.149
1.6	0.769	0.723 - 0.700	1.262 - 1.209
1.7	0.772	0.719 - 0.695	1.319 - 1.263
1.8	0.775	0.716 - 0.691	1.374 - 1.312
1.9	0.777	0.715 - 0.689	1.426 - 1.361
2.0	0.780	0.716 - 0.690	1.476 - 1.406

<sup>(1)</sup> First value is for 0 to 27 kts; second is for 32 kts.

Table A-3. Propeller Operating Efficiency Versus P/D Ratio

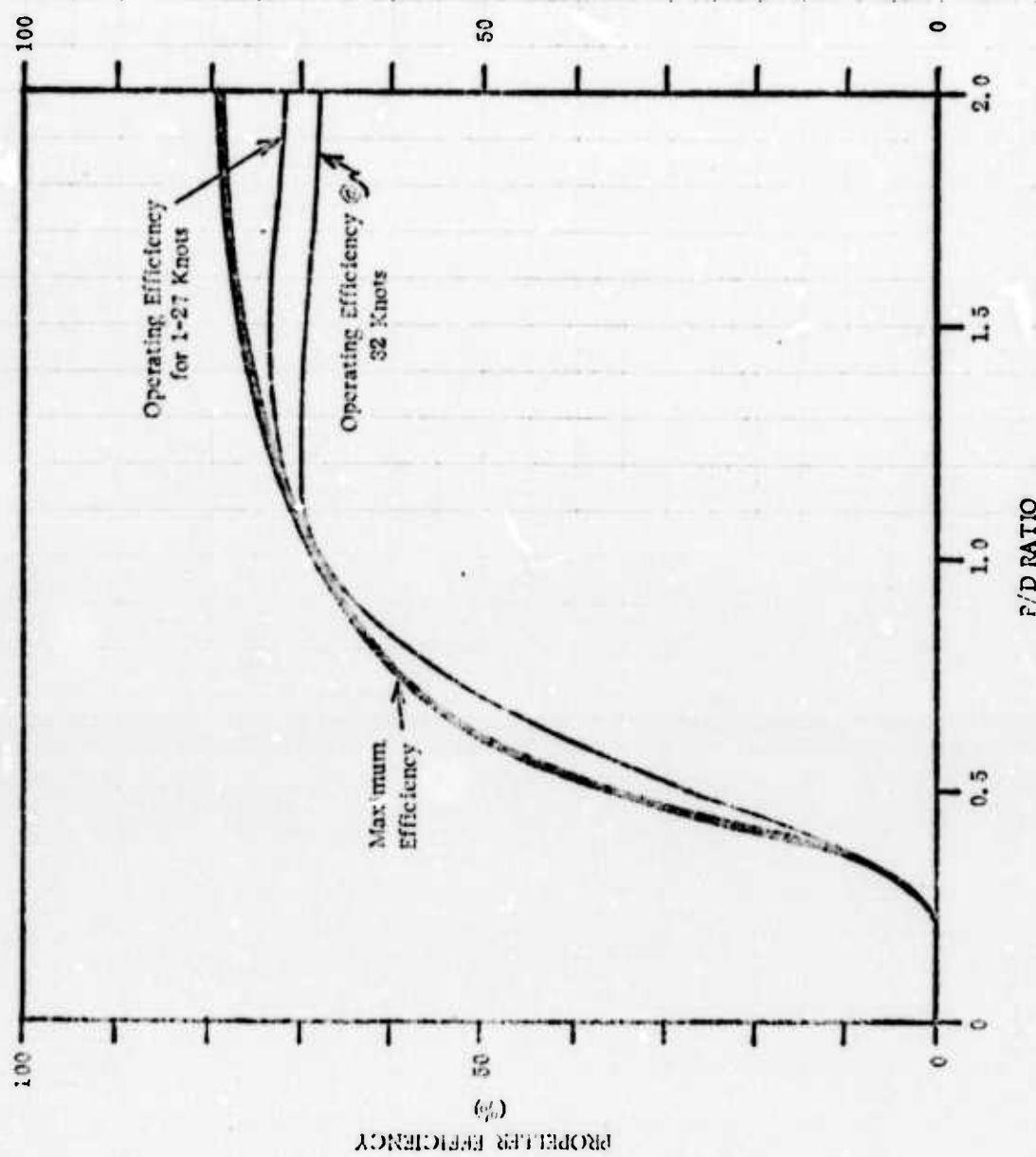


Figure A-8. Propeller Efficiency vs. P/D Ratio

From Section A.2,

$$J = 5.961 \frac{V}{S} \quad (A14)$$

This results in a limitation on P/D ratio if propeller shaft speed is limited; for example, 32 knots:

<u>Maximum Allowed Shaft rpm</u>	<u>Minimum Allowable P/D Ratio</u>
160	1.57
165	1.51
170	1.45
175	1.39
180	1.34

## A.4.2 Propeller/Turbine Performance

### A.4.2.1 Optimum Pitch

As discussed in A.4.1 and A.1, propeller efficiency and turbine efficiency are both affected by shaft rpm. If there is a fixed mechanical gear ratio between the propeller shaft and turbine, the optimum P/D ratio for minimum fuel rate will occur at some value other than that for the turbine or propeller alone. For example, with two main turbines operating at 23 kts and 96% drive efficiency:

Maximum Propeller Efficiency = 0.728 at 120 rpm  
With a P/D ratio of 1.4

Maximum Turbine IOM = 0.862 at 3392 rpm  
With an output of 26,050 hp

If the gear ratio were 28.3 to 1 (3392 rpm/120 rpm), the turbine would deliver 25,010 shaft hp and effective power would be 18,210 hp with an (ideal) efficiency of:

$$0.728 \times 0.862 \times 0.960 = 0.602.$$

However, with a fixed gear ratio of 21.5 to 1, optimum performance occurs as shown in figure A9:

P/D Ratio	= 1.27
Shaft Speed	= 130 rpm
Turbine Speed	= 2783 rpm
Effective Power	= 17,030 <sup>(1)</sup>

---

<sup>(1)</sup> Fixed at 17,030 hp by drag at 23 knots.

Shaft Power	= 23,470 hp
Turbine Power	= 24,450 hp <sup>(1)</sup>
Fuel Rate	= 10,930 lbs/hr
Propeller Efficiency	= 0.726
Turbine FOM	= 0.853
Drive Efficiency	= 0.960
Overall Propulsion Efficiency	= 0.594

For the same conditions (23 knots with two main turbines) the electrical drive system is optimized by adjusting the "gear ratio" through reduction of the generator magnetic field and optimizes as follows:

P/D Ratio	= 1.35
Shaft Speed	= 124 rpm
Turbine Speed = 2960 rpm	(76.6% magnet field)
Effective Gear Ratio	= 23.9 to 1
Effective Power	= 17,030 hp
Shaft Power	= 23,040 hp
Turbine Power	= 24,100 hp
Fuel Rate	= 10,800 lbs/hr
Propeller Efficiency	= 0.728
Turbine FOM	= 0.852 <sup>(2)</sup>
Drive Efficiency	= 0.971
Overall Propulsion Efficiency	= 0.602

---

(1) Turbine Power = (Effective hp)/(propulsion efficiency x drive efficiency)

(2) The slight decrease over the geared case in turbine FOM reflects the drop in turbine power required; 0.852 is the maximum FOM for 24,100 hp from two turbines.

The electric drive is thus 1.3% more efficient at 23 knots; at lower speeds the difference is more pronounced, leading to an overall 6-7% advantage for the electric drive when averaged over the mission profile.

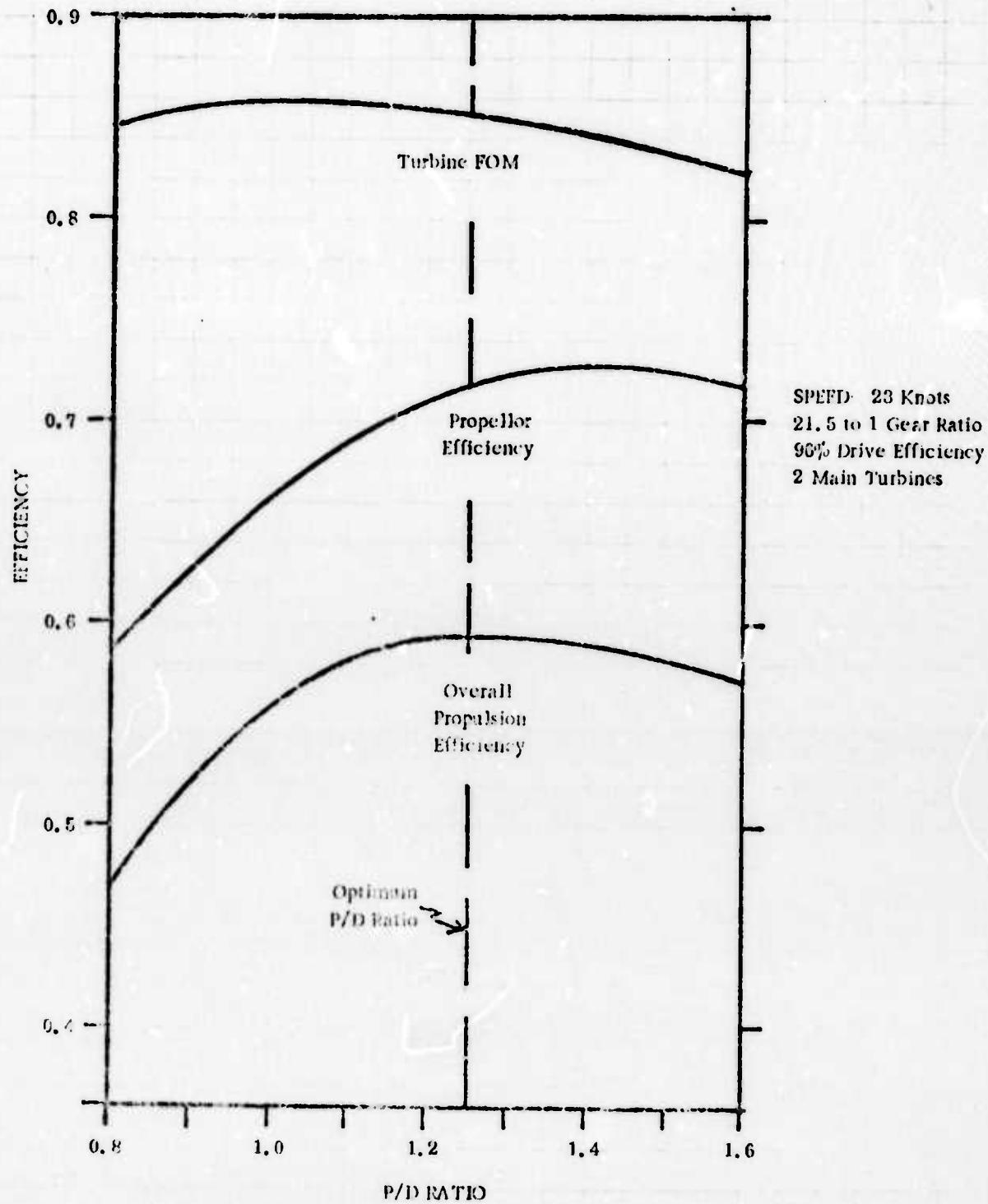


Figure A-9. Operating Point With Fixed Gear Ratio

#### A.4.2.2 Selection of Gear Ratios and Electric Machinery Voltages

The propeller pitch determines the propeller rpm at each speed; turbine rpm and efficiency then depend on the gear ratio, in the geared drive case, and on the motor/generator emf (volts/rpm), in the electric drive case. The combination is limited by:

- Propeller cavitation
- Turbine upper speed limit.

In order to determine the optimum gear ratios for the turbines and the optimum electric machine voltages, the system math model was exercised subject to the following constraints:

- Propeller limited to 168 rpm<sup>(1)</sup>
- Main turbine limited to 3600 rpm
- Cruise turbine limited to 7200 rpm

The results gave, for minimum fuel consumption:

- Main Gear Ratio 21.5 to 1
- Cruise Gear Ratio: 74.0 to 1
- Electric Motor emf: 1.6328 v/rpm<sup>(2)</sup>
- Main Generator: 0.0911 v/rpm<sup>(2)</sup>
- Cruise Generator: 0.0209 v/rpm<sup>(2)</sup>

---

(1) Based on cavitation; see, D.A. Rains and R.J. d'Arcy, "Considerations in the DD 963 Propulsion System Design," Naval Engineers Journal, August 1972, p. 68.

(2) The electric drive system has a variable "gear ratio" with minimum values of 17.9 to 1 for the main turbines and 78 to 1 for the cruise turbines.

#### A.4.2.3 Selection of Operating Pitches

With the gear ratios and electrical constants established, the optimum propeller pitch for each speed was determined. The result for the geared drive with main turbines is shown in figure A10. Below 5 knots with one turbine, and below 7 knots with two turbines, pitch must be used to regulate speed because the turbine fuel rate is at its minimum value of 1100 lbs/hr per turbine. At 5 knots, the optimum pitch for 1 turbine is 1.15; it drops to 1.06 at 11 knots and then rises to 1.16 at 21 knots. Similar effects occur for each combination of turbines. A continuously variable pitch is undesirable for cruise conditions, since the minimum fuel rate can be closely approached by using a fixed pitch for each combination of turbines in use.

Based on the results shown in figure A9 and similar results for the cruise turbines, fixed pitch ratios were selected for each combination of turbines. These values were verified as giving optimum performance by inserting them in the math model and running them over the mission profile. The values selected were:

Number of Turbines	Baseline System	Baseline +Alternators	Baseline +Cruise Turbines	Alternators +Cruise Turbines
1 Cruise	-	-	-	1.10
2 Cruise	-	-	1.25	1.30
1 Main	-	1.10	-	1.10
2 Main	1.20	1.30	1.30	1.30
3 Main	-	1.40	-	1.40
4 Main	1.50	1.50	1.50	1.50

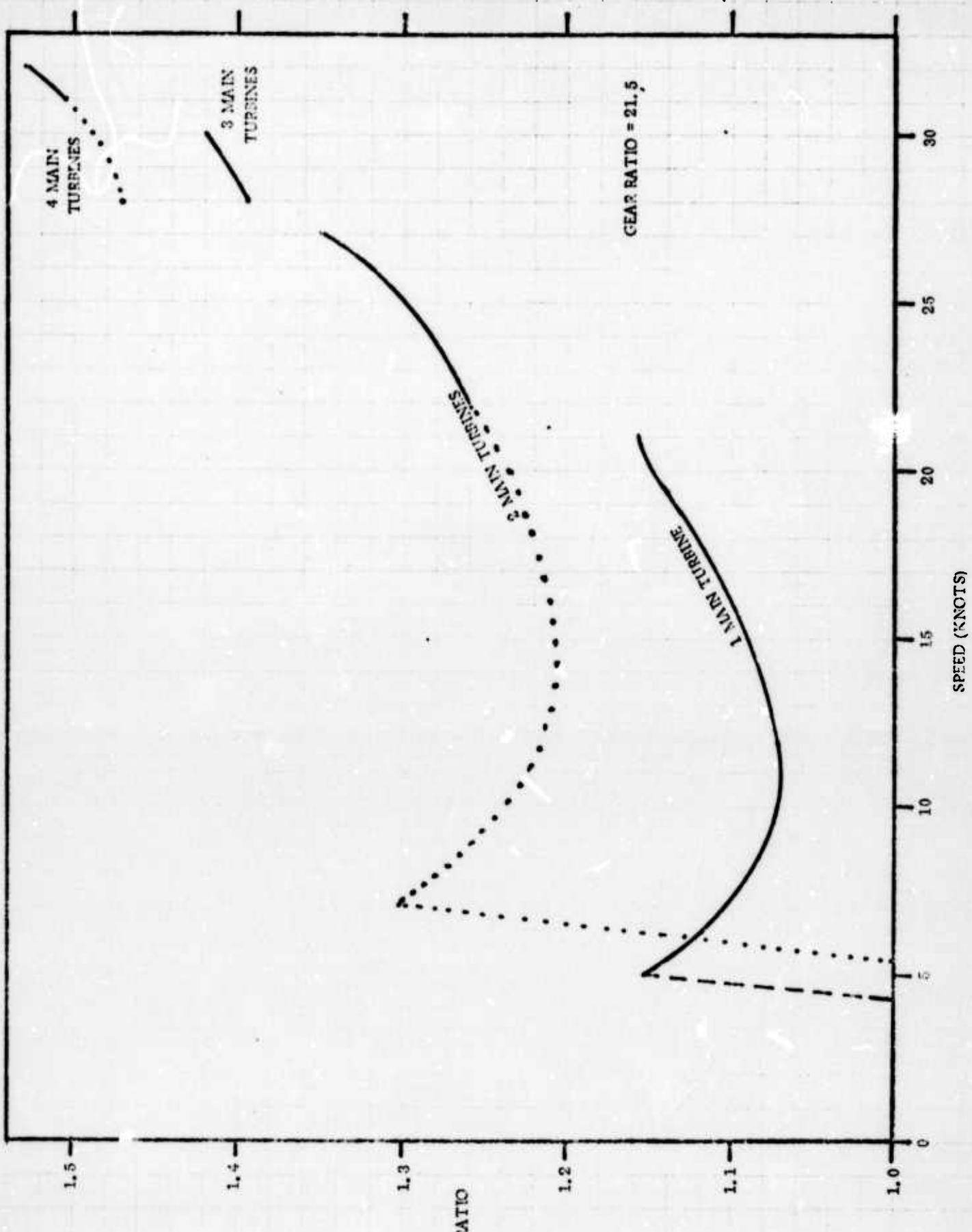


Figure A-10. Optimum P/D Ratio vs. Speed - Geared Drive

For the electric system, the optimum pitch is much closer to the pitch (1.38) where maximum propeller efficiency occurs, as shown in figure A11<sup>(1)</sup>. Because of the small variation in optimum pitch in the electric drive case, it is advantageous to use a fixed pitch propeller and a single pitch was therefore selected for the electric drive. The minimum fuel consumption over the mission profile occurs for a P/D ratio of 1.35; however, this requires a propeller speed of 179 rpm at 32 knots. In order to keep propeller speed close to 168 knots, a fixed P/D ratio of 1.45 was selected resulting in 169.6 rpm at 32 knots (a P/D of 1.50 would give 165.4 knots and the nearest 0.05 variation in P/D was selected).

---

(1) Pitch is set to 1.5 when the turbine fuel rate is at idle and speed is controlled by varying the magnet field.

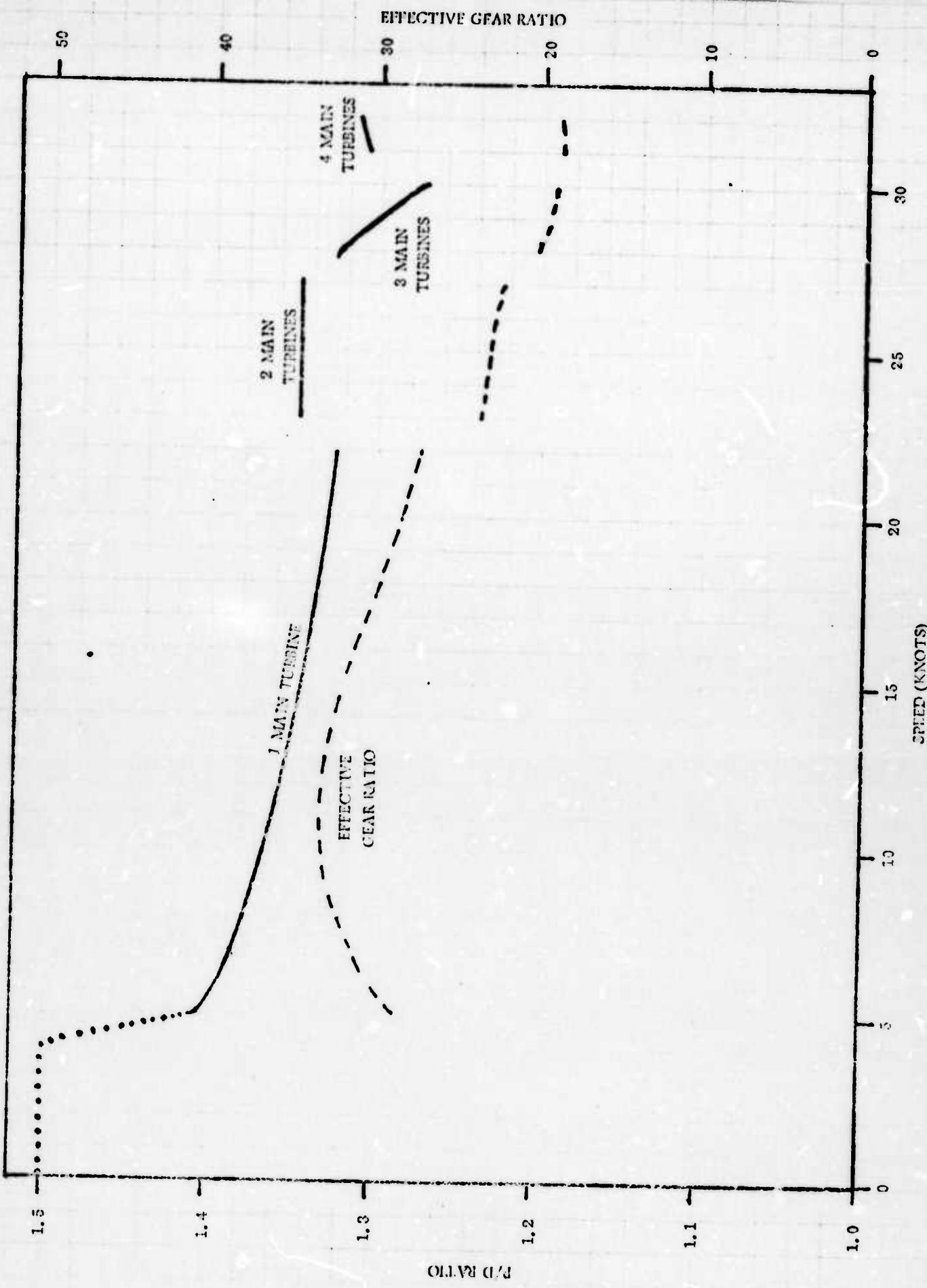


Figure A-11. Optimum P/D Ratio vs. Speed - Electric Drive

## A.5 ENDURANCE CALCULATIONS

Endurance calculations are based on BUSHIPS Design Data Sheet DDS 9400-1<sup>(1)</sup>. Values of endurance and endurance speed used to calculate endurance fuel load were selected to match those of the DD-931 and DL-2: 4500 miles at 20 knots<sup>(2)</sup>.

Endurance power and fuel rate were taken from the baseline math model analysis. Ships service electric load was estimated at 4,000 kw at a fuel rate of 0.8 lb/kw-hr (see Appendix B) and "fuel consumption for other services" was estimated at 10% of the ships service electric load. A "tailpipe allowance factor" of 0.95 was selected (i.e. 5% of the fuel is unavailable). The endurance fuel load calculations, based on DDS 9400-1, are shown in Table A4. The result of the calculation is 1428 long tons of fuel; 1430 tons was selected as the endurance fuel load.

- 
- (1) Design Data Sheet DDS 9400-1, "Calculation of Surface Ship Endurance Fuel Requirements," 1 Nov. 1963.
  - (2) R.T. Miller, C.L. Long and S. Reitz, "ASW Surface Ship of the "80's" Study," Naval Engineers Journal, Dec. 1972, p. 15.

Table A-4

ENDURANCE FUEL LOAD<sup>(1)</sup>

(1)	Endurance	4,500 n. miles <sup>(2)</sup>
(2)	Endurance Speed	20 knots <sup>(2)</sup>
(3)	Full Load Displacement	7,600 l. tons
(4)	Full Rated Power	80,000 SHP
(5)	Endurance Power at (2) and (3)	15,500 SHP <sup>(3)</sup>
(6)	Avg. Endurance Power $= 1.1 \times 5$	17,100 SHP
(7)	Ratio: (6) / (4)	0.21
(8)	Cruising Electric Load	4,000 kw <sup>(4)</sup>
(9)	Fuel Rate at (6)	0.517 lb/SHP-hr <sup>(3)</sup>
(10)	Prop. Fuel Consumption $= (6) \times (9)$	8,850 lbs/hr
(11)	Aux. Gen. Fuel Rate at (8)	0.8 lb/kw-hr <sup>(4)</sup>
(12)	Aux. Gen. Fuel Consumption $= (8) \times (11)$	3,200 lb/hr
(13)	Fuel Consumption for Other Services	320 lb/hr <sup>(5)</sup>
(14)	All-Purpose Fuel Consumption $= (10) + (12) + (13)$	12,370 lb/hr
(15)	All-Purpose Fuel Rate $= (14) / (6)$	0.723 lb/SHP-hr

(1) Ref: BUSHIPS Design Data Sheet DDS 9400-1, "Calculation of Surface Ship Endurance Fuel Requirements," 1 Nov. 1963.

(2) Values selected to equal DD-931 and DL-2.

(3) Values from baseline model.

(4) Estimated values for ships service.

(5) Estimated at 10% of auxiliary generator fuel consumption.

Table A-4 (Cont'd)

(16)	Fuel Rate Correction Factor	1.04 <sup>(1)</sup>
	based on (7)	
(17)	Specific Fuel Rate	0.752 lb/SHP-hr
	= (15) x (16)	
(18)	Endurance Fuel Rate	0.790 lb/SHP-hr
	= (17) x 1.05 <sup>(2)</sup>	
(19)	Burnable Fuel	1,357 l.tons
	= (1) x (6) x (18) / ((2) x 22.0)	
(20)	Tailpipe Allowance Factor	0.95 <sup>(3)</sup>
(21)	Endurance Fuel Load	1,428 l.tons
	= (19) / (20)	

(1) Value from ref. (1) above; (1.04 applies for (7)  $\leq 1/3$ ).

(2) Value from ref. (1) above; represents arbitrary 5% increase in fuel rate to allow for deterioration over two-year period.

(3) Value from ref. (1) above; 0.95 factor selected for broad, shallow tanks.

The endurance fuel load computation reduces to:

$$4.935 \times 10^{-4} K \left( \frac{\text{Endurance}}{\text{End. Speed}} \right) (\text{All-Purpose Fuel Consumption})$$

Where:

K = Fuel Rate Correction Factor

$$= 1.04 \text{ for } \left( \frac{\text{SHP}}{\text{Full Rated Power}} \right) \leq 0.33$$

$$= 1.03 \text{ for } 0.34 \leq \left( \frac{\text{SHP}}{\text{FRP}} \right) \leq 0.66$$

$$= 1.02 \text{ for } \left( \frac{\text{SHP}}{\text{FRP}} \right) > 0.67$$

$$\begin{aligned} \text{All-Purpose Fuel Consumption} &= (\text{Propulsion Fuel Consumption})^{(1)} \\ &+ (\text{Auxiliary Generator Fuel Consumption}) + (\text{Fuel Consumption} \\ &\text{for other Services}). \end{aligned}$$

Conversely:

$$\text{Range (Endurance)} = \frac{2027 \text{ (Speed) (Endurance Fuel Load)}}{K \text{ (All-Purpose Fuel Consumption)}} \quad (A20)$$

---

(1) Takes into account fuel required at endurance speed in endurance calculations (allows for adverse sea conditions and bottom fouling over a two year period).

In order to provide a comparison between various configurations, range was calculated according to the above expression. The total of auxiliary generator and other services was held fixed at 3520 lb/hr in all calculations. Fuel rate was taken from the computer results at each speed<sup>(1)</sup> and an allowance was made for additional ships service load as follows:

$$\begin{aligned}\text{Added Ship Service Load (kw)} &= (\text{Cooling Load}) \\ &+ (\text{Refrigeration Load}) + (\text{Lubrication Load})\end{aligned}$$

Where:

Cooling Load (kw) = 0.02 (Turbine HP - Shaft HP)  
(Estimated ship service load required for pumping coolant and seawater to remove heat generated by losses).

Refrigeration Load = Power required for helium compressors

Lubrication Load = Power required for lubrication of electrical generators<sup>(2)</sup>.

Added Fuel Load (lb/hr) = 0.8 x (Added Ships Service Load)

(1) No 110% adjustment factor used on power.

(2) Motor lubrication considered even tradeoff against mechanical gear system.

Example:

Electric drive system with cruise turbines at 25 knots; two main turbines operating:

Turbine HP = 30980  
Shaft HP = 30040 } 19 kw cooling load

Refrigeration Load = 130 kw

Lubrication Load = 2 kw (Two Generators)

Total added ships service load: 151 kw

x 0.8 = 121 lb/hr added fuel load

Fuel rates:

Turbines: 12,890 lb/hr

Added Load: 121 lb/hr

Ships Service: 3520 lb/hr

Total: 16,531 lb/hr (All-purpose fuel rate)

SHP  $\div$  Rated Power (80,000 HP) = 0.38; K = 1.03

Range =  $\frac{2027 (25) (1430)}{1.03 (16531)} = 4256 \text{ miles}$

Average results over the mission profile are based on the average mission speed of 15.8 knots and the average power loss and lubrication load. The endurance fuel load is reduced by the weight of any added propulsion equipment.

i.e., over the mission profile:

$$\text{Range} = \frac{2027 (15.8) (1430 - \text{Added Equipment Weight})}{1.04 (\text{Average All-Purpose Fuel Consumption})}$$

$$= \frac{30795 (1430 - \text{Added Weights})}{(\text{Average All-Purpose Fuel Consumption})} \quad (\text{A21})$$

Example:

For the geared-drive baseline:

$$\begin{aligned} \text{Average Turbine HP} &= 10770 \\ \text{Average Shaft HP} &= 10340 \\ \text{Refrigeration Load} &= 0 \\ \text{Lubrication Load} &= 0 \\ &\qquad\qquad\qquad 9 \text{ kw total load (7 lb/hr)} \end{aligned}$$

Fuel Rates:

$$\text{Average Turbine Fuel Rate} = 6392 \text{ lb/hr}$$

$$\text{Average Added Load} = 7 \text{ lb/hr}$$

$$\text{Ships Service Load} = \underline{3520 \text{ lb/hr}}$$

$$9919 \text{ lb/hr total}$$

$$\text{Added Weight} = 0$$

$$\text{Range} = \frac{30795 (1430)}{9919} = 4440 \text{ miles}$$

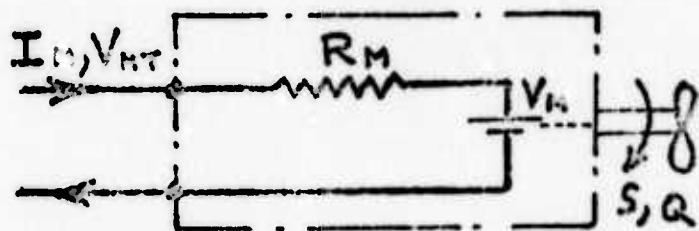
## A.6 ELECTRIC DRIVE MATH MODELS

Math models for the electric motors, generators, transmission lines, and buss lines are shown in figures A-12 through A-14.

## A.7 ALTERNATOR MATH MODEL

Analysis of the crossover efficiency, as shown in figure A-15 gives an expression for drive system efficiency in the crossover mode equal to 0.921 for a drive efficiency of 0.96 and alternator efficiencies of 0.98 each. The same result is obtained by using  $0.96 \times (0.98)^2$ ; i.e., by multiplying the drive efficiency by the alternator pair efficiency of 0.96. The latter method is used in the computer program whenever crossover is used.

MOTOR MATH MODEL



$I_M$  = Input Current (Amps)

$V_{MT}$  = Terminal Voltage

$V_M$  = Back emf (volts)

$R_M$  = Internal resistance (ohms)

$S$  = Shaft rpm

$Q$  = Shaft torque (lb-ft)

$K_M$  = Back emf (volts/rpm)

$K_F$  = Friction loss ( $\text{Kw}/\text{rpm}^2$ )

$K_E$  = Eddy current loss ( $\text{Kw}/\text{rpm}^2$ )

$K_V$  = Viscous loss ( $\text{Kw}/\text{rpm}^3$ )

Given  $S$  and  $Q$  (from propeller characteristics)

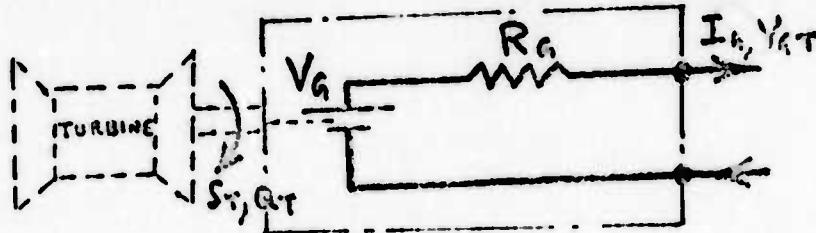
$$I_M = \frac{0.1428 S \cdot Q + 1000 (K_F S^2 + K_E S^2 + K_V M S^3)}{K_M S}$$

$$V_M = K_M S$$

$$V_{MT} = V_M + I_M R_M$$

Figure A-12

### GENERATOR MATH MODEL



$I_G$  = Generator Current (amps)

$V_{GT}$  = Terminal Voltage

$V_G$  = Back emf (volts)

$R_G$  = Internal Resistance (ohms)

$S_T$  = Shaft (turbine) rpm

$P_T$  = Turbine hp

$K_G$  = Back emf (volts/rpm)

$K_F$  = Friction loss ( $\text{Kw}/\text{rpm}^2$ )

$K_E$  = Eddy current loss ( $\text{Kw}/\text{rpm}^2$  at full field)

$K_V$  = Viscous loss ( $\text{Kw}/\text{rpm}^3$ )

$P_f$  = Percent magnet field

Given  $I_G$  and  $V_{GT}$  (from Buss Line):

$$V_G = V_{GT} - I_G R_G$$

$$S_T^* = \frac{V_G}{P_f K_G}$$

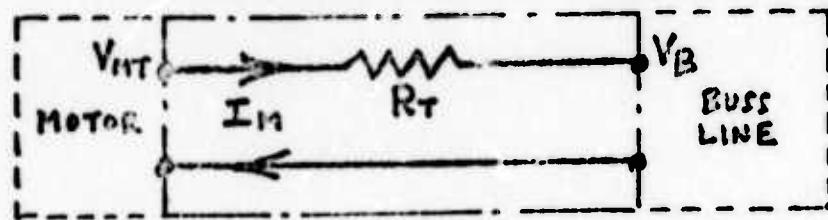
$$P_T^* = \frac{I_G V_G + 1000 \left[ K_F S_T^{*2} + K_E (P_f S_T)^2 + K_V S_T^3 \right]}{745.7}$$

---

\*  $S_T$  and  $P_T$  are a function of the percent magnet field.

Figure A-13

### TRANSMISSION LINE MATH MODEL



$V_{MT}$  = Motor terminal voltage

$V_B$  = Buss voltage

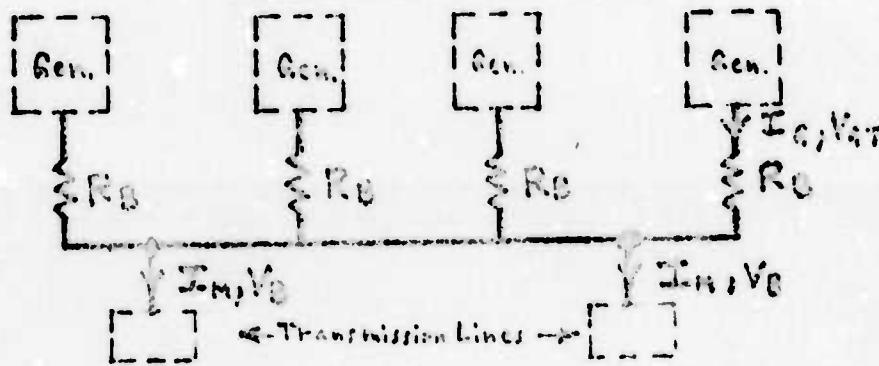
$I_M$  = Motor current (amps)

$R_T$  = Transmission line resistance (ohms)

Given  $I_M$  and  $V_{MT}$  (from motor):

$$V_B = V_{MT} + I_M R_T$$

### BUSS LINE MATH MODEL



$I_M$  = Motor current (amps)

$I_G$  = Generator current (amps)

$V_B$  = Buss voltage

$V_{GT}$  = Generator terminal voltage

$R_B$  = Buss resistance

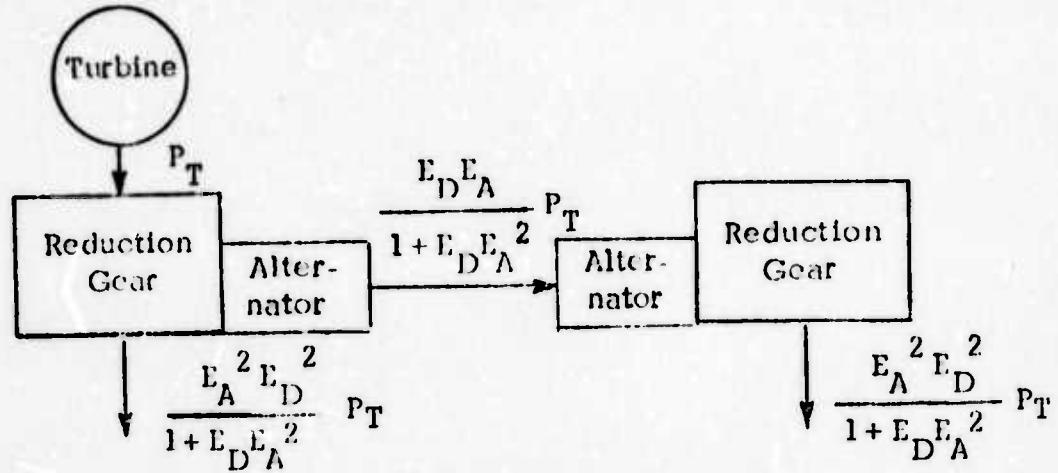
$N_T$  = No. of turbines operating

Given  $I_M$  and  $V_B$  (from transmission line):

$$I_G = \frac{2 I_M}{N_T}$$

$$V_{GT} = V_B + I_G R_B$$

Figure A-14



$$\text{Overall efficiency} = 2 \left( \frac{E_A^2 E_D^2}{1 + E_D E_A^2} \right)$$

Where:

$P_T$  = Turbine Shaft Power

$E_A$  = Alternator Efficiency

$E_D$  = Drive Efficiency

For  $E_A = 0.98$  and  $E_D = 0.96$ :

Power transferred =  $0.489 P_T$

Efficiency = 0.921

Figure A-15. Alternator Math Model

## APPENDIX B - SYSTEM COMPONENTS

This appendix contains details of the superconductive motors, generators and ancillary equipment used as a basis for electric drive performance in the study, as well as the alternator design used for the geared systems.

### B.1 MOTORS

The motor design used is based on a design developed at NSRDC, Annapolis, Maryland<sup>(1)</sup>; essential details are shown in figure B-1.

### B.2 MAIN GENERATORS

The 20,000 hp main generator design is also based on an NSRDC design<sup>(2)</sup> and is shown in figure B-2.

### B.3 CRUISE GENERATORS

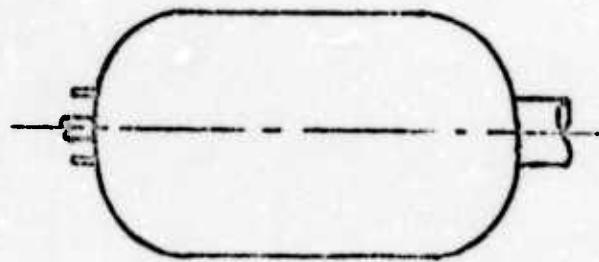
The 5,000 hp cruise generator is similar to a 5,000 hp, 15,000 rpm generator design developed at NSRDC. The generator was redesigned to operate at 7,200 rpm for use with the Garrett 990 gas turbine and machine losses and helium requirements were estimated using techniques

---

(1) T. J. Doyle, "Superconductive Propulsion Motor Development at NSRDC," Naval Ship Research and Development Center, Annapolis, Maryland, August, 1974.

(2) H.O. Stevens, "Superconductive Generation Development for Ship Electric Drive Systems," Naval Ship Research and Development Center, Annapolis, Maryland, August, 1974.

## 40,000 HP SUPERCONDUCTING MOTOR



### Design Point:

40,000 hp at 180 rpm  
(30,510 kw at 300 v)

### Size:

OD: 6.47 ft  
Length: 11.67 ft  
Volume: 384 ft<sup>3</sup>

### Weight:

Machine weight: 130,000 lbs  
Mount weight: 6,500 lbs  
Total weight: 136,500 lbs

### Performance at Design Point:

Power Input:	30,510	(40,915 hp)
Losses:	Ohmic	620.6 kw
	Brush Eddy Current	59.2 kw
	Brush Viscous Drag	0.4 kw
	Bearing, Seals and Windage	2.1 kw
		682 kw total (915 hp)
Power Output:	40,000 hp (29,828 kw)	
Current:	103,700 amps	
Voltage:	300 volts	Efficiency: 97.76%

### Helium Required:

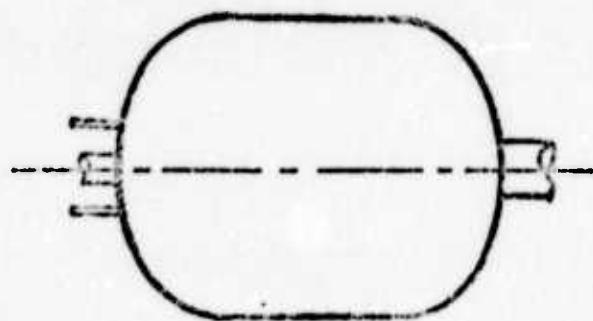
0.097 gm/sec at 4.5 K, 1.1 atmosphere

### Design Constants:

K <sub>M</sub> (Back emf):	1.6328 v/rpm
R <sub>M</sub> (Internal Resistance):	60 micro-ohm
K <sub>F</sub> (Friction Loss):	$6.481 \times 10^{-7}$ kw/(rpm) <sup>2</sup>
K <sub>E</sub> (Eddy Current Loss):	$1.827 \times 10^{-3}$ kw/(rpm) <sup>2</sup> (at full field)
K <sub>V</sub> (Viscous Loss):	$6.859 \times 10^{-9}$ kw/(rpm) <sup>3</sup>

Figure B-1

## 20,000 HP SUPERCONDUCTING MAIN GENERATOR



Design Point: 20,000 hp @ 3300 rpm  
(14,800 kw @ 300v)

<u>Size</u>	<u>Weight</u>
OD: 3.17 ft	Machine Weight: 10,000 lbs
Length: 4.17 ft	Mount Weight: 500 lbs
Volume: 32.8 ft	Total Weight: 10,500 lbs

### Performance at design point:

Power Input: 20,000 hp (14,914 kw)

Losses:	Ohmic:	27.3 kw
	Brush Eddy Current:	27.8 kw
	Brush Viscous Drag:	31.2 kw
	Bearings, Seals & Windage:	20.0 kw
		106 kw Total

Power Output: 14,808 kw

Current: 49,360 amps

Voltage: 300 volts Efficiency: 99.29%

Helium Required: 0.045 gm/sec at 4.5 K, 1.1 atmosphere

### Design Constant's:

$K_a$  (Back emf): 0.09111 volts/rpm

$R_a$  (Internal Resistance): 11.2 micro-ohms

(Friction Loss):  $1.8365 \times 10^{-6}$  kw/(rpm)<sup>2</sup>

$K_e$  (Eddy Current Loss):  $2.553 \times 10^{-6}$  kw/(rpm)<sup>2</sup> (At full field)

$K_v$  (Viscous Loss):  $8.682 \times 10^{-10}$  kw/(rpm)<sup>3</sup>

Figure B-2

similar to those used at NSRDC<sup>(1)</sup>. The final design is shown in figure B-3.

#### B.4 AC-DC GENERATOR

Garrett Airesearch Manufacturing Company has proposed a non-superconducting 5,000 hp ac-dc generator for use with the Garrett 990 turbine<sup>(2)</sup>. This generator develops the dc power required by the superconducting motors by generating ac power which is then rectified to dc by a bank of 120 diodes. The machine is less efficient than the superconducting cruise generator (96.5% against 99.2%) and weighs about 1-1/2 times as much. It has the advantages of not requiring liquid helium cooling and an ability for rapid changes in field excitation (very rapid field changes are not possible in the superconducting machine because of magnet and inductance limitations). The use of the ac-dc generator as a substitute for the superconducting generator is discussed in the text. Figure B-4 gives the essential design details.

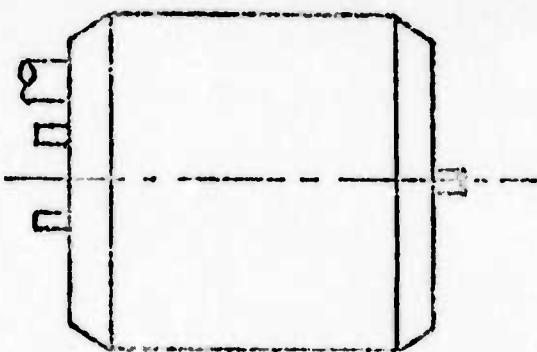
#### B.5 ALTERNATOR

The alternator used as a basis for the geared drive cross-over systems is also based on Airesearch designs developed for NAVSHIPS. It is, essentially, the ac-dc generator design without

(1) T.J. Doyle and M.J. Cannell, "Development of the Shaped Field Superconductive Motor," Naval Ship Research and Development Center, Bethesda, Maryland, Report No. 4178, January 1974.

(2) Work performed under the auspices of the U.S. Navy Naval Ships System Command under Contract No. N0024-73-C-5487.

## 5,000 HP SUPERCONDUCTING CRUISE GENERATOR



### Design Point:

5,000 hp @ 7,200 rpm  
(3,700 kw @ 150 v)

### Size:

OD: 2.33 ft  
Length: 2.33 ft  
Volume: 10.0 ft<sup>3</sup>

### Weight

Machine weight: 3,500 lbs  
Mount weight: 350 lbs  
Total weight: 3,850 lbs

### Performance at Design Point:

Power Input: 5,000 hp (3,728 kw)

Losses: Ohmic	14.6 kw
Brush Eddy Current	3.0 kw
Brush Viscous Drag	1.8 kw
Bearings, Seals and Windage	9.0 kw
	28 kw total

Power Output: 3,700 kw

Current: 24,640 amps

Voltage: 150 volts Efficiency: 99.24%

### Helium Required:

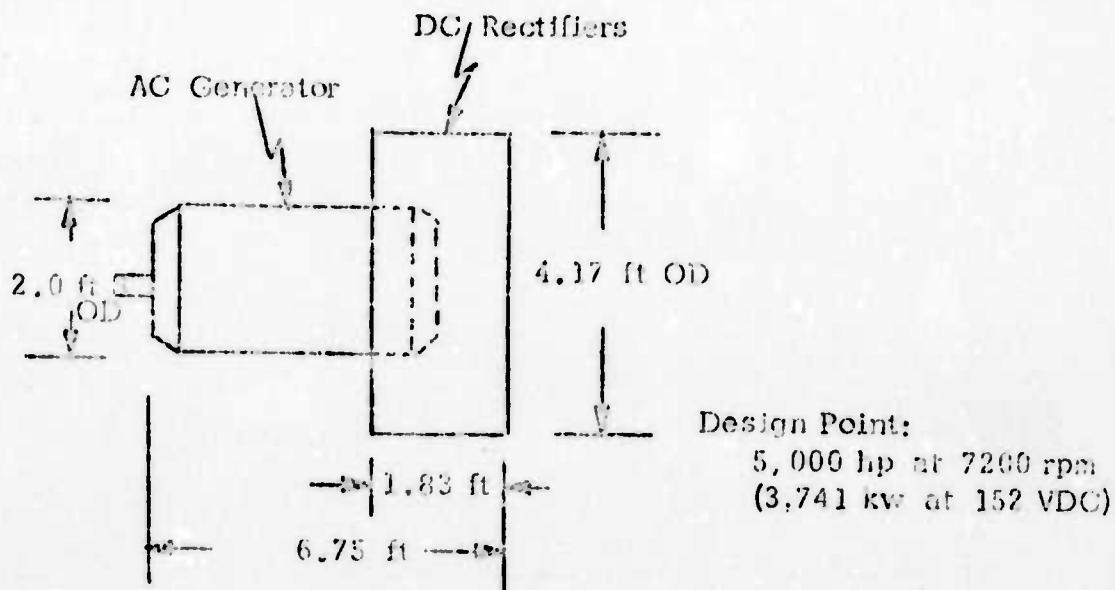
0.051 gm/sec at 4.5° K, 1.1 atmosphere

### Design Constants:

$K_b$ (Back emf):	0.0209 volts/rpm
$R_G$ (internal resistance):	24 micro-ohms
$E_f$ (Friction Loss):	$0.3736 \times 10^{-6}$ kw/(rpm) <sup>2</sup>
$E_j$ (Eddy Current Loss):	$0.0579 \times 10^{-6}$ kw/(rpm) <sup>2</sup> (at full filed)
$E_v$ (Viscous Loss):	$4.8225 \times 10^{-12}$ kw/(rpm) <sup>3</sup>

Figure B-3

## 5,000 HP AC-DC GENERATOR



### Size

See sketch  
Volume:  $28 \text{ ft}^3$  ( $41 \text{ ft}^3$  envelope)

### Weight

Machine weight: 5,570 lbs  
Mount weight: 500 lbs  
Total weight: 6,070 lbs

### Performance at Design Point:

Power Input:	5,000 hp (3,738 kw)
Losses: Ohmic (ac)	80.3 kw
Friction and windage	7.1 kw
Ohmic (rectifiers)	11.8 kw
	129 kw

Power Output:	3,599 kw
Current:	23,650 amps-de
Voltage:	152 volts-de
	Efficiency: 96.5%
Note:	ac efficiency (without rectifiers) = 97.6%

Figure B-4

rectifiers. Under the contract previously cited, three designs were developed with the following characteristics for the ac portion of the machines:

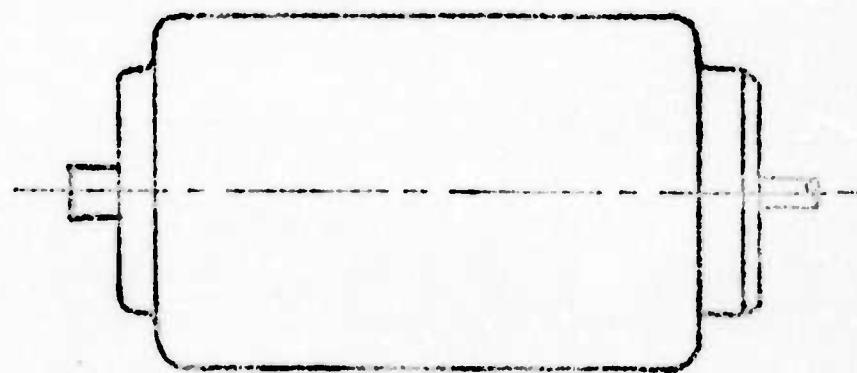
<u>Power</u>	<u>OD</u>	<u>Length</u>	<u>Weight</u>	<u>Speed</u>	<u>ac Efficiency</u>
3,000 hp	18"	43"	1,900 lbs	10,000 rpm	97.2%
5,000 hp	24"	61"	4,950 lbs	7,200 rpm	97.6%
20,000 hp	50"	84"	19,600 lbs	3,600 rpm	98.4%

The crossover alternator for this application must be capable of handling 10,000 hp when either one or three main turbines are used to power the two propeller shafts. The design data for the three machines above was extrapolated to arrive at the following specifications for the required alternator:

<u>Power</u>	<u>OD</u>	<u>Length</u>	<u>Weight</u>	<u>Speed</u>	<u>ac Efficiency</u>
10,000 hp	36"	72"	10,000 lbs	5,000 rpm	98.0%

The 98% efficiency is considered a conservative estimate in view of the fact that the original designs were constrained by the necessity of limiting voltages because of the rectifier bank in the ac-dc version; with those limitations removed, efficiency greater than 98% should be possible. The 98% value was used in the study and a value of 96% efficiency was used for a pair of alternators for crossover. Essential details of the alternator are shown in figure B-5.

## 10,000 HP AC ALTERNATOR



### Design Point:

10,000 hp at 5,000 rpm  
(7,450 kw @ 4,160 vac)

### Size:

CD: 3.0 ft  
Length: 6.0 ft  
Volume: 42.4 ft<sup>3</sup>

### Weight:

Machine weight: 10,000 lbs  
Mount weight: 1,000 lbs  
Total weight: 11,000 lbs

### Performance at Design Point:

Power input:	10,000 hp (7457 kw)
Losses:	149 kw (est.)
Power output:	7,308 kw (5,416 kva)
Current:	2,029 amperes
Voltage:	4,160 volts
	Efficiency: 96.9%

Figure B-5

## B.6 TRANSMISSION LINES

Varying the transmission line resistances vs. performance over the mission profile provided the following relationship for the baseline configuration:

Fuel consumed due to line resistances (in lbs/hr),

$$W_F = 0.76 R_T + 0.98 R_{MG} + 0.22 R_C \quad (\text{Main Turbines only})$$

$$= 0.69 R_T + 0.80 R_{MG} + 0.20 R_C + 0.14 R_{CG} \quad (\text{Main + Cruise Turbines})$$

Where:

$R_T$  = Motor transmission line resistance

$R_{MG}$  = Main generator buss line resistance

$R_{CG}$  = Cruise generator buss line resistance

$R_C$  = Crossover line resistance

(All in micro-ohms)

Taking the transmission lines as coaxial aluminum tubes with integral fluid cooling tubes, the cross-sectional area required for the aluminum and the cooling tubes is:

$$\text{Aluminum: } 53.76 \frac{L}{R} \text{ (in}^2\text{)}$$

$$\text{Coolant: } 2.663 \times 10^{-11} I^2 R \text{ (in}^2\text{)}$$

Where:

L = Length (ft)

R = Resistance (micro-ohms)

I = Maximum design current (amps)

An additional 20% is allowed for coolant pipe and insulation thickness.

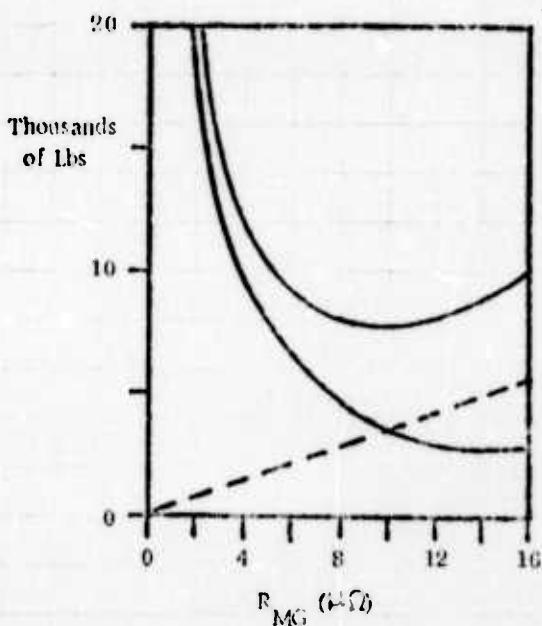
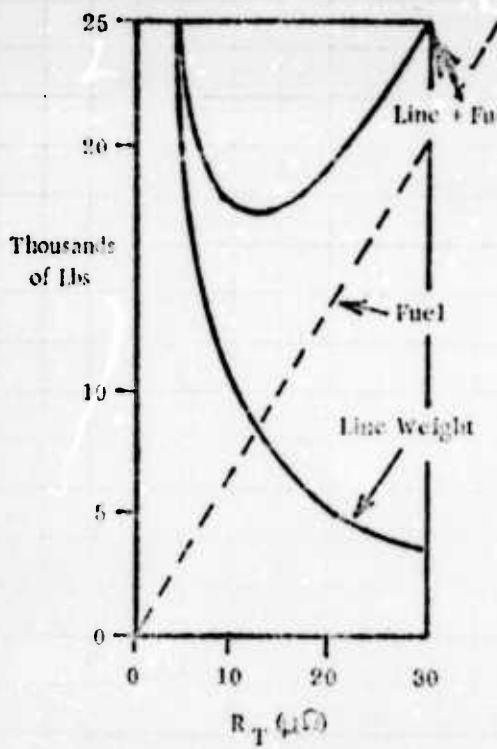
The total weight of the transmission line is:

$$W_L = \frac{43.56}{R} \cdot I^2 + 1.385 \times 10^{-11} I^2 R \cdot L \text{ (lbs)}$$

A trade-off thus occurs between the transmission line weights and the weight of fuel consumed, as shown in figure - B-6.

The transmission line weights were optimized against the amount of fuel burned in 500 hours with the following results:

- Baseline configuration
  - .. Motor transmission lines(2): 17  $\mu\Omega$ , 32' long, 3000 lbs each.
  - .. Main generator bus lines: 9  $\mu\Omega$  each, 55' total, 4190 lbs total.
  - .. Fwd cruise generator line: 80  $\mu\Omega$ , 82', 4000 lbs.
  - .. Aft cruise generator line: 72  $\mu\Omega$ , 52', 1910 lbs.
  - .. Crossover line: 110  $\mu\Omega$ , 157', 11260 lbs.
- Reconfigured Engine Room Version
  - .. Motor transmission lines(2): 62  $\mu\Omega$  each; fwd. line 137', 16100 lbs; aft line 44'; 1899 lbs.
  - .. Main generator bus lines: 10  $\mu\Omega$ , 72' total, 5600 lbs total.
  - .. Fwd cruise generator line: 97  $\mu\Omega$ , 98', 5000 lbs.
  - .. Aft cruise generator line: 100  $\mu\Omega$ , 71', 2630 lbs.
  - .. Crossover line: 27  $\mu\Omega$ , 41', 3080 lbs.



NOTE: All Fuel Weights  
are for 500 Hrs  
of Operation

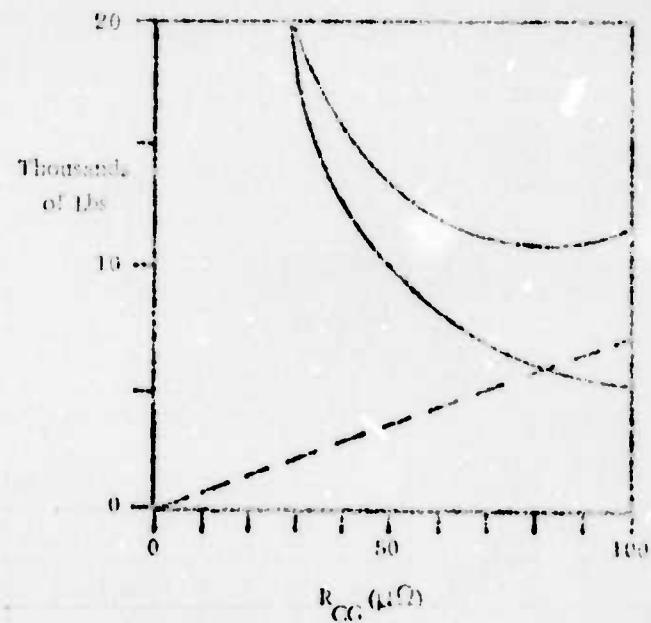
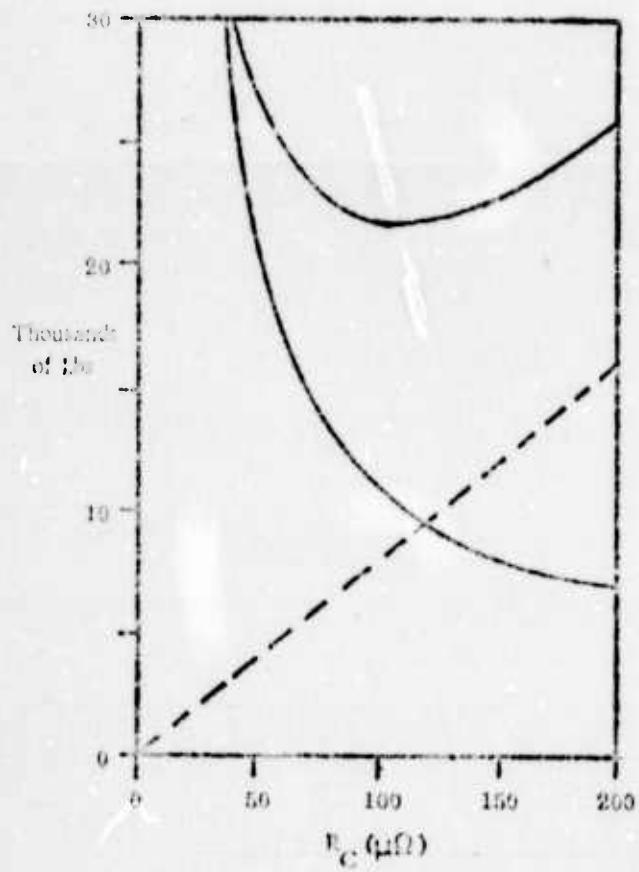


Figure B-6. Line and Fuel Rates vs. Resistances

The actual configurations are shown in figure B-7. As may be seen, the total resistance between motors and generators differs for each combination selected. In order to simplify analysis, a set of equivalent resistances were computed which would give the same ohmic ( $I^2R$ ) loss as the actual physical configuration, but which would permit a single motor transmission line resistance to be used between the motors and a common buss point. Each generator is then considered to be connected to this common point with a resistance which is the same as that for each of the other generators.

The resultant values are <sup>(1)</sup>:

<u>Baseline Configuration</u>	<u>Reconfigured Engine Room</u>
$R_T = 17$	55
$R_1 = 94.3$	98.7
$R_2 = 77.6$	107
$R_3 = 39.6$	8.72
$R_4 = 9.6$	17.0
$R_5 = 18.0$	3.59
$R_6 = 9.6$	17.0

where:

$R_T$  is resistance between motor and buss point

$R_1$  is for 1 engine/turbine

$R_2$  is for 2 engine turbines

$R_3$  is for 1 main turbine

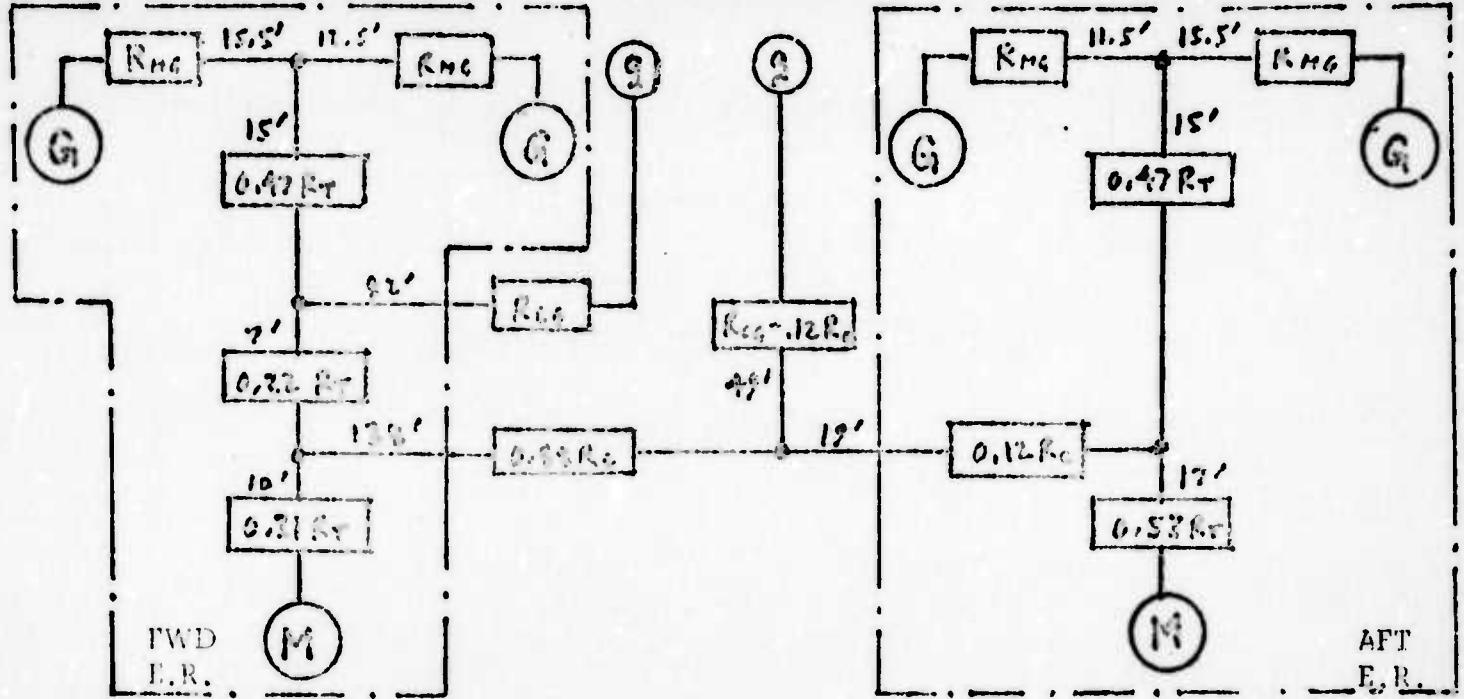
$R_4$  is for 2 main turbines

$R_5$  is for 3 main turbines

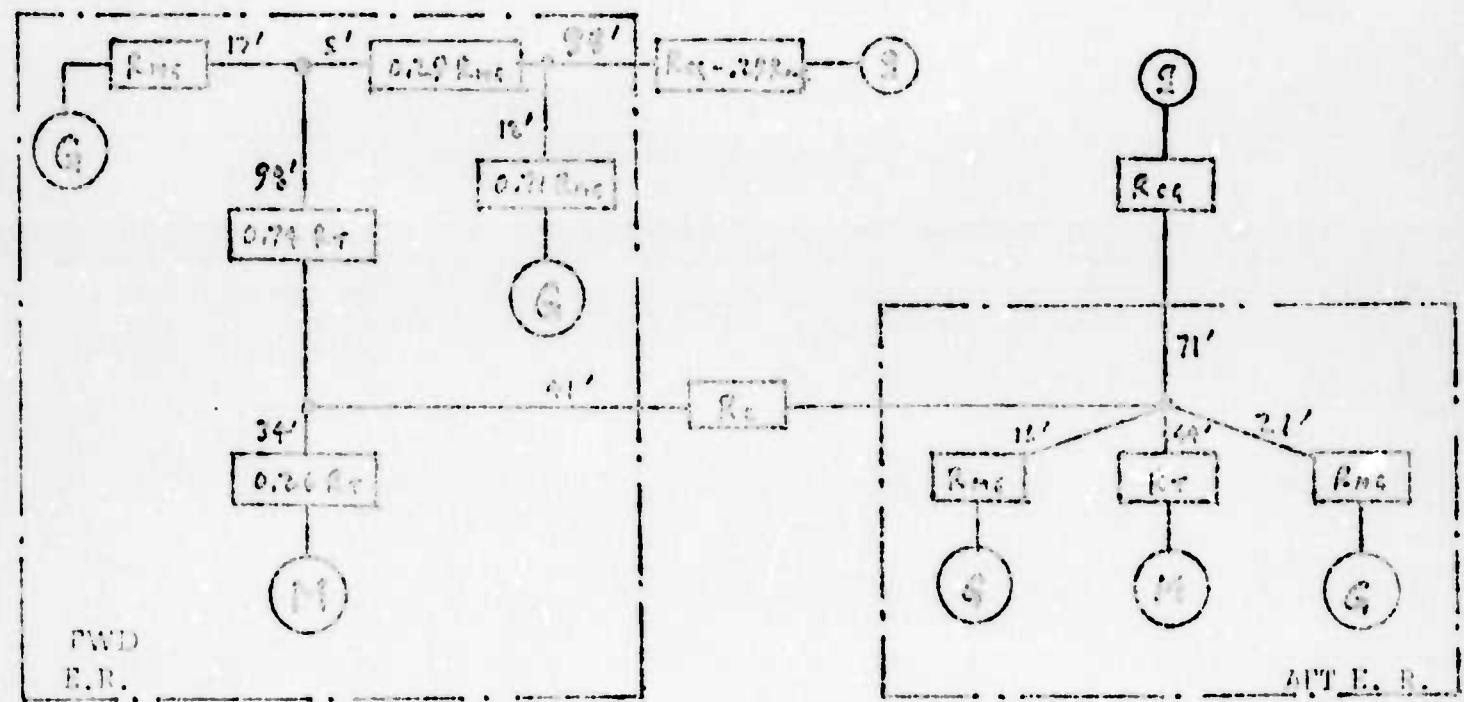
$R_6$  is for 4 main turbines

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(1) All values in micro-ohms.



Existing Engine Room



Reconfigured Engine Room

G - Cruise Turbine

G - Main Turbine

M - Motor

Figure B-7. Transmission Line Configurations

For cruise turbines located in the engine rooms, instead of topside, the transmission lines were assumed to be 20 ft/ long with a resistance of 27 micro-ohms each and a weight of 1500 lbs. for the pair. The values for  $R_T$  and  $R_3$  through  $R_6$  remain the same as for the reconfigured engine room case;  $R_1$  and  $R_2$  become:

$$R_1 = 18.72 \mu\Omega$$

$$R_2 = 27.00 \mu\Omega$$

## B.7 HELIUM COMPRESSORS

Based on the estimated motor and generator helium losses, the amount of compressor power required for each was estimated as follows:

<u>Machine</u>	<u>Helium Loss</u>	<u>Carnot Power Required to Reliquify</u>	<u>Compressor Power Required</u>
Motor	0.097 gm/sec	0.694 Kw	22.8 Kw
Main Generator	0.045 gm/sec	0.222 Kw	12.8 Kw
Cruise Generator	0.046 gm/sec	0.329 Kw	13.0 Kw

Assuming one compressor per engine room, the total compressor power required is:

Main Turbines Only: 48.4 Kw

Main + Cruise Turbines: 61.4 Kw

The compressor sizes required for these outputs were estimated at:

	<u>Main Turbines Only</u>	<u>Main + Cruise Turbines</u>
Maximum Power	50 Kw	65 Kw
Volume	33 ft <sup>3</sup>	43 ft <sup>3</sup>
Weight	2500 lbs	3250 lbs
Length	7 ft	7 ft
Diameter	2.5 ft	2.8 ft

## B.8 HELIUM CRYOSECTIONS

Helium cryosections are mounted adjacent to each superconducting machine and form the final refrigeration (expansion) stage. All cryosections were kept the same size for commonality, being sized to handle a maximum

load of 0.10 gm/sec of helium. Two cryosections are used per motor to facilitate rapid cooldown and to provide redundancy in case of failure. The generators have one cryosection each which normally operate at half capacity except during initial cooldown. Each cryosection is 2.0 ft. in diameter by 5.0 ft. long and weights 933 lbs.

#### B.9 HELIUM CRYOLINES

The cryogenic transfer lines between the compressors and cryosection were designed to handle the maximum load, based on the number of cryosections used. Line sizes and weights required are as follows:

<u>Number of Cryosections</u>	<u>Line OD</u>	<u>Weight (lbs/ft)</u>
1	2.0"	2.28
2	2.9"	4.56
3	3.5"	6.84
4	4.1"	9.12
5	4.6"	11.40

The total length of lines and total weight for each configuration is:

	<u>Baseline Configuration</u>	<u>Reconfigured Engine Room</u>
Fwd. Engine Room	46 ft; 232 lbs	140 ft; 752 lbs
Fwd. Cruise Turbine	80 ft; 184 lbs	70 ft; 175 lbs
Aft Engine Room	56 ft; 243 lbs	54 ft; 322 lbs
Aft Cruise Turbine	60 ft; 138 lbs	60 ft; 150 lbs

## B.10 SWITCHGEAR

Based on designs developed at RSRDC, Annapolis, the sizes and weights for electrical switches required were estimated as follows:

<u>For Use With</u>	<u>Size</u>	<u>Weight</u>
Cruise Generator	15" x 21" x 5"	85 lbs each
Main Generator	21" x 30" x 7"	275 lbs each
Crossover Line	17" x 26" x 5"	135 lbs each

The switches have been designed to handle the maximum currents + transients which occur in each application and serve to connect and disconnect the generators from the buss line, reverse generator polarities and to open and close the crossover line. In addition to the switches, rheostats are required so that voltages can be matched when bringing generators on and off line, when switching in crossover and when reversing the motors. The rheostats required were estimated as follows:

<u>For Use With</u>	<u>Size</u>	<u>Weight</u>
Cruise Generator	29" x 20" x 24"	740 lbs
Main Generator	40" x 40" x 48"	4000 lbs
Crossover Line	29" x 26" x 24"	770 lbs

For each application, four switches and one rheostat are required in order to provide forward/reverse polarities and disconnect. The total switchgear units resulting are packaged as follows:

<u>For Use With</u>	<u>Size</u>	<u>Weight</u>
Cruise Generator	24" x 30" x 41"	1100 lbs each
Main Generator	40" x 48" x 70"	5100 lbs each
Crossover Line	24" x 32" x 46"	1300 lbs each

## B.11 ESTIMATE OF SHIPS SERVICE POWER

Based on trends in electric power capacity aboard DD class vessels as follows:<sup>(1)</sup>

<u>Year</u>	<u>Kw Power</u>
1945	1,000
1955	2,000
1975	6,000

an installed capacity of 6,000 Kw was assumed. A steady load of 4,000 Kw was then assumed for assessing impact on ship's range (parametric variations in the study allow adjustment for changes in this power level).

A level of 4,000 Kw can be provided by one nominally 5000 hp turbine operating at near full load; fuel load would be 2700 lbs/hr. If a second, standby, turbine is assumed to be operating at all times at an idle fuel load of 360 lbs/hr, the total fuel load is 3060 lbs/hr for 4000 kw output, or 0.77 lb/Kw-hr. Based on this, the ships auxiliary generator fuel rate was assumed to be 0.8 lb/Kw-hr.

<sup>(1)</sup> G. Graham, "Factors Affecting Naval Ship Design", Naval Engineers Journal, February, 1972, p.85.

## APPENDIX C - COMPUTER STUDIES

### C.1 GENERAL

This appendix contains a general discussion of the computer program utilized for analysis of the various propulsion configurations over the mission profile and output data sheets for the most important cases.

Math models for the turbines, propellers, drag, electric motors and generators and electrical transmission lines which were incorporated into the computer program are detailed in Appendix A.

Electric drive system losses were analyzed based on the motor, generator and transmission line models. Gated drives were analyzed by assuming a fixed gear efficiency for the main reduction gears and shafting losses<sup>(1)</sup> and a fixed efficiency for the crossover alternators<sup>(2)</sup> and turbine horsepower required at each speed was obtained by dividing shaft horsepower by the efficiency.

Cooling loads were computed based on an estimated 0.02 kw of ship service load per hp lost in the transmission system and 0.8 lbs/kwh was used as the ship service auxiliary generator fuel rate. For the electrical

<sup>(1)</sup> 0.960 efficiency was used in the study.

<sup>(2)</sup> 0.980 efficiency per alternator, or 0.960 for the pair was used.

systems, 1 kw of power was added for each generator in use for lubrication pump power (motor lubrication was assumed to be an equal trade-off for the main reduction gear lube load). Constant helium compressor powers were used through the electrical drive missions<sup>(1)</sup>.

<sup>(1)</sup> 100 kw for main turbines only; 130 kw for main and cruise turbine configurations.

## C.2 COMPUTER PROGRAM

The math model computer program consists of a main program and four subprograms:

- . PITCH
- . GENM
- . MISSN
- . ROUND

The function of each is as follows:

### MAIN Program

- . Reads calculation limits and performance (speed and configuration) requirements.
- . Obtains fuel rate from PITCH for given pitch ratio.
- . Optimizes pitch, if pitch is not fixed, by a search procedure; fuel rate is obtained from PITCH for each pitch ratio until minimum fuel is obtained. Four different search procedures are utilized:
  - .. Fibonacci search for minimum fuel (used for electric drive).
  - .. Interval search for minimum fuel (used for geared drive.)
  - .. Interval search for fuel rate equal to turbine idle rate (used for geared drive under low power condition).
  - .. Pitch is fixed for electric drives when fuel rate drops below the idle rate.

- . Increases number of turbines when the fuel rate exceeds the maximum allowed with the existing configuration.
- . When cruise turbines are used, compares results for main turbines and uses the most efficient.
- . Calculates and prints final results for each speed.
- . Passes final result for each speed to MISSN and calls for summary when last speed is reached (last speed for which turbine configuration specified can attain results within allowed fuel and turbine speed limitations).
- . Reads new performance requirements when summary is complete.
- . Reads in new or changed specification data (gear ratios, electric constants, etc.) when called for.

#### PITCH Subprogram

- . Reads propeller and drag constants.
- . For geared drive, reads gear ratios, efficiencies and turbine constants.
- . For electric drive, reads motor constants and transmission line resistances.
- . Computes drag, propeller and turbine characteristics.
- . Computes turbine fuel when supplied with propeller pitch from MAIN (calculated directly for geared drive; for electric drive,

motor/propeller speed and torque are computed, voltages and currents are computed and required generator voltage and current are passed to GENM, which returns fuel rate).

GENM Subprogram (used for electric drive only)

- Reads generator and turbine constants.
- Computes turbine idle characteristics.
- Computes fuel rate when supplied with generator voltage and current.
  - .. If magnet field is not fixed, the optimum turbine speed is computed and the field is adjusted to match this field.
  - .. if the field is fixed, the corresponding speed and fuel rate are computed.
  - .. If fuel drops below the minimum turbine (idle) fuel rate, the magnet field is reduced until fuel rate equals idle unless no field change is allowed.
- "Flags" the result if maximum turbine speed is exceeded or fuel rate is above or below the allowable fuel rate.

MISSN Subprogram

- Reads mission profile (percent time at each speed).
- Receives ship speed, turbine configuration, propeller speed, horsepower (turbine, shaft and effective), pitch ratio, effective

gear ratio, turbine fuel rate, turbine figure of merit, refrigeration load and lubrication load from PITCH.

- Selects values corresponding to smallest fuel rate when more than two sets of data are received at the same speed.
- Computes miles/ton of turbine fuel, and, per thousand hours: miles, tons of fuel and total propulsion system (turbines plus electric system load) tons/mile. Prints results for each speed.
- Computes and prints average results over mission profile.
- Calls ROUND to round results to specified accuracy before printing.

#### ROUND Subprogram

- Rounds data to accuracy called for in input. For example, if 4-place accuracy is specified, 35693.1 becomes 35690.0; 21.2195 becomes 21.2200, etc.

#### Program Variables

The program has the following variables as inputs, independent of the specific configuration being investigated:

#### Overall Limits

- Required accuracy in fuel rate.
- Required accuracy in P/D ratio.
- Number of iterations allowed in search for minimum fuel.
- Maximum allowable P/D ratio.

### Drag Calculations

- . 3 Drag coefficients ( $C_{D0}$ ,  $V_X$  and  $C_2$ )

### Propellers

- . Propeller diameter
- . Water density
- . 6 thrust coefficients ( $T_{01}$ ,  $T_{02}$ , etc.)
- . 7 torque coefficients ( $Q_{01}$ ,  $Q_{02}$ , etc.)

### Turbines (Main and Cruise)

- . 4 Turbine fuel constants ( $w_1$ ,  $w_2$ ,  $w_3$  and  $w_4$ ).
- . Minimum fuel rates.
- . Maximum fuel rates.
- . Maximum rpms.

### Geared Drive

- . Main gear ratio
- . Cruise gear ratio
- . Gear efficiency
- . Alternator efficiency

### Electric Drive

- . Refrigeration power requirements
- . Lubrication power requirements
- . Magnet field (fixed or variable)

- . 5 Motor constants ( $K_{FM}$ ,  $K_{EM}$ ,  $K_{VM}$ ,  $K_M$  and  $R_M$ )
- . 5 Generator constants ( $K_{FG}$ ,  $K_{EG}$ ,  $K_{VG}$ ,  $K_G$  and  $R_G$ )  
(both cruise and main)
- . 7 Resistances ( $R_T$  and  $R_{B1}$  -  $R_{B6}$ )

Mission Profile

- . Percent time at each speed

For each configuration run, the following variables are input:

Speed

- . Minimum speed.
- . Maximum speed.
- . Increments in speed (between minimum and maximum speeds specified).
- . Minimum number of turbines and type.
- . Maximum number of turbines and type.
- . Odd number of turbines allowed or not allowed (i.e., crossover or no crossover).
- . P/D ratio (fixed or variable).
- . Percent magnet field (fixed or variable) (electric drive only).
- . Number of digits accuracy desired in final printout.
- . Magnet field adjustment allowed or not allowed (electric drive only).

In addition:

- . A punch card record of results for each speed may be called for.<sup>(1)</sup>
- . Step-by-step details of each search procedure may be called for.
- . The search calculation made may be changed (between Fibonacci and interval search).

---

(1) Cards may be used as input to an existing mission analysis program which gives details of performance of each system component at each speed and may be run over different mission profiles.

### C.3 COMPUTER RESULTS

This section contains results of the computer runs for various configurations and variations.

Included are:

- . Program constants used for the geared drive systems (Ref. No. 10).
- . Program constants used for the electric drive systems (baseline configuration, ref. no. 1; reconfigured engine room, ref. no. 2 and optimum configuration<sup>(1)</sup>, ref. no. 3).
- . Propeller performance, ship drag and mission profile.
- . Mission profile summaries<sup>(2)</sup> for the baseline, baseline + alternators, baseline + cruise turbines and baseline + alternators and cruise turbines configurations.
- . Mission profile summaries for the electric drive systems (baseline configuration, reconfigured engine room for the systems with and without cruise turbines and optimum configuration for the system with cruise turbines).

---

(1) Cruise turbines moved to engine room.

(2) "RANGE" is the range based on turbine fuel rate only; "TONS OF FUEL AND TONS PER MILE" include the impact of cooling, lube system and helium compressor loads. "SPEED RATIO" is the ratio of turbine speed to propeller rpms. "REF. NO." refers to the program constants.

- Mission Profile Summaries for the geared and electric configurations with variable (fully optimized) pitches.
- Mission Profile Summaries for the electric drive baseline configurations with the generator fields fixed (at 90%), fixed to the nearest 10% and fixed at "optimum" settings.<sup>(1)</sup>
- Mission Profile Summaries for each turbine (1 cruise, 2 cruise, 1 main, etc.) for the baseline configuration electric drive; included for these summaries is a second page for each giving details of propeller, turbine and drive efficiencies, percent magnet field, voltages and currents.

---

(1) 90% for cruise turbines  
60% for one main turbine  
75% for two main turbines  
90% for three and four main turbines

INTERFERED DISTANCE PER POSITIONING

LONG LAT POSITION COORDINATE SYSTEMS AND LATITUDE LONGITUDE

FUEL RATE 0.0030 CUBIC FEET PER HOUR FUEL RATE TO WEIGHT 0.0030 CUBIC FEET IN THE 5/0 PART

WEIGHT MAXIMUM 10000 POUNDS CHARGE BY LBS/HR 0.0100 LBS/HOUR

THE PROBLEMS IS SIMPLIFIED IF WE TAKE THAT THE VOLUME OF SPARES ARE ENOUGH

REACTIVE CONSTANTS

MAIN REACTOR POWER 70000 KW/HOUR

TRUST COFFEE PRICE/KG 1.0000

TRUST COFFEE PRICE/KG 1.0000

TRUST COFFEE PRICE/KG 1.0000

WEAK REACTOR POWER 10000 KW/HOUR



## ELECTRIC DRIVE ID NUMBER

MAIN CONSTANTS		TRANSMISSION CONSTANTS		TURBINE CONSTANTS		REF. NO. 32	
KF=	0.64810E-04	PT=	0.5500E-04				
KP4E=	0.18070E-02	R111=	0.56720E-04	A1(2)=	0.19700E-03		
KV4=	0.58550E-03	R112=	0.56720E-04	A1(3)=	0.17000E-04		
KV=	0.16328E-01	R113=	0.56720E-04	K1(1)=	0.17000E-04		
RM=	0.60000E-04			K1(2)=	0.17000E-04		

VALUES GIVEN BELOW ARE FOR 100 PERCENT GENERATOR FIELD

MAIN GENERATOR CONSTANTS..KF=0.19350E-03		TURBINE CONSTANTS..A1(1)=5600.000	
KF=	0.25530E-03	A2=	1.000
PT=	0.56720E-04	A3=	0.143
R111=	0.56720E-04	A4=	0.1143E-02
R112=	0.56720E-04	WMIN=	1100.0 PPH
R113=	0.56720E-04	WSMAX=	6400.0 PPH
		SMAX=	3600.0
TURBINE POWER=	16.49 HP AT 1.72.51 RPM		
INLET FUEL=	1100.00 RPM		
MAX POWER=	27324.06 HP AT 52.545 RPM (2.622 HP/LA/MIN)		

VALUES GIVEN BELOW ARE FOR 100 PERCENT GENERATOR FIELD

CRUISE GENERATOR CONSTANTS..KF=0.17360E-03		TURBINE CONSTANTS..A1(1)=750.000	
KF=	0.57500E-07	A2=	0.263
KV=	0.45225E-11	A3=	3.350
KV=	0.23500E-04	A4=	0.1000E-03
RG=	0.24300E-04	WMIN=	300.0 PPH
		WSMAX=	2740.0 PPH
WATER POWER=	4.05 WAT 1.502-45 RPM	SMAX=	7200.0
INLET FUEL=	360.00 RPM		
MAX POWER=	5715.50 HP AT 7235.21 RPM (2.117 HP/LA/MIN)		

SPECIFICATION POWER= 100.00 KW FOR MAIN GENERATORS JUNY AND 130.00 KW FOR MAIN + CRUISE GENERATORS  
 INLET FUEL= 1.00 KW PER GENERATOR

CRUISE COEFFICIENTS...CD0=1.4000 Vx=21.00 C2=0.0000

WATER DENSITY=1.0000

PROPELLER DIAMETER=17.50

THRUST COEFFICIENTS...

TR1= 0.0500 TR2= 1.0130 T03= 0.0060  
TR1=-0.2600 TR2= 1.0000 T43=-0.1500

THRUST COEFFICIENTS...

TR1= 0.4550 CD2= 0.5470 C02= 0.1577  
Cv1= 0.1530 Cv2= 0.1633 C13= 1.0160 RA=1.4220

**MAIN CONSTANTS**

KEN = 0.5-810E-02	TRANSMISSION CONSTANTS
KEM = 0.1-6270E-02	RTE = 0.390E-10
KVM = 0.68590E-07	K(1) = 0.16720E-20
KVR = 0.16326E-01	K(2) = 0.87250E-20
KME = 0.50000E-02	K(3) = 0.45450E-20
KVE = 0.27000E-02	K(4) = 0.17000E-20

VALUES GIVEN BELOW ARE FOR 100 PERCENT GENERATOR FIELD

**MAIN GENERATOR CONSTANTS**.. $K_1=0.17309E-015$     **TOURINE CONSTANTS**.. $\alpha=66.9-000$

$K_2=0.75930E-025$	$n_2=1.050$
$K_3=0.24572E-019$	$n_3=0.143$
$K_4=0.11430E-014$	$n_4=0.1143E-02$
$K_{ME}=0.11200E-017$	$\alpha_{ME}=1.050-0$
$K_{VE}=0.20000E-02$	$\alpha_{VE}=0.923-0$
$K_{VM}=0.50000E-02$	$\alpha_{VM}=0.023-0$

**TOURINE POWER** = 16.49 KW AT 1472.91 RPM  
**TOURINE FRICTION** = 1160.00 NPM ... 154.18 VOLTS AT TERMINALS  
**MAX POWER** = 22024.56 KW AT 3245.46 RPM ( 2.672 MP/RB/4R )

VALUES GIVEN BELOW ARE FOR 100 PERCENT GENERATOR FIELD

**CRUISE GENERATOR CONSTANTS**.. $K_1=0.17309E-015$     **TOURINE CONSTANTS**.. $\alpha=720-000$

$K_2=0.37800E-017$	$n_2=0.360$
$K_3=0.11430E-014$	$n_3=0.1143E-02$
$K_4=0.11200E-017$	$n_4=0.11200E-02$
$K_{ME}=0.11200E-017$	$\alpha_{ME}=0.923-0$
$K_{VE}=0.20000E-02$	$\alpha_{VE}=0.023-0$
$K_{VM}=0.50000E-02$	$\alpha_{VM}=0.023-0$

**TOURINE POWER** = 2.704 KW AT 3502.05 RPM  
**TOURINE FRICTION** = 360.00 NPM ... 73.20 VOLTS AT TERMINALS  
**MAX POWER** = 5715.50 KW AT 7256.21 RPM ( 2.617 MP/LB/R )

AT OPERATING POINT POWER = 150.00 KW FOR MAIN GENERATORS AND 130.00 KW FOR MAIN + CRUISE GENERATORS

**TOURINE POWER** = 1.00 KW PER GENERATOR  
**MAIN COEFFICIENTS**... $G_1=1.4000$      $K=27.00$      $\alpha=2.0000$   
**WATER DENSITY** = 1.9905  
**PROPELLER DIAMETER** = 17.00

**TOURINE COEFFICIENTS**...  
 $T_{11} = 0.0500$      $T_{12} = 1.0170$      $T_{13} = 0.0260$   
 $T_{21} = 0.2600$      $T_{22} = 1.0500$      $T_{23} = 0.1600$

**TOURINE COEFFICIENTS**...  
 $G_{11} = 0.4550$      $G_{12} = 0.5470$      $G_{13} = 0.1577$   
 $G_{21} = 0.1330$      $G_{22} = 0.1631$      $G_{23} = 1.5160$      $K_{12} = 1.4250$



SCHLESINGER - ARTHUR B. 1886-1955

C-17

پاکستانی ملکہ نویں ملکہ نویں

卷之三

AVERAGE ELECTRICAL LOAD	TOTAL LOAD	W.H.
PROPULSION COOLING...	0.	KW
GENERATOR LUBE SYSTEM	0.	KW
BELT CONVEYOR SYSTEMS...	0.	KW
		W.H.

ארכיאולוגיה של ירושלים (1993)

卷之三

**TOTAL** 1,212 162 12,518 (42)

CONSTITUTION OF THE UNITED STATES - ARTICLE I, SECTION 8, CLAUSE 3

卷之三

PER THOUSAND HORSES		NO. OF TURBINES		TONS PER MILE		NETT FUEL		TONS FUEL		CRUISE	
KTRS	H.P.	SHFT	RPM	SPEED	HP	45	45	MILES	MILES	CRUISE	CRUISE
1	1-10	6-286	31-10	74-63	1-43	135.30	140.70	720.	3-111	3-54	0-371
2	1-20	6-371	34-52	74-50	11-23	119.20	126.20	720.	6-222	2-86	C-161
3	1-20	6-542	35-29	54-50	17-32	115.20	120.20	720.	9-353	3-66	0-107
4	1-20	6-504	76-59	74-50	35-20	152.10	144.30	720.	12-444	3-36	0-090
5	1-20	1-250	25-55	74-50	17-50	21-82	21-70	607.	13-830	4-32	0-572
6	1-20	1-250	34-27	74-50	17-50	322.40	414.40	643.	14-220	5-05	0-573
7	1-20	1-250	40-61	74-50	460.20	460.60	1105.	14-190	5-92	0-574	
8	1-20	1-250	45-72	74-50	716.60	932.60	1295.	13-560	6-94	0-572	
9	1-20	1-250	51-64	74-50	1021.00	1427.00	1516.	13-303	6-13	0-575	
10	1-20	1-250	57-19	74-50	1430.00	1693.30	2013.30	1720.	9-43	0-576	
11	1-20	1-250	62-37	74-50	1843.80	2572.80	2560.30	11-260	5-32	0-577	
12	1-20	1-250	63-54	74-50	2417.70	3272.70	3273.	11-130	7-165	0-578	
13	1-20	1-250	7-62	74-50	3074.60	4449.60	4449.	12-114	9-64	0-579	
14	1-20	1-250	80-01	74-50	3542.00	5224.00	3190.	9-313	10-40	0-580	
15	1-20	1-250	95-73	74-50	4725.60	6523.00	6756.00	9-137	1020.	9-123	
16	1-20	1-250	91-44	74-50	5744.00	7517.00	6246.00	6221.	11-15	0-146	
17	1-20	1-250	97-16	74-50	6756.00	8446.00	6441.00	4533.	7-379	0-127	
18	1-20	1-250	103-76	74-50	8074.60	11383.60	11383.	12-114	9-64	0-172	
19	1-20	1-250	120-01	74-50	10421.60	16201.60	16201.	9-313	10-40	0-173	
20	1-20	1-250	135-13	74-50	12202.00	17202.00	17202.	11-124	11-123	0-174	
21	1-20	1-250	151-30	74-50	17675.20	21561.00	16261.	13-760	10-60	0-175	
22	1-20	1-250	167-43	74-50	21-53	14-914.30	21-53	16261.	14-144	0-144	0-176
23	1-20	1-250	183-57	74-50	121-90	23-452.00	26410.00	1020.	4-925	9-46	0-177
24	1-20	1-250	199-69	74-50	132-65	17630.00	11440.	4-711	3-45	7-34	0-213
25	1-20	1-250	215-80	74-50	17630.00	20150.00	20150.	4-502	312.	0-222	0-222
26	1-20	1-250	231-93	74-50	21-53	31-560.00	31-560.	175.	4-323	0-233	0-233
27	1-20	1-250	248-06	74-50	24644.60	32422.00	32422.	4-125	130.	0-244	0-244
28	1-20	1-250	264-19	74-50	31-56	37410.00	37410.	13-56	3-916	11-763	0-336
29	1-20	1-250	280-32	74-50	41-66	47561.00	47561.	21-53	2-933	28-25	0-336
30	1-20	1-250	296-45	74-50	51-60	52150.00	52150.	23-10.	2-775	31-39	0-361
31	1-20	1-250	312-57	74-50	61-53	63250.00	63250.	2660.	5-579	34-95	0-382
32	1-20	1-250	328-69	74-50	71-47	63350.00	63350.	2920.	2-393	35-92	0-419
33	1-20	1-250	344-82	74-50	81-40	69460.00	69460.	2222.	93.	43-35	0-452
34	1-20	1-250	360-94	74-50	91-33	72310.00	72310.	2222.	96.	2222.	0-452

AVERAGE ELECTRICAL LOAD		PROPULSION COOLING...		9. KW	
		GENERATOR LUBE SYSTEM		2. KW	
		HELIUM COMPRESSORS...		2. KW	
SPEED.....	15.76 KNOTS				
EFFECTIVE PROPER	742.5 H.P.				
SHAFT POWER...	1026.0 H.P.				
USEFUL POWER...	1045.0 H.P.				
USEFUL POWER...	954.5 H.P.	LESS 1/2 ( 3.157 TRANS/MILE )			
USEFUL POWER...	954.5 H.P.	1/2 ( 3.157 TRANS/MILE )			
TOTAL...	1262.0 H.P.			9. KW ( 6.8 LBS/H.R.)	

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## SEPARATE DRIVE SYSTEM

REF. NO. 101

## MISSION PROFILE SUMMARY - ASCENT + ALITERNATORS AND CRUISE TURBINES

KTS	PCT.	TYPE	P/C	SHAFT RATIO	SPEED RPM	EFFECTIVE RATIO	SHAFT HP	TURBINE HP	FUEL RATE (PPH)	RANGE (NM/TON)	NAUT. MILES	TONS	PER MILE	NO. OF TURBINES	PER THOUSAND HOURS			
															CRUISE	CRUISE	CRUISE	CRUISE
1	1.10	0.297	25.94	74.00	1.43	75.57	75.56	360.	5.222	1.1.	1.77	0.161	1	1	1	1	1	
2	1.20	0.423	26.52	74.00	11.20	67.28	73.01	360.	12.40	24.	1.93	0.030	1	1	1	1	1	
3	1.20	0.735	26.82	74.00	37.80	70.35	76.32	360.	13.673	36.	1.93	0.054	1	1	1	1	1	
4	1.20	1.100	25.35	74.00	89.60	127.30	137.40	417.	21.41	40.	2.23	0.047	1	1	1	1	1	
5	1.20	1.100	31.70	74.00	175.00	24.50	254.10	514.	21.780	60.	2.75	0.243	1	1	1	1	1	
6	1.20	1.100	38.04	74.00	302.40	42.40	454.90	635.	21.142	72.	3.40	0.097	1	1	1	1	1	
7	1.20	1.100	46.58	74.00	462.20	55.00	550.40	781.	20.930	84.	4.19	0.058	1	1	1	1	1	
8	1.20	1.100	50.72	74.00	716.60	101.60	1102.00	955.	13.773	66.	5.12	0.253	1	1	1	1	1	
9	1.20	1.100	57.05	74.00	1021.00	147.50	1509.00	1150.	17.330	108.	6.22	0.056	1	1	1	1	1	
10	1.20	1.100	62.39	74.00	1403.60	149.40	2154.00	1400.	16.020	120.	7.51	0.253	1	1	1	1	1	
11	1.30	1.100	56.73	74.00	183.00	264.00	2865.00	1578.	14.693	692.	47.29	0.043	1	1	1	1	1	
12	1.30	1.100	76.07	74.00	241.70	342.00	3720.00	1999.	13.650	836.	58.92	0.275	1	1	1	1	1	
13	1.30	1.100	82.41	74.00	3776.00	415.00	4729.00	2348.	12.320	910.	74.18	0.062	1	1	1	1	1	
14	1.30	1.300	77.56	74.00	3542.00	5235.00	5505.00	3198.	9.305	594.	101.50	0.202	2	2	2	2	2	
15	1.30	1.300	83.10	74.00	4725.00	6500.	8500.	5771.	3677.	9.139	1020.	111.70	0.112	2	2	2	2	2
16	1.30	1.300	98.64	74.00	5732.00	7639.	8639.	6216.00	4215.	9.593	976.	114.60	0.116	2	2	2	2	2
17	1.30	1.300	94.18	74.00	6674.00	9452.	9857.00	4820.	7.901	112.	142.20	0.127	2	2	2	2	2	
18	1.30	1.300	114.10	21.50	8165.00	11570.	12560.00	5667.	7.050	129.	129.60	0.142	1	1	1	1	1	
19	1.30	1.300	129.40	21.50	6512.00	13610.	16760.00	6350.	6.772	1463.	212.60	0.153	1	1	1	1	1	
20	1.30	1.300	125.00	21.50	12200.00	12676.	17226.00	7875.	6.352	1730.	281.60	0.156	1	1	1	1	1	
21	1.30	1.300	131.10	21.50	12574.00	18570.	19300.00	18366.	5.933	1575.	264.20	0.158	1	1	1	1	1	
22	1.30	1.300	121.50	21.50	14910.00	20510.	21350.00	10310.	4.925	946.	192.40	0.203	2	2	2	2	2	
23	1.30	1.300	127.40	21.50	17040.	23330.	24610.00	10940.	4.711	345.	73.34	0.213	2	2	2	2	2	
24	1.30	1.300	133.00	21.50	19250.00	25630.	27730.00	11940.	4.502	312.	69.40	0.222	2	2	2	2	2	
25	1.30	1.300	131.50	21.50	21870.00	32290.	31350.00	11320.	4.320	175.	40.76	0.233	2	2	2	2	2	
26	1.30	1.300	144.00	21.50	24614.00	34650.	35260.00	14160.	4.105	130.	31.72	0.244	2	2	2	2	2	
27	0.40	1.100	142.60	21.50	27560.00	37410.	38430.00	15450.	3.916	102.	27.62	0.253	2	2	2	2	2	
28	0.30	1.400	147.50	21.50	22130.00	49340.	48110.00	15840.	3.462	86.	26.65	0.317	3	3	3	3	3	
29	0.30	1.400	154.10	21.50	37750.00	51580.	56500.00	22240.	2.921	67.	26.57	-0.343	3	3	3	3	3	
30	0.30	1.400	160.70	21.50	42950.00	59470.	54970.00	24220.	2.696	90.	33.47	0.372	3	3	3	3	3	
31	0.30	1.500	159.00	21.50	49240.00	66460.	72360.00	29200.	2.393	93.	26.92	0.419	4	4	4	4	4	
32	0.30	1.500	165.40	21.50	56300.00	75800.	63130.00	32320.	2.218	96.	43.35	0.452	-4	-4	-4	-4	-4	

## PERFORMANCE AVERAGES OVER MISSION PROFILE (1000 HOURS)

SPEED 15.76 KNOTS  
 EFFECTIVE POWER 7426. HP  
 SHAFT POWER 10400. HP  
 THRUST POWER 11600. HP  
 THRUST FUEL 5217. LBS/HR  
 PROPULSION FUEL 5023. LBS/HR

## AVERAGE ELECTRICAL LOAD OVER MISSION PROFILE (1000 HOURS)

PROPELLER COOLING 14. KW  
 GENERATOR LINE SYSTEM 3. KW  
 HELIUM COMPRESSORS 0. KW  
 TOTAL LOAD 14. KW + 110.0 LBS/HR

MISSION PROFILE SUMMARY = MISSION PROFILE

PER THOUSAND HOURS									
KTS	PCT.	P/D	SHAFT RPM	SPEED RATIO	EFFECTIVE HP	SMALL HP	TURBINE HP	FUEL RATE (PPH)	RANGE (NM/TON)
1	1.10	1.450	5.09	291.10	1.40	1.92	11.27	1122.	2.036
2	1.20	1.450	10.18	143.40	11.28	15.34	24.46	1109.	4.073
3	1.20	1.450	13.26	91.59	17.83	51.96	61.70	1100.	6.109
4	1.20	1.450	20.35	61.81	47.60	123.20	132.90	1100.	6.175
5	1.20	1.450	25.44	29.50	172.00	24.05	24.870	1102.	10.176
6	1.20	1.450	30.53	31.25	302.00	41.57	42.940	1235.	10.360
7	1.20	1.450	35.61	32.80	403.00	60.51	63.150	1365.	11.243
8	1.20	1.450	40.70	33.57	716.00	90.53	1018.00	1576.	11.373
9	1.20	1.450	45.76	36.21	1021.00	1423.00	1783.	11.310	126.
10	1.20	1.450	50.88	34.62	1400.00	1924.00	1991.00	2018.	11.100
11	5.30	1.450	55.97	34.79	1863.00	2561.00	2552.00	2234.	10.793
12	6.78	1.450	61.05	34.77	2415.00	3329.00	3349.00	2584.	10.493
13	7.63	1.450	66.14	34.56	3076.00	4223.00	4356.00	2921.	9.49
14	7.10	1.450	71.25	34.27	3442.00	5239.00	5452.00	3299.	9.39
15	6.30	1.450	76.32	33.84	4722.00	6492.00	6750.00	3721.	9.329
16	6.60	1.450	81.40	33.33	5734.00	8201.00	8451.00	4151.	9.321
17	6.69	1.450	86.46	32.75	6872.00	9457.00	9644.00	4713.	9.079
18	7.26	1.450	91.58	32.11	8165.00	11223.00	11700.00	9291.	7.621
19	7.70	1.450	96.67	31.44	9603.00	13200.00	13700.00	5928.	7.179
20	6.50	1.450	101.60	30.75	11230.00	15392.00	15100.00	6025.	6.754
21	7.50	1.450	106.63	30.24	12973.00	17820.00	16660.00	7348.	6.329
22	6.30	1.450	111.60	29.52	14916.00	20493.00	21460.00	6258.	5.982
23	6.30	1.450	117.04	27.53	17034.00	23415.00	24170.00	10620.	6.753
24	1.33	1.450	122.10	24.86	19324.00	26300.00	27470.00	11620.	4.515
25	0.70	1.450	127.20	24.44	21870.00	30074.00	31070.00	12920.	4.354
26	0.50	1.450	132.30	24.00	24616.00	33560.00	34470.00	14590.	4.132
27	0.40	1.450	137.40	23.55	27560.00	37330.00	37330.00	19194.	3.939
28	0.20	1.450	142.70	21.62	32130.00	44320.00	45320.00	15210.	3.205
29	0.30	1.450	148.10	21.25	37250.00	51750.00	53750.00	21230.	3.217
30	0.36	1.450	155.50	20.87	42650.00	60010.00	62410.00	24110.	3.237
31	0.36	1.450	163.00	19.57	45750.00	65240.00	71960.00	23790.	3.241
32	0.30	1.450	169.60	19.24	48300.00	69520.00	72750.00	23220.	3.259

OFFICIAL COPY OF THE REPORT OF THE MISSION TO CHINA

SPEED	15-76	KNOTS
EFFECTIVE POWER	7423.	HP
SHRAFT POWER	10230.	HP
THRUSTING POWER	10550.	HP
TURBINE EFFICIENCY	95.88.	LBS/HR
GENERATION EFFI.	50.76.	LBS/HR

Speed - - - - - 15-76  
Kilometres per hour

PAPILLON COOLING... 5. KW  
 GENERATOR LUBE SYSTEM 1. KW  
 HELIUM COMPRESSORS... 100. KW

MESSAGE STATISTICAL 103

PAPILLON COOLING... 5. KW  
 GENERATOR LUBE SYSTEM 1. KW  
 HELIUM COMPRESSORS... 100. KW

## ELECTRIC DRIVE SYSTEM

REF. NO. 02

## MISSION PROFILE SUMMARY - MAIN ONLY - SECURED ENGINE RUNS

KTS	PCT.	P/H	SHAFT RATED HP	SPEED HP	EFFECTIVE HP	SHAFT HP	TURBINE HP	FUEL RATE (PPH)	NO. OF TURBINES		
									RANGE NM/TON	NAUT. MILES	FUEL TONS PER MILE
1	1.16	1.450	5.06	291.10	1.43	1.42	11.27	11.20	2.056	11.	2.50
2	1.20	1.450	10.18	143.40	11.20	15.34	24.95	11.00	4.073	24.	6.33
3	1.20	1.450	15.26	51.59	37.60	51.46	11.00	6.100	0.179	1	MAIN
4	1.20	1.450	20.35	61.83	49.60	123.20	132.80	3.145	43.	6.33	MAIN
5	1.23	1.450	25.44	26.48	175.00	240.50	24.840	11.02	10.106	1	MAIN
6	1.26	1.450	30.53	31.24	30.70	415.70	426.80	10.170	10.863	0.053	MAIN
7	1.29	1.450	35.61	32.52	45.20	600.10	606.00	10.947	11.250	0.094	MAIN
8	1.29	1.450	40.70	33.54	57.00	582.40	581.00	11.750	11.350	0.092	MAIN
9	1.20	1.450	45.79	24.23	1321.00	1405.00	1447.00	17.61	11.320	1	MAIN
10	1.20	1.450	50.56	34.59	1436.00	1524.00	1546.00	20.00	11.110	1	MAIN
11	6.36	1.450	55.97	34.76	16.00	2201.00	2072.00	22.00	15.890	0.054	MAIN
12	6.76	1.450	61.05	26.74	2117.00	3365.00	3446.00	22.00	15.420	0.099	MAIN
13	7.00	1.450	66.50	24.55	3616.00	4228.00	4471.00	24.43	9.965	9.93	MAIN
14	7.10	1.450	71.23	36.23	3642.00	3263.00	5600.00	32.95	9.54	10.24	MAIN
15	6.63	1.450	76.32	36.81	4725.00	5795.00	6726.00	37.13	9.649	11.13	MAIN
16	6.12	1.450	81.40	35.73	5724.00	7532.00	6173.00	41.64	3.574	11.16	MAIN
17	6.42	1.450	86.47	32.72	61.40	64.47	64.47	3.101	11.20	11.20	MAIN
18	7.20	1.450	91.53	32.05	3162.00	11225.00	11225.00	52.75	7.54	12.40	MAIN
19	7.70	1.450	96.57	31.42	9503.00	13208.00	13720.00	59.09	7.20	14.63	MAIN
20	5.90	1.450	101.60	31.72	11230.00	12340.00	15020.00	66.00	6.792	17.60	MAIN
21	7.50	1.450	106.66	33.61	12570.00	1780.00	18560.00	73.70	5.393	15.75	MAIN
22	6.10	1.450	111.50	26.50	14910.00	20470.00	21370.00	47.21	3.101	11.20	MAIN
23	1.50	1.450	117.00	25.36	17530.00	26410.00	26410.00	24.30	7.54	12.40	MAIN
24	1.30	1.450	122.10	24.53	19360.00	26000.00	27700.00	30.00	11.620	14.63	MAIN
25	6.76	1.450	127.20	24.50	21510.00	33070.00	31430.00	31.30	4.293	17.55	MAIN
26	6.50	1.450	132.30	24.55	24610.00	35070.00	35380.00	34.220	4.65	13.00	MAIN
27	0.40	1.450	137.40	23.60	27750.00	37840.00	39500.00	3.901	10.8	27.63	MAIN
28	0.30	1.450	143.70	21.63	32170.00	44460.00	46430.00	4.516	3.245	26.54	MAIN
29	0.30	1.450	150.10	21.24	37250.00	51750.00	54220.00	21.670	2.917	29.19	MAIN
30	0.33	1.450	156.50	20.60	42500.00	62500.00	63000.00	24.600	2.767	32.70	MAIN
31	0.30	1.450	163.00	18.67	49270.00	69270.00	73030.00	27.10	2.735	35.15	MAIN
32	0.30	1.450	169.60	19.29	56300.00	76200.00	84360.00	24.000	2.212	43.60	MAIN

## PERFORMANCE AVERAGES OVER MISSION PROFILE I 1000 HOURS

SPEED	15.76	KNOTS
EFFECTIVE POWER	7428.	HP
SHFT POWER	10230.	HP
TURBINE POWER	10640.	HP
TURBINE FUEL	4585.	LBS/HR
PROPSIGN FUEL	5072.	LBS/HR

## AVERAGE ELECTRICAL LOAD OVER MISSION PROFILE I 1000 HOURS

AVERAGE ELECTRICAL LOAD	8. KW
PROPELLION COUPLING...	8. KW
GENERATOR LUBE SYSTEM...	1. KW
HELIUM COMPRESSORS...	100. KW
TOTAL LOAD.. 108. KW ( 87.5 LBS/HR )	

## ELECTRIC DRIVE SYSTEM

REF. NO. 01

## MISSION PROFILE SUMMARY - GAUTHERRESE - BASELINE

RTS	PCT.	P/H	RATING	SHPFT	SPEED	SHFT RPM	RATED HP	EFFECTIVE HP	SHAFT RATED HP	TURBINE 4P	FUEL RATE (PPH)	RANGE (NM/TON)	NAUT. MILES	TONS OVER MILE	NO. OF TURBINES	PER THOUSAND HOURS	
1	1.10	1.450	5.09	636.10	11.0	1.92	5.19	360.	5.19	5.422	11.	2.28	0.208	1	CRUISE		
2	1.20	1.450	10.18	326.20	11.20	15.54	16.68	560.	12.470	2.47	2.49	0.104	1	CRUISE			
3	1.20	1.450	15.25	177.70	47.60	51.46	55.64	360.	15.870	4.81	2.49	0.264	1	CRUISE			
4	1.20	1.450	20.35	126.80	89.50	12.50	12.60	126.30	4.65.	22.110	4.81	2.72	0.057	1	CRUISE		
5	1.20	1.450	25.44	114.80	175.00	240.50	250.30	492.	22.70	60.	3.20	0.053	1	CRUISE			
6	1.20	1.450	30.53	118.20	302.40	412.70	362.50	599.	22.440	72.	3.77	0.052	1	CRUISE			
7	1.20	1.450	35.61	115.60	460.20	660.10	557.20	557.00	21.500	84.	4.47	0.053	1	CRUISE			
8	1.20	1.450	40.70	119.20	716.60	960.40	1027.00	1027.00	667.	20.210	96.	5.31	0.059	1	CRUISE		
9	1.20	1.450	45.76	117.70	1024.20	1403.60	1524.50	1524.50	1524.50	13.75.	13.750	108.	6.32	0.059	1	CRUISE	
10	1.20	1.450	50.83	115.50	146.60	1524.60	1524.60	1524.60	2012.00	129.	17.200	120.	7.93	0.063	1	CRUISE	
11	6.30	1.450	55.90	112.70	1603.00	2061.00	2083.00	2083.00	1252.	15.770	653.	6.95	0.064	2	CRUISE		
12	6.70	1.450	61.05	103.70	2419.00	3325.00	3490.00	3490.00	1672.	14.360	804.	59.20	0.074	1	CRUISE		
13	7.00	1.450	66.14	135.70	3076.00	4273.00	4447.00	4447.00	2231.	11.050	910.	73.10	0.080	1	CRUISE		
14	7.10	1.450	71.23	88.56	3842.00	5250.00	5471.00	5471.00	3166.	9.994	994.	102.80	0.104	2	CRUISE		
15	6.60	1.450	76.32	75.39	4729.00	6462.00	6736.00	6736.00	3626.	9.203	1020.	114.70	0.112	2	CRUISE		
16	6.10	1.450	81.40	55.33	5754.00	7462.00	7631.00	7631.00	4191.	6.351	6351.	117.10	0.124	1	MAIN		
17	6.60	1.450	86.48	26.43	6875.00	8574.00	8744.00	8744.00	4729.	3.379	3.379.	1122.	0.127	1	MAIN		
18	7.20	1.450	91.56	32.11	8192.00	11720.00	11720.00	11720.00	5291.	7.361	1296.	175.70	0.134	1	MAIN		
19	7.70	1.450	96.67	31.44	8593.00	13200.00	13740.00	13740.00	5298.	7.179	1463.	207.70	0.142	1	MAIN		
20	8.50	1.450	101.80	40.75	14200.00	15550.00	15100.00	15100.00	6629.	6.758	1750.	263.00	0.151	1	MAIN		
21	7.50	1.450	106.80	20.64	17970.00	17970.00	18600.00	18600.00	7338.	6.399	1575.	251.60	0.160	1	MAIN		
22	4.70	1.450	26.43	26.43	4544.00	4544.00	4544.00	4544.00	4713.	3.379	3.379.	1122.	0.127	1	MAIN		
23	1.30	1.450	25.30	25.30	1704.00	2341.00	2341.00	2341.00	10620.	4.763	4.763.	73.21	0.212	2	MAIN		
24	1.30	1.450	122.12	24.88	1635.00	2660.00	2770.00	2770.00	11630.	4.535	4.535.	312.	0.222	2	MAIN		
25	3.70	1.450	127.20	24.44	21870.00	33070.00	31700.00	31700.00	12930.	4.534	4.534.	175.	0.232	2	MAIN		
26	0.50	1.450	132.30	24.44	26610.00	35520.00	34970.00	34970.00	14360.	6.132	6.132.	130.	0.244	2	MAIN		
27	6.40	1.450	137.40	23.55	27560.00	37560.00	34100.00	34100.00	15350.	2.939	108.	27.65	0.252	2	MAIN		
28	0.30	1.450	143.70	21.60	32150.00	44450.00	46550.00	46550.00	19210.	3.205	84.	25.91	0.308	3	MAIN		
29	0.30	1.450	150.40	21.25	57250.00	53750.00	53750.00	53750.00	21530.	3.517	67.	29.02	0.354	3	MAIN		
30	0.30	1.450	156.50	26.87	42950.00	60000.00	62410.00	62410.00	24100.	2.717	90.	32.49	0.381	3	MAIN		
31	0.30	1.450	162.20	19.57	45740.00	52740.00	52740.00	52740.00	28750.	2.412	93.	38.76	0.447	4	MAIN		
32	0.30	1.450	168.60	18.24	55300.00	75300.00	77760.00	77760.00	32250.	2.259	96.	43.05	0.449	4	MAIN		

## PERFORMANCE AVERAGES OVER MISSION PROFILE ( 1000 CLASS )

SPEED	15.70	KNOTS	
EFFECTIVE POWER	7420.	HP	
SHFT POWER	10230.	HP	
MOTOR POWER	10400.	HP	
THRUSTING FUEL	4750.	LBS/HR	( 3.132 LBS/MILE )
PROPULSION FUEL	4262.	LBS/HR	( 3.132 LBS/MILE )

AVERAGE ELECTRICAL LOAD	9. KVA
P2 PROPULSION COOLING...	1. KVA
GENERATOR LUBE SYSTEM...	1. KVA
HELICOPTER COMPRESSORS...	130. KVA
TOTAL LOAD...	140. KVA ( 111.9 LBS/HR )

## MISSION PROFILE SUMMARY - MAIN + CRUISE - RECONFIGURED ENGINE ROOM

KTS	PCT.	TYPE	RATING	SHAFT RPM	SPEED - HP	EFFECTIVE RATIO	SHAFT HP	TURBINE HP	FUEL RATE (PPH)	RANGE (NM/TON)	NAUT. MILES	TONS PER MILE	TCNS	FUEL PER MILE	NO. OF TURBINES	PER THOUSAND HOURS	
																NAUT. MILES	TONS PER MILE
1	1.10	1-450	5.39	686.10	1.40	1.47	5.19	360.	5.222	11.	2.78	6.209	1	CRUISE	1	CRUISE	
2	1.20	1-450	10.16	326.10	1.20	1.34	8.89	360.	12.40	24.	2.49	8.104	1	CRUISE	1	CRUISE	
3	1.20	1-450	15.26	17.60	1.40	1.46	5.70	360.	13.67	36.	2.49	8.269	1	CRUISE	1	CRUISE	
4	1.20	1-450	20.35	102.50	8.60	123.20	12.60	405.	22.10	43.	2.73	8.057	1	CRUISE	1	CRUISE	
5	1.20	1-450	25.44	11.40	175.50	240.50	250.50	492.	22.74	60.	3.20	8.053	1	CRUISE	1	CRUISE	
6	1.20	1-450	30.53	11.60	302.40	415.70	433.60	630.	22.41	72.	3.73	8.022	1	CRUISE	1	CRUISE	
7	1.20	1-450	35.61	11.80	460.20	560.10	664.50	730.	21.47	73.	4.48	8.055	1	CRUISE	1	CRUISE	
8	1.20	1-450	40.70	11.60	716.50	935.30	1031.00	868.	20.17	96.	5.32	8.055	1	CRUISE	1	CRUISE	
9	1.26	1-450	45.75	11.70	1021.00	1403.50	1770.50	1075.	13.71	106.	6.24	8.059	1	CRUISE	1	CRUISE	
10	1.20	1-450	50.83	11.50	1430.00	1821.00	1821.00	1323.	17.20	120.	7.55	8.063	1	CRUISE	1	CRUISE	
11	6.36	1-450	55.97	11.20	1633.00	2561.00	2577.00	1563.	15.74	693.	47.11	8.268	1	CRUISE	1	CRUISE	
12	6.76	1-450	61.05	10.60	2415.00	3325.00	3510.00	1374.	14.32	644.	59.43	8.074	1	CRUISE	1	CRUISE	
13	7.66	1-450	66.14	10.50	3078.00	4224.00	4714.00	2241.	12.95	910.	73.43	8.081	1	CRUISE	1	CRUISE	
14	7.12	1-450	71.23	8.60	3892.00	5250.00	5252.00	3167.	9.84	994.	106.50	8.105	2	CRUISE	2	CRUISE	
15	6.80	1-450	76.32	8.60	4725.00	6025.00	6135.00	3577.	9.13	1022.	115.00	8.113	2	CRUISE	2	CRUISE	
16	6.12	1-450	81.40	8.30	5754.00	7582.00	6170.00	4161.	8.57	971.	116.60	8.120	1	MAIN	1	MAIN	
17	5.56	1-450	86.49	8.20	61.05	93.00	93.00	4701.	8.10	122.	141.80	8.126	1	MAIN	1	MAIN	
18	7.20	1-450	61.55	39.55	11220.00	1105.00	11450.00	5275.	7.64	1296.	173.20	8.134	1	MAIN	1	MAIN	
19	7.70	1-450	64.67	41.42	683.00	1320.00	1372.00	5299.	7.20	1463.	207.50	8.142	1	MAIN	1	MAIN	
20	7.90	1-450	61.80	41.60	1520.00	15350.00	15320.00	6006.	6.75	1780.	257.60	8.150	1	MAIN	1	MAIN	
21	7.50	1-450	73.01	35.01	17972.00	17972.00	17972.00	7375.	6.39	1575.	250.70	8.159	1	MAIN	1	MAIN	
22	4.36	1-450	26.45	32.72	6878.00	9354.00	9408.00	4701.	5.10	122.	141.80	8.126	1	MAIN	1	MAIN	
23	4.56	1-450	111.60	28.30	14910.00	21570.00	21570.00	8205.	9.35	946.	159.80	8.169	1	MAIN	1	MAIN	
24	1.36	1-450	122.10	24.50	15340.00	23410.00	24430.00	10930.	4.72	345.	73.75	8.214	2	MAIN	2	MAIN	
25	0.76	1-450	127.20	24.50	21870.00	30370.00	31430.00	13030.	4.55	312.	65.92	8.224	2	MAIN	2	MAIN	
26	0.56	1-450	132.30	24.50	26610.00	32820.00	32390.00	14220.	4.29	175.	41.12	8.235	2	MAIN	2	MAIN	
27	0.40	1-450	127.40	25.60	37500.00	37800.00	35660.00	15200.	3.95	130.	32.64	8.246	2	MAIN	2	MAIN	
28	0.36	1-450	143.70	21.60	32130.00	46470.00	46470.00	15320.	3.24	108.	27.92	8.225	3	MAIN	3	MAIN	
29	0.36	1-450	156.10	21.20	37250.00	54720.00	54720.00	21670.	2.99	87.	26.07	8.210	3	MAIN	3	MAIN	
30	0.32	1-450	166.50	20.60	42500.00	68100.00	63900.00	24200.	2.76	97.	32.74	8.236	3	MAIN	3	MAIN	
31	0.30	1-450	163.00	17.60	65290.00	65740.00	65350.00	25100.	2.53	93.	39.21	8.242	4	MAIN	4	MAIN	
32	0.30	1-450	169.00	19.20	56320.00	74520.00	84050.00	32400.	2.21	96.	45.64	8.455	4	MAIN	4	MAIN	

## C-24 PERFORMANCE AVERAGES OVER MISSION PROFILE (1000 HOURS)

SPEED...00000	15.76	KNOTS
EFFECTIVE POWER	7428.	HP
SHAFT POWER....	10230.	HP
TURBINE POWER....	10670.	HP
TURBINE FUEL....	4753.	LBS/HR
PROPELLER FUEL	4565.	LBS/HR

C-24

PERFORMANCE AVERAGES OVER MISSION PROFILE (1000 HOURS)

AVERAGE ELECTRICAL LOAD	9. KW
PROPULSION COOLING...	9. KW
GENERATOR LUBE SYSTEM	1. KW
HELIUM COMPRESSORS...	130. KW
TOTAL LOAD... 140. KW (112.1 LBS/HR)	

## MISSION PROFILE SUMMARY - MAIN + CRUISE - OPTIMUM CONFIGURATION

KIS	PCT. TIME	P/D RATIO	SHAFT SPEED	EFFECTIVE RATIO	SHAFT HP	TURBINE HP	FUEL RATE (PPH)	(N/MIN)	RANGE MILES	NAUT. TONS	TONS PER MILE	NO. OF TURBINES	PER THOUSAND HOURS	
													PER THOUSAND HOURS	TONS
1	1.10	1.450	5.00	6.96:10	1.40	1.92	2.18	300.	6.222	11.	2.28	3.28	1	CRUISE
2	1.20	1.450	10.18	326:20	1.20	1.54	1.64	300.	12.440	24.	2.49	6.164	1	CRUISE
3	1.20	1.450	15.00	178:00	1.20	1.96	55:4	360.	18.670	36.	2.49	0.069	1	CRUISE
4	1.20	1.450	20.35	108:60	1.20	123:23	177:70	305.	22.130	49.	2.73	0.057	1	CRUISE
5	1.20	1.450	25.44	112:60	1.20	201:52	275:40	311.	22.600	60.	3.19	0.053	1	CRUISE
6	1.20	1.450	30.53	117:60	1.20	245:70	477:30	547.	22.500	72.	3.76	0.052	1	CRUISE
7	1.20	1.450	35.61	119:20	1.20	301:10	641:63	727.	21.500	64.	4.46	0.053	1	CRUISE
8	1.20	1.450	40.69	118:60	1.20	345:30	882.	1017:30	20.310	76.	5.29	0.052	1	CRUISE
9	1.20	1.450	45.79	117:40	1.20	403:60	1469:60	1069.	19.870	126.	6.27	0.050	1	CRUISE
10	1.20	1.450	50.86	116:60	1.20	460:00	1989:50	1289.	17.370	120.	7.47	0.052	1	CRUISE
11	6.36	1.450	57.97	111:50	1.20	563:00	2544:30	1553.	15.900	693.	4.57	0.057	1	CRUISE
12	6.76	1.450	61.50	123:40	1.20	526:00	3726:30	1254.	14.500	854.	5.83	0.073	1	CRUISE
13	7.00	1.450	65.14	106:70	1.20	576:00	4248:0	24381:30	13.200	910.	72.30	0.079	1	CRUISE
14	7.10	1.450	71.23	160:90	1.20	542:60	5250:30	24779:30	2613.	12.000	94.	0.077	1	CRUISE
15	6.60	1.450	76.32	86:76	1.20	4725:60	6492:00	6724:30	1045.	10.200	114.	0.112	2	CRUISE
16	6.16	1.450	81.40	33:50	1.20	5734:00	7652:00	8170:30	4181.	976.	116.	0.120	1	MAIN
17	5.60	1.450	86.49	37:72	1.20	6978:00	9424:00	9424:00	5808.	5701.	1122.	0.126	1	MAIN
18	7.20	1.450	91.53	37:65	1.20	51:00	11225:00	11225:00	5275.	7642.	1296.	0.134	1	MAIN
19	7.70	1.450	96.67	31:42	1.20	50:00	13230:00	13230:00	5309.	74202.	1463.	0.142	1	MAIN
20	6.90	1.450	101:60	31:72	1.20	53:00	15230:00	15230:00	5606.	6752.	1780.	0.150	1	MAIN
21	7.50	1.450	106:60	30:61	1.20	5761:00	17761:00	16530:00	7370.	5333.	1575.	0.159	1	MAIN
22	6.30	1.450	111:60	29:60	1.20	6200:00	20420:00	21370:00	6205.	6205.	156:00	0.169	1	MAIN
23	1.50	1.450	117:00	25:36	1.20	51:00	24430:00	24430:00	10900.	4723.	345.	0.214	2	MAIN
24	1.20	1.450	122:10	24:63	1.20	52:00	27760:00	11420.	6505.	312.	49.	0.214	2	MAIN
25	0.76	1.450	127:20	24:50	1.20	5170:00	30470:00	31430:00	13030.	4293.	175.	0.235	2	MAIN
26	0.56	1.450	132:30	24:05	1.20	5610:00	35390:00	14220:00	4605.	4605.	130.	0.246	2	MAIN
27	0.40	1.450	137:40	22:60	1.20	57560:00	37660:00	39360:00	15500.	39301.	108.	0.259	2	MAIN
28	0.32	1.450	143:70	21:67	1.20	5210:00	44000:00	46430:00	15300.	3245.	87.	0.310	3	MAIN
29	0.30	1.450	150:10	21:26	1.20	57250:00	51750:00	54220:00	21670.	21670.	87.	0.330	3	MAIN
30	0.20	1.450	156:50	20:56	1.20	5610:00	62900:00	63360:00	24290.	2797.	90.	0.364	3	MAIN
31	0.20	1.450	163:00	19:62	1.20	59270:00	62490:00	73030:00	29110.	2385.	93.	0.422	4	MAIN
32	0.20	1.450	169:60	15:74	1.20	56300:00	74520:00	84360:00	32400.	2212.	96.	0.494	4	MAIN

PERFORMANCE AVERAGES OVER MISSION PROFILE (1000 HOURS)

EFFECTIVE SPEED	15.76 KNOTS
EFFECTIVE POWER	7423 HP
SHAFT POWER	13230 HP
TURBINE POWER	16600 HP
TURBINE FUEL	4705 LBS/HR (0.133 TONS/MILE)
PROPELLION FUEL	4.815 LBS/HR (0.136 TONS/MILE)

AVERAGE ELECTRICAL LOAD	8. KW
PROPELLION COOLING...	
GENERATOR LUBE SYSTEM	1. KW
HELIUM COMPRESSORS...	130. KW
TOTAL LOAD...	140. KW (111.6 LBS/HR)

## GEARED DRIVE SYSTEM

## MISSION PROFILE SUMMARY - BASELINE - VARIABLE PITCH

REF. NO. 101

KTS	PCT.	RATIO	SHAFT RPM	SPEED RATIO	EFFECTIVE HP	SHAFT HP	TURBINE HP	FUEL SATU. (PSI)	RANGE (NM/TON)	MILE	TONS PER MILE	PER THOUSAND HOURS	NO. OF TURBINES		
1.10	0.278	44.08	21.50	1.40	44.00	455.60	2200.	1.018	11.	10.81	0.982	2	MAIN		
1.20	0.305	47.58	21.50	1.10	410.20	427.30	2200.	2.035	24.	11.73	0.431	2	MAIN		
1.30	0.329	50.78	21.50	0.80	371.50	269.10	2200.	3.055	35.	11.75	0.327	2	MAIN		
1.40	0.3487	52.03	21.50	0.60	355.40	373.30	2200.	4.073	48.	11.79	0.246	2	MAIN		
1.50	0.3646	53.07	21.50	0.40	375.00	388.10	2200.	5.091	60.	11.79	0.166	2	MAIN		
1.60	0.3677	42.35	21.50	0.20	322.40	451.50	2200.	6.109	72.	11.79	0.164	2	MAIN		
1.70	1.301	38.78	21.50	0.00	460.20	650.60	2200.	6.658	84.	12.62	0.150	2	MAIN		
1.80	1.220	45.98	21.50	0.20	716.60	987.20	1028.00	6.212	26.	12.88	0.145	2	MAIN		
1.90	1.247	51.57	21.50	0.40	1021.00	1402.00	1465.00	7.052	106.	15.30	0.142	2	MAIN		
2.00	1.222	57.17	21.50	0.60	1400.00	1936.00	2017.00	3.151	7.102	120.	0.82	0.141	2	MAIN	
2.10	1.220	64.15	21.50	0.80	1563.00	2591.00	2666.00	3.490	7.080	623.	0.73	0.141	2	MAIN	
2.20	1.212	70.12	21.50	1.00	2419.00	3552.00	3552.00	3.645	6.921	624.	0.73	0.143	2	MAIN	
2.30	1.207	75.49	21.50	1.20	3075.00	4257.00	4445.00	4.247	6.956	910.	132.80	0.145	2	MAIN	
2.40	1.203	82.28	21.50	1.40	3842.00	5322.00	5551.00	4.690	6.687	994.	146.80	0.150	2	MAIN	
2.50	1.208	89.16	21.50	1.60	4725.00	6554.00	6627.00	5.174	6.494	1020.	157.20	0.154	2	MAIN	
2.60	1.211	95.86	21.50	1.80	5754.00	7652.00	8283.00	5.704	6.253	976.	155.50	0.156	2	MAIN	
2.70	1.216	98.39	21.50	2.00	6372.00	9559.00	9559.00	6.371	6.062	1172.	135.30	0.156	2	MAIN	
2.80	1.222	104.69	21.50	2.20	7165.00	11310.00	11310.00	7.170	5.875	1266.	227.40	0.172	2	MAIN	
2.90	1.231	110.10	21.50	2.40	8103.00	13282.00	13282.00	8.000	5.605	1463.	261.20	0.176	2	MAIN	
3.00	1.238	115.20	21.50	2.60	1200.00	15480.00	15120.00	8.232	5.377	1780.	231.50	0.185	2	MAIN	
3.10	1.247	120.30	21.50	2.80	12970.00	17510.00	18130.00	9.133	5.175	1575.	306.20	0.194	2	MAIN	
3.20	1.259	125.59	21.50	3.00	14910.00	20570.00	21420.00	9.999	4.929	946.	192.20	0.203	2	MAIN	
3.30	1.273	132.50	21.50	3.20	17930.00	23470.00	24450.00	10.930	4.712	73.32	213.20	0.213	2	MAIN	
3.40	1.286	138.49	21.50	3.40	1834.00	21930.00	22650.00	11.940	4.555	212.	69.30	0.222	2	MAIN	
3.50	1.278	142.76	21.50	3.60	21870.00	30100.00	31350.00	13.020	4.306	175.	40.76	0.233	2	MAIN	
3.60	1.293	146.99	21.50	3.80	21870.00	31350.00	31350.00	14.100	4.155	130.	31.72	0.244	2	MAIN	
3.70	1.313	148.99	21.50	4.00	24610.00	33830.00	35240.00	15.440	3.917	108.	27.61	0.256	2	MAIN	
3.80	1.328	147.12	21.50	4.20	2550.00	37570.00	39450.00	16.920	3.683	54.	28.20	0.256	4	MAIN	
3.90	1.3472	142.12	21.50	4.40	32130.00	44440.00	45290.00	21.040	3.476	67.	31.30	0.361	4	MAIN	
4.00	1.365	147.9	21.50	4.60	37250.00	51920.00	53500.00	23.900	3.276	2.579	90.	34.65	0.369	4	MAIN
4.10	1.389	152.50	21.50	4.80	42250.00	60140.00	62560.00	25.640	3.076	93.	33.92	0.410	4	MAIN	
4.20	1.409	156.49	21.50	5.00	43260.00	66500.00	72360.00	29.020	2.873	96.	43.54	0.452	4	MAIN	
4.30	1.432	158.49	21.50	5.20	56300.00	79970.00	82310.00	22.310	2.218						

## PERFORMANCE AVERAGES OVER MISSION PROFILE ( 1000 HOURS )

SPEED.....	15.76	KNOTS
EFFECTIVE POWER	7428.	HP
SHAFT POWER.....	10760.	HP
TURBINE POWER.....	16730.	HP
TURBINE FUEL.....	6586.	LBS/H2
PROPELLION FUEL	6393.	LBS/H2

## AVERAGE ELECTRICAL LOAD ( 1000 HOURS )

AVERAGE ELECTRICAL LOAD	9. KW
PROPELLION COOLING...	9. KW
GENERATOR LUBE SYSTEM...	0. KW
HELIUM COMPRESSORS...	0. KW
TOTAL LOAD...	9. KW

## PERIODIC PROFILE ( 1000 HOURS )

AVERAGE ELECTRICAL LOAD	6.9 LBS/H2
PROPELLION COOLING...	6.9 LBS/H2
GENERATOR LUBE SYSTEM...	0. LBS/H2
HELIUM COMPRESSORS...	0. LBS/H2
TOTAL LOAD...	6.9 LBS/H2

C-26

## GEARED DRIVE SYSTEM

REF. NO. 101

## MISSION PROFILE SUMMARY - BASELINE + ALTERNATORS + CRUISE TURBINES - VARIABLE PITCH

KTS	PCT.	TIME	P/TN	SHAFT	SPEED	RATIO	EFFECTIVE	SHAFT	TURBINE	FUEL RATE	RANGE	NAUT. MILES	TONS	TONS PER MILE	NO. OF TURBINES	PER THOUSAND HOURS	
																HP	HP
1	1-10	0.297	25.94	74.00	1.40	70.57	76.28	350.	5.222	11.	1.77	0.161	1	CRUISE			
2	1-20	0.423	26.52	74.00	1.20	57.26	73.01	360.	12.440	24.	1.63	0.080	1	CRUISE			
3	1-20	0.735	26.22	74.00	37.80	76.05	76.32	360.	18.670	36.	1.93	0.054	1	CRUISE			
4	1-20	1-115	25.15	74.00	87.60	126.60	137.40	-	4.17.	21.490	45.	2.23	0.047	1	CRUISE		
5	1-20	1-584	31.91	74.00	175.00	243.60	259.70	-	514.	21.780	60.	2.76	0.046	1	CRUISE		
6	1-20	1-276	35.52	74.00	362.40	431.50	468.50	634.	21.180	72.	3.43	0.047	2	CRUISE			
7	1-20	1-574	45.37	74.00	480.70	561.80	744.70	725.	20.040	84.	4.16	0.050	2	CRUISE			
8	1-20	1-679	51.58	74.00	71.60	102.00	1105.00	954.	15.770	95.	5.12	0.053	1	CRUISE			
9	1-20	1-389	57.58	74.00	1021.30	1451.00	1275.00	1530.	17.380	108.	6.22	0.058	1	CRUISE			
10	1-20	1-100	63.42	74.00	1405.00	1984.00	2153.00	1400.	16.000	140.	7.51	0.063	1	CRUISE			
11	1-20	1-103	69.15	74.00	1863.00	2633.00	2856.00	1678.	14.690	693.	4.72	0.063	1	CRUISE			
12	6.30	1-171	74.42	74.00	2415.00	3492.00	3497.00	1697.	13.440	804.	59.86	0.074	1	CRUISE			
13	7.70	1-151	78.47	74.00	3214.00	4307.00	4674.00	2364.	12.320	910.	74.04	0.081	1	CRUISE			
14	7.10	1-258	79.50	74.00	3622.00	5296.00	5417.00	3198.	9.813	994.	101.40	0.102	2	CRUISE			
15	6.80	1-279	84.25	74.00	4725.00	6504.00	6760.00	2876.	8.141	1020.	111.70	0.116	2	CRUISE			
16	5.10	1-269	85.74	74.00	5754.00	7575.00	7830.00	6218.	42.15.	8502.	975.	0.115	2	CRUISE			
17	4.60	1-322	94.05	74.00	6576.00	9544.00	9544.00	6319.	7.923	1122.	142.20	0.127	2	CRUISE			
18	7.20	1-122	112.60	21.50	8145.00	11510.00	12480.00	5685.	7.032	1296.	163.20	0.141	1	MAIN			
19	7.70	1-133	117.50	21.50	9506.00	12493.00	14540.00	6345.	6.737	1463.	218.70	0.153	1	MAIN			
20	8.60	1-146	123.70	21.50	11236.00	15700.00	1706.00	7064.	6.342	1780.	261.50	0.153	1	MAIN			
21	7.50	1-156	128.20	21.50	12570.00	18150.00	18150.00	7846.	5.925	1575.	263.50	0.167	1	MAIN			
22	4.30	1-259	125.10	21.50	14610.00	20570.00	21420.00	9996.	4.929	946.	192.20	0.202	2	MAIN			
23	1-50	1-273	125.50	21.50	17630.00	23470.00	24450.00	10930.	4.712	345.	73.32	0.213	2	MAIN			
24	1-46	1-283	124.40	21.50	19330.00	26426.00	27760.00	11940.	4.503.	312.	6.939	0.322	2	MAIN			
25	0.70	1-269	139.70	21.50	21670.00	30120.00	31350.00	31350.00	6.342	1780.	261.50	0.153	1	MAIN			
26	0.50	1-313	143.00	21.50	24610.00	33830.00	35230.00	35230.00	7.846.	1575.	263.50	0.167	2	MAIN			
27	0-42	1-326	147.10	21.50	27560.00	37470.00	37470.00	37470.00	14190.	4.105.	130.	31.72	0.244	2	MAIN		
28	0-30	1-297	148.10	21.50	32150.00	44330.00	44330.00	44330.00	15440.	3.917	108.	27.61	0.253	2	MAIN		
29	0-20	1-458	152.40	21.50	37250.00	51370.00	51370.00	51370.00	19640.	3.162	84.	26.65	0.317	3	MAIN		
30	0-30	1-420	150.40	21.50	42950.00	574920.00	574920.00	574920.00	22230.	2.922	67.	25.37	0.313	3	MAIN		
31	0-30	1-506	158.40	21.50	49290.00	65020.00	72390.00	72390.00	24920.	2.537	90.	33.48	0.372	3	MAIN		
32	0-30	1-527	163.20	21.50	56200.00	79790.00	63410.00	63410.00	29020.	2.393	93.	36.92	0.419	4	MAIN		
										2.218	96.	43.34	0.452	4	MAIN		

## PERFORMANCE AVERAGES OVER MISSION PROFILE 4 (1000 HOURS)

SPEED 15.76 KNOTS  
 EFFECTIVE POWER 7426.4P  
 SHAFT POWER 10350.4P  
 TURBINE POWER 11030.4P  
 TURBINE FUEL 5012.504T  
 PROPULSION FUEL 5024.504T

AVERAGE ELECTRICAL LOAD 14. KW  
 PROPULSION COOLING 14. KW  
 GENERATOR LUBE SYSTEM 0. KW  
 HELIUM COMPRESSORS 0. KW  
 TOTAL LOAD 14. KW ( 11.0 LBS/HR )

## ELECTRIC DRIVE SYSTEM

## MISSION PROFILE SUMMARY - MAIN ONLY - VARIABLE P/D

PER THOUSAND HOURS

KTS	PCT. TIME	P/D	SHAFT RPM	SPEED RPM	EFFECTIVE HP	SHAFT HP	TURBINE HP	FUEL RATE (GPH)	RANGE (NM/TON)	NAUT. MILES	FUEL TONS	TONS PER MILE	NO. OF TURBINES
1	1.10	1.500	4.96	268.70	1.40	1.93	11.27	2130.	2.23.5	11.	5.30	0.527	1 MAIN
2	1.20	1.500	9.92	147.20	11.20	15.42	24.95	1130.	4.07.3	24.	6.36	0.264	1 MAIN
3	1.20	1.500	14.67	93.59	37.60	52.05	61.73	1100.	6.10.9	36.	6.35	0.176	1 MAIN
4	1.20	1.500	19.33	63.42	68.60	123.40	133.00	1100.	8.145	48.	6.33	0.122	1 MAIN
5	1.20	1.465	26.08	28.77	175.00	246.32	248.50	1102.	10.170	62.	6.34	0.106	1 MAIN
6	1.20	1.390	31.51	30.83	302.43	412.20	425.10	1237.	13.360	72.	7.36	0.396	1 MAIN
7	1.20	1.346	35.65	31.43	408.20	529.40	561.40	1352.	11.240	84.	7.91	0.394	1 MAIN
8	1.20	1.340	42.54	32.25	716.60	934.20	1027.00	1272.	11.380	96.	8.47	0.352	1 MAIN
9	1.20	1.361	47.96	32.65	1221.00	1401.00	1448.00	1432.	11.320	108.	9.56	0.092	1 MAIN
10	1.20	1.364	53.42	32.96	1430.00	1925.00	1967.00	2016.	11.110	120.	11.24	0.094	1 MAIN
11	6.30	1.364	56.76	33.12	1663.00	2259.00	2846.00	2242.	12.800	693.	66.48	0.096	1 MAIN
12	6.70	1.360	64.25	33.62	2419.00	3322.00	3638.00	2581.	13.420	804.	79.67	0.299	1 MAIN
13	7.05	1.354	69.64	32.73	3075.00	4224.00	4374.00	2917.	9.932	910.	93.76	0.103	1 MAIN
14	7.10	1.346	75.57	32.25	3827.00	5467.00	5677.00	3294.	9.520	954.	107.10	0.108	1 MAIN
15	6.52	1.346	80.97	31.87	4725.00	6493.00	6730.00	3715.	9.045	1020.	115.30	0.115	1 MAIN
16	6.10	1.346	86.36	31.36	5764.00	7877.00	8175.00	4183.	8.558	976.	116.20	0.117	1 MAIN
17	6.60	1.315	92.39	30.90	6674.00	9450.00	9814.00	4703.	8.098	1122.	141.10	0.126	1 MAIN
18	7.20	1.312	97.73	30.07	6162.00	11226.00	11660.00	5273.	7.640	1256.	172.50	0.133	1 MAIN
19	7.76	1.327	103.70	29.50	9603.00	13209.00	13750.00	5911.	7.230	1463.	206.30	0.141	1 MAIN
20	6.96	1.327	109.10	28.65	11240.00	15390.00	16030.00	6639.	6.779	1780.	266.20	0.150	1 MAIN
21	7.50	1.327	114.60	27.93	12870.00	17620.00	18570.00	7373.	6.360	1575.	250.95	0.154	1 MAIN
22	4.30	1.325	120.20	27.29	14510.00	20490.00	21340.00	6208.	6.004	946.	159.40	0.164	1 MAIN
23	4.50	1.346	123.50	23.69	17530.00	23400.00	24190.00	16600.	4.772	345.	72.91	0.211	2 MAIN
24	4.30	1.346	136.50	24.44	19350.00	26580.00	27400.00	11600.	4.554	312.	69.35	0.221	2 MAIN
25	6.70	1.346	134.90	23.63	21870.00	30460.00	32650.00	12650.	4.364	175.	40.59	0.232	2 MAIN
26	6.50	1.346	140.30	22.61	24610.00	33350.00	34860.00	14060.	4.142	130.	31.61	0.243	2 MAIN
27	6.40	1.346	145.70	22.16	27500.00	35200.00	35860.00	15320.	3.948	108.	27.53	0.255	2 MAIN
28	6.50	1.321	154.60	20.95	32150.00	44300.00	45600.00	19150.	3.276	84.	25.75	0.307	3 MAIN
29	2.30	1.201	163.70	19.51	37250.00	53420.00	55130.00	21420.	3.032	67.	26.84	0.332	3 MAIN
30	0.30	1.201	173.60	16.66	42600.00	59200.00	61670.00	23960.	2.805	90.	32.24	0.358	3 MAIN
31	0.30	1.305	176.70	18.41	49250.00	58880.00	61310.00	28610.	2.427	93.	36.48	0.424	4 MAIN
32	0.30	1.311	163.20	18.43	56300.00	79020.00	81920.00	31600.	2.254	95.	42.76	0.445	4 MAIN

## PERFORMANCE AVERAGES OVER MISSION PROFILE ( 1300 HOURS )

SPEED	15.76	MINUTES	AVERAGE ELECTRICAL LOAD	9. KW
EFFECTIVE POWER	742.0	HP	PROPELLION COOLING...	
SHAFT POWER	1020.	HP	GENERATOR LUBE SYSTEM	1. KW
TURBINE POWER	1060.	HP	HELIUM COMPRESSORS...	100. KW
TURBINE FUEL	4975.	LBS/HR	TOTAL LOAD...	109. KW ( 37.1 LBS/HR )
PROPULSION FUEL	5953.	LBS/HR		

## ELECTRIC DRIVE SYSTEM

REF. NO. 01

## MISSION PROFILE SUMMARY - MAIN + CRUISE - VARIABLE 270

## PER THOUSAND HOURS

KTS	PCT.	P/R	SHAFT RPM	SPEED RATIO	EFFECTIVE RPM	SHAFT HP	TURBINE HP	FUEL RATE (PPH)	RANGE (NM/TON)	NAUT. MILES	TONS PER MILE	NO. OF TURBINES
1	1.10	1.530	4.96	704.10	1.43	1.94	5.16	360.	6.222	11.	2.23	1 CRUISE
2	1.22	1.530	9.92	534.70	11.20	15.82	13.48	360.	12.440	24.	2.49	1 CRUISE
3	1.22	1.530	12.87	162.30	37.50	52.95	59.63	360.	13.670	36.	2.49	1 CRUISE
4	1.26	1.430	20.64	125.70	69.60	123.20	126.30	405.	22.110	43.	2.73	1 CRUISE
5	1.26	1.336	26.35	116.80	175.00	240.30	250.10	452.	22.770	60.	3.20	1 CRUISE
6	1.26	1.372	31.50	113.10	302.40	415.20	431.90	599.	22.450	72.	3.77	1 CRUISE
7	1.26	1.364	57.37	113.60	486.20	654.40	655.90	724.	21.520	84.	4.47	1 CRUISE
8	1.23	1.354	42.96	112.90	71.60	96.50	102.40	685.	20.240	96.	5.31	1 CRUISE
9	1.23	1.345	45.53	110.90	140.20	140.20	140.20	1075.	18.720	108.	6.31	1 CRUISE
10	1.23	1.336	53.67	164.63	1426.00	1924.40	2005.00	1295.	17.230	120.	7.51	1 CRUISE
11	6.43	6.64	73.60	184.63	185.60	258.00	267.00	1525.	15.810	693.	8.64	1 CRUISE
12	6.72	1.327	65.47	151.20	5419.00	3525.00	3475.00	1866.	14.400	634.	9.03	1 CRUISE
13	7.63	1.325	71.31	97.75	1C75.00	4227.60	4428.00	2225.	13.100	510.	10.30	1 CRUISE
14	7.13	1.346	75.57	62.45	3242.00	5217.00	5456.00	3161.	9.922	994.	103.60	2 CRUISE
15	6.96	1.346	60.97	61.39	4725.00	6450.00	6716.00	3642.	9.223	1020.	113.92	1.12
16	6.16	1.345	56.36	21.23	5731.00	7577.00	7877.00	4163.	8.568	976.	116.96	1 MAIN
17	5.60	1.336	62.30	30.16	6575.00	9429.00	9470.00	6117.00	8.595	1122.	141.30	0.124
18	7.23	1.332	97.75	33.97	81.65	1142.00	1156.00	5213.	7.370	1295.	173.22	2 MAIN
19	7.76	1.327	103.70	25.40	63.05	1320.00	1376.00	5911.	7.260	1463.	207.10	1.42
20	6.90	1.327	102.10	28.45	112.02	1539.00	1603.00	6006.	6.779	1780.	267.10	0.150
21	7.50	1.327	114.60	27.99	12970.00	17520.00	15370.00	7373.	6.380	1575.	250.80	1.159
22	4.36	1.325	120.20	27.29	14910.00	20460.00	21350.00	6225.	6.004	946.	159.90	1 MAIN
23	1.52	1.346	123.90	23.63	17280.00	24100.00	24100.00	10800.	4.772	345.	73.03	0.212
24	1.36	1.346	123.50	23.44	19350.00	26540.00	27440.00	11830.	4.554	312.	69.50	0.222
25	0.76	1.346	134.60	23.63	21270.00	30450.00	30450.00	12350.	4.344	175.	46.67	0.332
26	6.50	1.345	143.30	22.61	24610.00	32350.00	34860.00	14060.	4.142	130.	31.56	0.244
27	0.46	1.346	145.70	22.19	27560.00	37850.00	35040.00	15320.	3.948	108.	27.58	0.255
28	0.30	1.321	156.60	20.05	32130.00	44540.00	45540.00	19150.	3.276	64.	25.92	0.307
29	0.50	1.301	163.50	19.51	57220.00	51640.00	53410.00	21430.	3.032	87.	28.33	0.332
30	2.30	1.275	173.00	16.26	42950.00	59520.00	61650.00	23960.	2.305	90.	32.58	0.359
31	2.36	1.355	176.80	15.41	42270.00	58880.00	57130.00	28100.	2.427	93.	36.51	0.414
32	0.36	1.311	183.20	15.44	56360.00	79320.00	61920.00	31300.	2.254	56.	42.79	0.446

## PERFORMANCE AVERAGES OVER MISSION PROFILE ( 1000 HOURS )

SPEED	15.76 KNOTS
EFFECTIVE POWER	7423. HP
SHAFT POWER	10220. HP
TURBINE POWER	16270. HP
TOTAL FUEL	4735. LBS/HR ( 0.134 TONS/MILE )
PROPELLION FUEL	4848. LBS/HR ( 0.137 TONS/MILE )

## AVERAGE ELECTRICAL LOAD ( 1000 HOURS )

PROPELLION COOLING	8. KW
GENERATOR LUBE SYSTEM	1. KW
HELIUM COMPRESSOR	130. KW
TOTAL LOAD	139. KW ( 111.3 LBS/HR )

## MISSION PROFILE SUMMARY - FIELDS FIXED AT 90 PERCENT - MAIN TURBINES ONLY

KTS	P/C TIME	SHAFT RPM	SPEED RATIO	EFFECTIVE HP	SHAFT HP	TURBINE HP	FUEL RATE (LPH)	RANGE (NM/TCN)	NAUT. MILES	TONS PER MILE	NO. OF TURBINES	PER THOUSAND HOURS			
												TCS	FUEL	TONS PER MILE	NO. OF TURBINES
1	1-10	1-450	5-09	291-10	1-40	1-92	11-27	11CC.	2-026	11-	5-80	0-527	1	MAIN	
2	1-20	1-450	10-16	143-40	11-20	15-59	24-56	1100-	4-073	24-	6-33	0-264	1	MAIN	
3	1-20	1-450	15-26	91-58	37-30	51-96	61-69	1100-	6-1C9	35-	6-33	0-176	1	MAIN	
4	1-20	1-450	20-35	61-50	39-60	123-20	132-90	1100-	8-145	48-	6-33	0-152	1	MAIN	
5	1-20	1-450	25-44	40-10	175-00	240-50	247-60	1131-	9-9C2	60-	6-49	0-108	1	MAIN	
6	1-20	1-450	30-53	26-14	302-40	415-70	427-40	1291-	10-410	72-	7-35	0-152	1	MAIN	
7	1-20	1-450	35-61	26-16	460-20	660-10	676-40	1430-	10-600	84-	3-56	0-108	1	MAIN	
8	1-20	1-450	40-70	26-21	716-30	935-30	1013-00	1695-	16-550	96-	9-53	0-089	1	MAIN	
9	1-20	1-450	45-79	22-25	1021-00	1493-00	1443-00	1948-	10-350	165-	10-87	0-101	1	MAIN	
10	1-20	1-450	50-88	20-29	1460-00	1924-00	1951-00	2230-	10-040	126-	12-39	0-103	1	MAIN	
11	6-30	1-450	55-97	20-32	1863-00	2561-00	2639-00	2547-	9-673	693-	72-95	0-107	1	MAIN	
12	6-70	1-450	61-05	20-36	2412-00	3325-00	3429-00	2906-	9-269	804-	65-21	0-111	1	MAIN	
13	7-00	1-450	66-14	20-40	3076-00	4226-00	4366-00	3291-	8-950	916-	105-48	0-116	1	MAIN	
14	7-10	1-450	71-23	20-43	3642-00	5280-00	5456-00	3724-	8-425	994-	120-69	0-121	1	MAIN	
15	6-50	1-450	76-32	20-47	4775-00	6495-00	6724-00	4192-	8-014	1020-	129-89	0-127	1	MAIN	
16	6-10	1-450	81-40	20-51	5754-00	7582-00	6172-00	4706-	7-613	976-	130-59	0-134	1	MAIN	
17	6-60	1-450	86-49	20-55	6875-00	9454-00	9816-00	5276-	7-225	1122-	157-80	0-141	1	MAIN	
18	7-20	1-450	91-58	20-58	8165-00	11220-00	11670-00	3291-	6-857	1225-	191-60	0-148	1	MAIN	
19	7-70	1-450	96-57	20-52	9603-00	13209-00	13750-00	6542-	6-505	1463-	228-00	0-156	1	MAIN	
20	8-90	1-450	101-60	20-36	11230-00	15390-00	16060-00	7259-	6-172	1780-	292-00	0-164	1	MAIN	
21	7-50	1-450	106-50	20-69	12630-00	17520-00	18420-00	8033-	5-256	1575-	272-10	0-173	1	MAIN	
22	4-30	1-450	111-50	20-36	14610-00	20450-00	21060-00	10190-	4-836	946-	32-21	0-209	2	MAIN	
23	1-50	1-450	117-00	20-35	17050-00	23410-00	24120-00	11120-	4-635	345-	75-06	0-218	2	MAIN	
24	1-30	1-450	122-10	20-42	19350-00	27420-00	26600-00	12110-	4-439	312-	70-35	0-227	2	MAIN	
25	0-70	1-450	127-20	20-42	21670-00	30270-00	31030-00	13180-	4-246	175-	41-50	0-237	2	MAIN	
26	0-50	1-450	132-30	20-44	24610-00	33820-00	34930-00	14330-	4-065	130-	32-21	0-249	2	MAIN	
27	0-40	1-450	137-40	20-46	27560-00	37280-00	39150-00	15560-	3-856	106-	27-96	0-259	2	MAIN	
28	0-20	1-450	143-70	20-45	32130-00	44400-00	45030-00	19240-	3-280	84-	25-92	0-309	3	MAIN	
29	0-30	1-450	148-10	20-53	37250-00	51750-00	53730-00	21540-	3-015	87-	29-03	0-333	3	MAIN	
30	0-30	1-450	156-50	20-55	42550-00	601C0-00	62400-00	24120-	2-787	90-	32-46	0-361	3	MAIN	
31	0-30	1-450	162-00	20-55	49260-00	69240-00	71590-00	28660-	2-466	93-	36-61	0-417	4	MAIN	
32	-0-30	1-450	169-50	20-59	56300-00	79520-00	82610-00	32150-	2-230	96-	43-24	0-450	4	MAIN	

## PERFORMANCE AVERAGES OVER MISSION PROFILE ( 1000 HOURS )

SPEED...\*\*\*\*\*  
 EFFECTIVE POWER... HP  
 SHAFT POWER... HP  
 TURBINE POWER... HP  
 TURBINE FUEL... LBS/HR. ( 0.155 TONS/MILE )  
 PROPULSION FUEL 5557-1 LBS/HR. ( 0.158 TONS/MILE )

C-30

C-30

SPEED...\*\*\*\*\*  
 EFFECTIVE POWER... HP  
 SHAFT POWER... HP  
 TURBINE POWER... HP  
 TURBINE FUEL... LBS/HR. ( 0.155 TONS/MILE )  
 PROPULSION FUEL 5557-1 LBS/HR. ( 0.158 TONS/MILE )

AVERAGE ELECTRICAL LOAD		PROPELLION COOLING	GENERATOR LUBE SYSTEM	HELIUM COMPRESSORS	KW
15-76	KNOTS				
7428-	HP				
10230-	HP				
1C610-	HP				
5420-	LBS/HR.	( 0.155 TONS/MILE )			
5557-	LBS/HR.	( 0.158 TONS/MILE )			
TOTAL LOAD.. 109. KW ( 87.1 LBS/HR )					

## ELECTRIC DRIVE SYSTEM

## MISSION PROFILE SUMMARY - FIELDS FIXED AT 90 PERCENT - MAIN + CRUISE TURBINES

KTS	PCT.	S/E RATIO	SHAFT HPN	SPEED RATIO	EFFECTIVE HP	SHAFT HP	TURBINE HP	FUEL RATE (PPH)	RANGE (NM/TON)	NAUT. MILES	TONS PER PILE	NC. OF TURBINES	PER THOUSAND HOURS	
													TENS. FUEL	NAUT. MILES
1.10	1.450	5.09	686.10	1.40	1.92	5.19	360.	6.222	11.	2.28	C.208	1	CRUISE	
1.2	1.450	10.15	326.10	11.20	15.39	18.88	260.	12.440	24.	2.49	C.104	1	CRUISE	
1.3	1.450	15.26	177.70	37.80	51.56	55.63	360.	18.670	36.	2.49	C.059	1	CRUISE	
1.4	1.450	20.35	57.90	69.60	123.29	127.60	409.	21.880	42.	2.75	C.057	1	CRUISE	
1.5	1.450	25.44	65.24	175.22	240.50	249.40	502.	22.300	60.	2.25	C.054	1	CRUISE	
1.6	1.450	30.53	65.52	302.40	415.70	431.00	617.	21.790	72.	3.87	C.054	1	CRUISE	
1.7	1.450	35.61	65.81	450.20	650.10	655.00	756.	20.750	94.	4.61	C.055	1	CRUISE	
1.8	1.450	40.70	65.99	716.40	985.30	1024.00	921.	19.460	96.	5.50	C.057	1	CRUISE	
1.9	1.450	45.79	69.37	1021.00	1403.00	1461.00	1116.	18.070	108.	6.54	C.061	1	CRUISE	
2.0	1.450	50.88	65.65	1400.00	1924.00	2028.00	1343.	16.680	120.	7.76	C.065	1	CRUISE	
2.1	1.450	55.97	65.94	1865.00	2561.00	2679.00	1607.	15.320	693.	4.20	C.070	1	CRUISE	
2.2	1.450	61.05	65.22	2412.00	3225.00	3486.00	1912.	14.020	904.	5.40	C.075	1	CRUISE	
2.3	1.450	66.14	60.50	3075.00	4228.00	4443.00	2263.	12.570	910.	7.12	C.081	1	CRUISE	
2.4	1.450	71.23	60.79	3542.00	5280.00	5564.00	2657.	11.760	956.	87.59	C.082	1	CRUISE	
2.5	1.450	76.32	69.23	4725.00	6495.00	6738.00	3654.	9.195	1020.	114.30	C.112	2	CRUISE	
2.6	1.450	81.40	61.40	5734.00	7382.00	8172.00	4705.	7.513	976.	131.20	C.134	1	MAIN	
2.7	1.450	86.49	60.51	6245.00	7832.00	8515.00	5270.	7.226	1122.	158.50	C.141	1	MAIN	
2.8	1.450	91.58	65.55	6973.00	8573.00	9545.00	5270.	7.226	1122.	158.50	C.141	1	MAIN	
2.9	1.450	96.67	62.67	7354.00	11220.00	11670.00	5830.	6.957	1296.	129.60	C.149	1	MAIN	
3.0	1.450	101.76	61.39	11220.00	15320.00	13750.00	6542.	6.505	1463.	228.90	C.153	1	MAIN	
3.1	1.450	106.85	60.56	12620.00	15320.00	16460.00	7259.	6.172	1750.	293.00	C.155	1	MAIN	
3.2	1.450	111.94	60.56	12620.00	17620.00	18620.00	8033.	5.953	1575.	272.90	C.173	1	MAIN	
3.3	1.450	117.03	65.55	16973.00	21090.00	21090.00	16160.	4.938	1976.	197.60	C.205	2	MAIN	
3.4	1.450	122.12	62.42	21870.00	26410.00	27430.00	12110.	4.635	345.	75.22	C.216	2	MAIN	
3.5	1.450	127.20	60.42	24270.00	30070.00	31030.00	13180.	4.438	312.	70.59	C.222	2	MAIN	
3.6	1.450	132.29	60.42	27470.00	32220.00	34930.00	14350.	4.248	175.	41.57	C.228	2	MAIN	
3.7	1.450	137.38	60.42	30670.00	36070.00	37130.00	15160.	4.055	130.	32.25	C.246	2	MAIN	
3.8	1.450	142.47	60.42	33870.00	39150.00	39150.00	15560.	3.863	106.	28.00	C.256	2	MAIN	
3.9	1.450	147.56	60.42	37070.00	42450.00	46040.00	16240.	3.674	70.	25.95	C.269	3	MAIN	
4.0	1.450	152.65	60.42	40270.00	44650.00	51750.00	21540.	3.015	87.	29.49	C.334	3	MAIN	
4.1	1.450	157.74	60.42	43470.00	60210.00	62420.00	24120.	2.767	90.	32.49	C.361	3	MAIN	
4.2	1.450	162.83	60.42	46670.00	69240.00	71640.00	26660.	2.465	95.	36.95	C.416	4	MAIN	
4.3	1.450	167.92	60.42	53870.00	75520.00	82810.00	32150.	2.230	96.	43.27	C.451	4	MAIN	

PERFORMANCE AVERAGES OVER MISSION PROFILE (1000 HOURS)

SPEED	KNOTS	AVERAGE ELECTRICAL LOAD
5.09	15.76	PROPELLION COOLING
1.450	7423.	GENERATOR LUBE SYSTEM
1.450	10230.	HELIUM COMPRESSORS
1.450	10630.	TOTAL LOAD.. 138. KW (111.5 LBS/HR)
1.450	50532.	( 0.144 TONS/MILE )
1.450	51944.	( 0.147 TONS/MILE )

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AVERAGE ELECTRICAL LOAD  
PROPELLSION COOLING  
GENERATOR LUBE SYSTEM  
HELIUM COMPRESSOR

COMPRESSOR S... 100. KH TOTAL LOAD 110 KW ( 87.71 AS/HB )

## ELECTRIC DRIVE SYSTEM

REF. NO. 1

## MISSION PROFILE SUMMARY - MAIN + CRUISE - NEAREST 10 PERCENT MAGNET FIELD

KTS	PCT.	P/D	TIME	SHAFT RPN	SPEED RATIO	EFFECTIVE HP	SHAFT HP	TURBINE HP	FUEL RATE (PPH)	RANGE (NM/TON)	NAUT. MILES	TONS PER MILE	NO. OF TURBINES	PER THOUSAND HOURS	
														FUEL	TONS
1	1.10	1.450	5.05	58.6-00	1.40	1.92	5.19	360-	6.222	11-	2.28	0.208	1	CRUISE	
2	1.20	1.450	10.18	32.5-00	11.20	15.39	18.88	350-	12.440	24-	2.49	0.104	1	CRUISE	
3	1.29	1.450	15.26	17.7-40	37.80	51.96	55.62	360-	18.570	36-	2.49	0.069	1	CRUISE	
4	1.29	1.450	20.35	11.3-10	39.60	121.20	126.40	405-	22.090	48-	2.73	0.057	1	CRUISE	
5	1.29	1.450	25.44	11.3-50	175.-00	240.-00	250.-30	492-	22.760	50-	3.20	0.053	1	CRUISE	
6	1.29	1.450	30.53	11.3-00	302.-00	41.5.-00	432.-30	529-	22.420	72-	3.77	0.052	1	CRUISE	
7	1.29	1.450	35.51	11.4-20	450.-00	66.0.-10	68.0.-60	730-	21.480	84-	4.47	0.053	1	CRUISE	
8	1.29	1.450	40.50	11.4-50	71.6.-60	92.5.-50	102.6.00	887.-	20.260	96-	5.32	0.055	1	CRUISE	
9	1.29	1.450	45.49	11.4-90	192.1.-00	1403.-00	1464.-00	1075.-	16.750	108-	6.33	0.059	1	CRUISE	
10	1.29	1.450	50.48	11.5-30	1924.-00	2012.-00	2129.-	1299.-	17.250	120-	7.53	0.063	1	CRUISE	
11	6.30	1.450	55.47	11.5-60	1363.-00	2561.-00	2683.-00	1564.-	15.750	670-	46.99	0.068	1	CRUISE	
12	6.70	1.450	61.05	10.1-50	2419.-00	3225.-00	3458.-00	1877.-	14.320	804-	56.26	0.074	1	CRUISE	
13	7.00	1.450	66.64	10.1-90	3076.-00	4228.-00	4446.-00	2232.-	13.050	910-	73.00	0.080	2	CRUISE	
14	7.10	1.450	71.23	10.2-30	3077.-00	5250.-00	5561.-00	2567.-	11.750	964-	87.29	0.085	2	CRUISE	
15	6.29	1.450	75.52	6.5-20	4725.-00	5495.-00	6733.-00	3554.-	9.195	1050-	114.70	0.112	2	CRUISE	
16	6.10	1.450	81.40	6.0-45	5734.-00	7382.-00	8182.-00	4292.-	8.530	975-	117.40	0.120	2	CRUISE	
17	5.50	1.450	85.49	5.0-82	6878.-00	9454.-00	9841.-00	4723.-	8.063	1122-	142.40	0.127	2	MAIN	
18	7.22	1.450	91.58	3.0-87	8155.-00	11220.-00	11700.-00	5295.-	7.615	1296-	173.50	0.134	2	MAIN	
19	7.70	1.450	96.67	3.0-93	9403.-00	13200.-00	13730.-00	5929.-	7.179	1463-	207.70	0.142	1	MAIN	
20	8.60	1.450	101.30	3.0-98	104.-30	15390.-00	16100.-00	5650.-	6.757	1730-	256.00	0.151	1	MAIN	
21	7.50	1.450	106.30	3.0-04	1256.-00	17820.-00	18650.-00	7495.-	6.352	1575-	251.00	0.159	1	MAIN	
22	4.20	1.450	111.40	3.0-00	14910.-00	20460.-00	21490.-00	8284.-	5.963	945-	161.00	0.170	1	MAIN	
23	1.50	1.450	117.50	2.5-20	17930.-00	23410.-00	24190.-00	10850.-	4.755	345-	345.50	0.212	2	MAIN	
24	1.30	1.450	122.10	2.6-23	19350.-00	26600.-00	27490.-00	11950.-	4.534	312-	59.51	0.223	2	MAIN	
25	0.70	1.450	127.20	2.2-97	21870.-00	32070.-00	31250.-00	12950.-	4.324	175-	40.85	0.233	2	MAIN	
26	0.50	1.450	132.30	2.2-00	24610.-00	35820.-00	34960.-00	14110.-	4.128	130-	31.77	0.244	2	MAIN	
27	0.40	1.450	137.40	2.5-02	17930.-00	23410.-00	24190.-00	10850.-	4.056	108-	27.65	0.256	2	MAIN	
28	0.30	1.450	143.50	2.0-48	32130.-00	44200.-00	46020.-00	12940.-	3.933	103-	25.95	0.269	3	MAIN	
29	0.30	1.450	148.50	2.0-53	37230.-00	51750.-00	53730.-00	13150.-	3.815	105-	26.40	0.274	3	MAIN	
30	0.30	1.450	153.50	2.0-57	43950.-00	60010.-00	62400.-00	14120.-	3.787	100-	32.49	0.361	3	MAIN	
31	0.30	1.450	158.00	1.8-49	46290.-00	69240.-00	71920.-00	28850.-	2.407	93-	36.84	0.413	4	MAIN	
32	0.30	1.450	169.60	1.8-53	56330.-00	79520.-00	82730.-00	32040.-	2.237	96-	43.13	0.449	4	MAIN	

## PERFORMANCE AVERAGES OVER MISSION PROFILE ( 1000 HOURS )

SPEED	15.70	KNOTS
EFFECTIVE POWER	7425.-	HP
SHAFT POWER	15230.-	HP
TURBINE POWER	10670.-	HP
TURBINE FUEL	14720.-	LBS/HR
PROPELLION FUEL	4632.-	LBS/HR

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PERFORMANCE AVERAGES OVER MISSION PROFILE ( 1000 HOURS )

AVERAGE ELECTRICAL LOAD	9.56
PROPELLION COOLING	9.56
GENERATOR LUBE SYSTEM	1.00
HELIUM COMPRESSORS	130. KW
TOTAL LOAD	140. KW (112.0 LBS/HR)

## ELECTRIC DRIVE SYSTEM

## MISSION PROFILE SUMMARY - MAIN ONLY - FIXED FIELDS

KTS	PCT.	TIME	P/D RATIO	SHAFT RPM	SPEED RATIO	EFFECTIVE HP	SHAFT HP	TURBINE HP	FUEL RATE (PPH)	RANGE (NM/TCN)	NAUT. MILES	TONS FUEL	TONS PER MILE	NO. OF TURBINES	PER THOUSAND HOURS		
1	1-10	1-450	5.89	291.10	1.40	1.92	11.27	1100.	2.036	11.	5.80	0.527	1	MAIN			
1	1-20	1-450	10.15	143.60	1.15	1.20	15.39	24.96	4.673	24.	6.23	0.264	1	MAIN			
3	1-20	1-450	15.26	91.54	3.780	51.96	61.69	1100.	6.1C9	36.	6.33	0.176	1	MAIN			
4	1-20	1-450	20.35	61.72	39.60	123.20	132.90	1100.	9.145	48.	6.23	0.132	1	MAIN			
5	1-20	1-450	25.44	50.15	175.30	240.40	243.80	1102.	10.160	60.	6.34	0.106	1	MAIN			
6	1-20	1-450	30.54	30.24	302.40	415.70	429.20	1236.	10.860	72.	7.06	0.099	1	MAIN			
7	1-20	1-450	35.64	30.24	306.20	660.10	691.00	1397.	11.230	84.	7.92	0.094	1	MAIN			
8	1-20	1-450	40.74	45.70	350.34	716.80	805.30	1616.60	1581.	11.340	96.	8.90	0.093	1	MAIN		
9	1-20	1-450	45.84	45.76	1921.60	1423.00	1448.00	1791.	11.460	105.	10.03	0.093	1	MAIN			
10	1-20	1-450	50.93	50.63	1469.00	1454.00	1537.00	2030.	11.640	120.	11.21	0.094	1	MAIN			
11	1-20	1-450	56.03	56.43	1853.50	2561.60	2647.00	2799.	10.740	692.	66.95	0.097	1	MAIN			
12	1-20	1-450	61.12	56.49	1853.50	2413.00	3325.00	3440.00	2602.	10.320	804.	80.31	0.100	1	MAIN		
13	1-20	1-450	66.22	61.05	306.54	2076.00	4228.00	4378.00	2941.	9.901	91.5.	94.51	0.104	1	MAIN		
14	1-20	1-450	71.32	66.14	36.60	2076.00	5280.00	5475.00	3319.	9.449	99.4	107.20	0.109	1	MAIN		
15	1-20	1-450	76.42	71.25	74.65	36.60	6475.00	6742.00	3739.	8.956	1020.	116.15	0.114	1	MAIN		
16	1-20	1-450	81.52	76.71	86.32	4725.00	7652.00	8193.00	4209.	8.522	97.6.	116.50	0.120	1	MAIN		
17	1-20	1-450	86.62	81.40	86.32	5734.00	7652.00	9454.00	4723.	8.063	112.	141.70	0.126	1	MAIN		
18	1-20	1-450	91.72	91.56	91.56	50.87	11220.00	11700.00	5295.	7.615	129.6	173.00	0.134	1	MAIN		
19	1-20	1-450	96.82	96.57	96.57	96.93	9603.00	12200.00	13730.00	5929.	7.179	146.3	206.90	0.141	1	MAIN	
20	1-20	1-450	101.92	101.60	101.60	101.60	12200.00	15390.00	16100.00	6630.	6.757	178.0	267.10	0.150	1	MAIN	
21	1-20	1-450	107.02	106.80	106.80	106.80	12970.00	17820.00	18660.00	7405.	6.352	1575.	251.10	0.159	1	MAIN	
22	1-20	1-450	112.12	111.85	111.85	111.85	14910.00	20490.00	21490.00	8264.	5.963	94.6.	160.50	0.170	1	MAIN	
23	1-20	1-450	117.22	117.00	117.00	117.00	23130.00	23410.00	24160.00	10320.	4.761	34.5.	73.39	0.212	2	MAIN	
24	1-20	1-450	122.32	122.10	122.10	122.10	12650.00	26600.00	27470.00	11630.	4.545	31.2.	69.21	0.222	2	MAIN	
25	1-20	1-450	127.42	126.50	126.50	126.50	12650.00	30070.00	31070.00	12920.	4.334	175.	45.48	0.232	2	MAIN	
26	1-20	1-450	132.52	132.30	132.30	132.30	24610.00	32820.00	34580.00	14100.	4.130	130.	31.70	0.244	2	MAIN	
27	1-20	1-450	137.62	137.40	137.40	137.40	27560.00	37630.00	39200.00	15380.	3.932	108.	27.65	0.256	2	MAIN	
28	1-20	1-450	142.72	142.50	142.50	142.50	31650.00	44400.00	46030.00	19240.	3.260	84.	25.92	0.309	3	MAIN	
29	1-20	1-450	147.82	147.50	147.50	147.50	37250.00	51750.00	53730.00	21540.	3.015	87.	26.00	0.333	3	MAIN	
30	1-20	1-450	152.92	152.50	152.50	152.50	42750.00	65010.00	62400.00	26120.	2.767	90.	32.46	0.361	3	MAIN	
31	1-20	1-450	158.02	158.00	158.00	158.00	48250.00	69240.00	71990.00	28260.	2.406	93.	36.82	0.417	4	MAIN	
32	1-20	1-450	163.12	163.00	163.00	163.00	54300.00	82910.00	82920.00	32150.	2.230	96.	43.24	0.450	4	MAIN	

## PERFORMANCE AVERAGES OVER MISSION PROFILE ( 1000 HOURS )

SPEED  
EFFECTIVE POWER  
SHAFT POWER  
TURBINE POWER  
TURBINE FUEL  
PROPULSION FUEL

AVERAGE ELECTRICAL LOAD

PROPELLER COOLING

GENERATOR LUBE SYSTEM

HELIUM COMPRESSORS

TOTAL LOAD = 110. KW ( 87.7 LBS/HR )



## ELECTRIC DRIVE SYSTEM

REF-N.C. SCI-1

## MISSION PROFILE SUMMARY - SINGLE CRUISE TURBINE

RTS	PCT.	TIME	P/D RATIO	SHAFT RPM	SPEED RATIO	EFFECTIVE HP	SHAFT HP	TURBINE HP	FUEL RATE (LPH)	RANGE (NM/TCN)	HAUL MILES	TONS FUEL	TONS PER MILE	PER THOUSAND HOURS		NO. OF TURBINES
														TURBINE FUEL RATE (LPH)		
1	1-10	1-450	5.00	686.10	1.40	1.92	1.40	5.19	360.	6.222	1.1	2.28	C-2CE	1	CRUISE	
2	1-20	1-450	10-10	375.70	1.20	2.0	1.39	16.88	300.	12.410	2.4	2.49	C-104	1	CRUISE	
3	1-20	1-450	15-10	237.70	1.20	2.0	1.56	55.63	360.	16.670	3.6	2.49	C-063	1	CRUISE	
4	1-20	1-450	20-10	103.60	1.20	2.0	69.60	126.30	405.	22.110	4.6	2.75	C-057	1	CRUISE	
5	1-20	1-450	25-10	149.70	1.20	2.0	24.60	250.30	462.	22.760	5.0	2.20	C-053	1	CRUISE	
6	1-20	1-450	30-10	115.20	1.20	2.0	302.40	415.70	412.50	22.440	7.2	3.77	O-052	1	CRUISE	
7	1-20	1-450	35-10	115.60	1.20	2.0	480.20	656.10	637.20	21.500	94.	4.47	C-053	1	CRUISE	
8	1-20	1-450	40-10	119.20	1.20	2.0	716.50	935.30	1027.00	20.210	95.	5.31	C-055	1	CRUISE	
9	1-20	1-450	45-10	117.70	1.20	2.0	1021.00	1403.00	1454.00	16.750	105.	6.32	C-059	1	CRUISE	
10	1-20	1-450	50-10	115.20	1.20	2.0	1400.00	1904.00	2012.00	12.990	17.50	7.53	C-063	1	CRUISE	
11	1-20	1-450	55-10	115.20	1.20	2.0	1263.00	2561.00	2681.00	15.630	15.770	6.95	O-055	1	CRUISE	
12	1-20	1-450	60-10	122.20	1.20	2.0	2419.00	3325.00	3440.00	1872.	14.360	5.920	C-074	1	CRUISE	
13	1-20	1-450	65-10	121.70	1.20	2.0	2076.00	4226.00	4447.00	2231.	13.350	910.	C-050	1	CRUISE	

\* \* INSUFFICIENT DATA FOR FULL MISSION PROFILE \* \* \*

## PERFORMANCE AVERAGES OVER MISSION PROFILE ( 215 HOURS )

SPEED..... 5.61 KNOTS  
 EFFECTIVE POWER..... 1710. HP  
 SHAFT POWER..... 2351. HP  
 TURBINE POWER..... 2467. HP  
 TURBINE FUEL..... 1437. LBS/HR ( 0.067 TONS/MILE )  
 PROPULSION FUEL..... 1563. LBS/HR ( 0.072 TONS/MILE )

AVERAGE ELECTRICAL LOAD  
 PROPULSION COOLING... 1. KW  
 GENERATOR LUBE SYSTEM... 0. KW  
 HELIUM COMPRESSORS... 130. KW  
 TOTAL LOAD... 131. KW ( 104.8 LBS/HR )

## SINGLE CRUISE TURBINE

TURBINE SP/FTD	SP/FTD (KNOTS)	SHAFT RPM	TURBINE RPM	FUEL RATE	P/D	PROP. EFF.	TURBINE EFF.	DRIVE EFF.	TOTAL EFF.	SPEED FIELD RATIO	PERCENT BUSS FIELD VOLTAGE	MOTOR AMPS	MOTOR VOLTS
CRUISE 1.000	5.09	393.86	744.87	1.4500	72.75	0.41	91.09	0.27	76.40	100.00	6.31	92.27	LF
CRUISE 1.000	5.09	393.86	744.87	1.4500	72.75	0.41	91.09	0.27	76.40	92.43	16.64	92.27	LF
CRUISE 2.000	9.97	605.64	232.71	1.4500	72.75	2.72	94.70	1.57	85.09	92.28	79.48	24.92	LF
CRUISE 3.000	16.18	5.64	336.13	1.4500	72.75	7.64	95.51	5.21	69.28	79.48	24.92	79.92	LF
CRUISE 3.000	15.26	5.64	405.31	1.4500	72.75	14.95	92.97	16.44	103.78	72.77	33.34	140.51	LF
CRUISE 4.000	22.35	15.50	271.53	1.4500	72.75	24.03	98.02	16.60	114.84	69.16	41.71	21.68	74
CRUISE 5.000	25.44	24.83	292.14	1.4500	72.75	32.75	95.11	25.85	116.23	67.26	50.09	21.44	71
CRUISE 6.000	30.53	35.76	360.93	1.4500	72.75	34.11	95.11	25.85	116.23	50.09	42.73	42	LF
CRUISE 7.000	35.61	48.67	425.77	1.4500	72.75	44.51	96.95	31.10	119.55	66.85	56.46	55.74	88
CRUISE 8.000	40.70	63.57	4653.68	1.4500	72.75	54.71	95.75	38.19	119.25	67.24	66.99	55.74	88
CRUISE 9.000	45.79	80.45	5350.26	1.4500	72.75	64.34	92.32	44.65	117.72	66.33	75.31	70.49	97
CRUISE 10.000	50.88	96.33	5892.31	1.4500	72.75	73.17	95.66	50.92	115.23	59.99	63.74	84.96	91
CRUISE 11.000	55.97	120.18	6263.21	1.4500	72.75	82.93	95.43	56.33	112.22	72.12	92.19	105.15	69
CRUISE 12.000	61.06	145.05	6658.72	1.4500	72.75	92.03	95.28	61.05	100.55	74.07	100.55	125.08	11
CRUISE 13.000	66.14	167.50	6946.92	1.4500	72.75	94.16	95.28	65.13	105.02	77.55	106.12	146.73	26
CRUISE 14.000	71.23	194.59	7207.92	1.4500	72.75	99.41	94.35	68.60	101.19	80.74	117.61	170.11	17

LF = FUEL BELOW MINIMUM REQUIRED RATE  
 HF = FUEL ABOVE MAXIMUM FUEL RATE  
 HS = TURBINE SPEED EXCESSIVE  
 HFS = TURBINE FUEL AND SPEED EXCESSIVE

## SINGLE CRUISE TURBINE

TURBINE CONFIG.	SPEED (KNOTS)	SHAFT RPM	SHEET TPS (TH-LB-FT)	TURBINE FUEL RATE	P/D RATIO	PROP. EFF.	TURBINE EFF.	DRIVE EFF.	TOTAL EFF.	PERCENT FIELD VOLTAGE	MOTOR AMPS
1 CRUISE	1.00	5.09	3490.66	360.00	1.4500	.72-.75	0.58	.37-.40	0.19	686.09	5.31
1 CRUISE	2.00	10.18	3.97	3316.76	360.00	1.4500	.72-.75	2.48	81.55	1.47	326.15
1 CRUISE	3.00	15.26	3.94	2712.58	360.00	1.4500	.72-.75	93.40	4.98	44.40	24.93
1 CRUISE	4.00	20.35	15.89	2012.73	405.21	1.4500	.72-.75	14.86	95.97	10.44	108.73
1 CRUISE	5.00	25.44	24.82	2321.29	482.88	1.4500	.72-.75	24.83	96.95	16.82	114.34
1 CRUISE	6.00	30.53	35.76	3609.31	595.32	1.4500	.72-.75	34.11	26.11	23.85	116.25
1 CRUISE	7.00	35.61	48.67	4257.73	729.30	1.4500	.72-.75	44.51	95.85	31.10	119.55
1 CRUISE	8.00	40.70	63.57	4853.68	836.56	1.4500	.72-.75	54.71	95.95	38.19	119.25
1 CRUISE	9.00	45.79	80.45	5380.26	1074.88	1.4500	.72-.75	61.34	95.82	44.65	117.72
1 CRUISE	10.00	50.88	99.43	5865.31	1298.86	1.4500	.72-.75	73.17	95.66	50.92	115.28
1 CRUISE	11.00	55.97	120.18	6230.24	1592.55	1.4500	.72-.75	81.09	95.46	56.33	112.22
1 CRUISE	12.00	60.05	143.03	6563.72	1671.68	1.4500	.72-.75	82.08	95.28	61.05	108.74
1 CRUISE	13.00	65.14	167.68	6545.02	2230.81	1.4500	.72-.75	94.16	95.02	55.13	105.02
1 CRUISE	14.00	71.23	194.62	7207.52	2645.16	1.4500	.72-.75	99.41	94.86	63.50	101.19
								80.74		80.74	117.51
											17011.17 HS

LF = FUEL BELOW MINIMUM REQUIRED RATE

HF = FUEL ABOVE MAXIMUM FUEL RATE

HS = TURBINE SPEED EXCESSIVE

HFS = TURBINE FUEL AND SPEED EXCESSIVE

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## MISSION PROFILE SUMMARY - TWO CRUISE TURBINES

KTS TIME	PCT. TIME	P/D RATIO	SHAFT RPM	SPEED RATIO	EFFECTIVE HP	SHAFT HP	TURBINE HP	FUEL RATE (PPH)	RANGE (NM/TON)	NAUT. MILES	TONS PER MILE	NO. OF TURBINES	PER THOUSAND HOURS	
													TURBINE HR	FUEL TONS PER MILE
1	1-10	1-450	5-C9	683.40	1-43	1-92	2-35	720.	3-111	11-	4-05	0-365	2	CRUISE
2	1-20	1-450	10-18	336.10	11-20	15-39	22-04	720.	6-222	24-	4-42	0-184	2	CRUISE
3	1-20	1-450	15-26	207.90	37-90	51-96	58-76	720.	5-333	36-	4-42	0-123	2	CRUISE
4	1-20	1-450	20-35	122.00	89-60	123-20	128-70	720.	12-440	48-	4-42	0-092	2	CRUISE
5	1-20	1-450	25-44	86-32	175-00	240-50	249-10	804.	13-923	60-	4-43	0-081	2	CRUISE
6	1-20	1-450	30-53	90-06	302-40	415-70	429-80	937.	14-340	72-	5-59	0-078	2	CRUISE
7	1-20	1-450	35-61	92-70	480-20	660-10	662-00	1095.	14-220	84-	6-43	0-077	2	CRUISE
8	1-20	1-450	40-70	94-19	715-60	935-30	1016-00	1279.	14-010	96-	7-42	0-077	2	CRUISE
9	1-20	1-450	45-79	94-72	1021-00	1403-00	1449-00	1495.	13-490	108-	8-58	0-079	2	CRUISE
10	1-20	1-450	50-83	94-49	1400-00	1924-00	1963-00	1744.	12-840	120-	9-91	0-083	2	CRUISE
11	6-30	1-450	55-97	92-63	1262-00	2551-00	2645-00	2031.	12-130	693.	50-14-	0-087	2	CRUISE
12	6-70	1-450	60-05	92-23	2415-00	3525-00	3440-00	2251.	11-230	824.	73-84	0-092	2	CRUISE
13	7-00	1-450	65-14	90-37	3076-00	4225-00	4377-00	2735.	10-640	916.	83-94	0-095	2	CRUISE
14	7-10	1-450	71-23	88-58	3242-00	5230-00	5471-00	3166.	9-504	103-00	8-104	0-104	2	CRUISE
15	6-20	1-450	73-32	86-39	4725-00	6495-00	6735-00	3651.	9-203	1020-	114-20	0-112	2	CRUISE
16	6-10	1-450	81-40	94-06	5734-00	7982-00	8184-00	4197.	8-540	976.	117-30	0-120	2	CRUISE
17	6-60	1-450	86-49	81-76	6876-00	9454-00	9828-00	4808.	7-919	1122.	145-00	0-129	2	CRUISE

\* \* INSUFFICIENT DATA FOR FULL MISSION PROFILE \* \* \*

## PERFORMANCE AVERAGES OVER MISSION PROFILE ( 555 HOURS )

SPEED..... 12.27 KNOTS  
 EFFECTIVE POWER..... 5322. HP  
 SHAFT POWER..... 4556. HP  
 TURBINE POWER... 4726. HP  
 TURBINE FUEL... 2814. LBS/HR ( 0.102 TONS/MILE )  
 PROPULSION FUEL 2921. LBS/HR ( 0.106 TONS/MILE )

AVERAGE ELECTRICAL LOAD  
 PROPULSION COOLING... 2. KW  
 GENERATOR LUBE SYSTEM 1. KW  
 HELIUM COMPRESSORS... 130. KW  
 TOTAL LOAD.. 133. KW ( 106.5 LBS/HR )

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## TWO CRUISE TURBINES

REF-NO. 501-2

TURBINE	SPEED (NUTS)	SHAFT RPM	SHIFT TRQ (TH.IR-FT)	TURBINE RATE	FJF	P/R	PROP. RATIO	TURBINE EFF.	DRIVE EFF.	TOTAL EFF.	PERCENT BUSS FIELD VOLTAGE	MOTOR AMPS.
2 CRUISE	1.00	5.79	0.69	358.26	431.40	1.4533	72.75	0.21	89.13	0.14	78.28	100.00
2 CRUISE	2.00	10.18	1.57	796.00	532.64	1.4533	72.75	1.45	93.37	6.59	78.42	100.00
2 CRUISE	3.00	15.26	8.04	1156.21	602.78	1.4533	72.75	4.25	95.59	2.96	76.57	100.00
2 CRUISE	4.00	20.35	15.69	1673.31	693.25	1.4533	72.75	3.71	96.29	6.11	80.25	98.08
2 CRUISE	5.00	25.44	24.83	2168.32	804.45	1.4533	72.75	14.63	96.59	10.26	86.32	91.57
2 CRUISE	6.00	30.53	35.76	937.53	1.4533	72.75	21.65	95.71	15.24	90.06	87.72	50.09
2 CRUISE	7.00	35.61	43.67	3391.55	1094.90	1.4533	72.75	29.42	96.73	20.70	85.36	59.48
2 CRUISE	8.00	40.70	63.57	3833.65	1279.49	1.4533	72.75	37.57	96.31	26.46	94.19	66.89
2 CRUISE	9.00	45.79	80.45	4737.44	1494.60	1.4533	72.75	45.80	96.31	32.26	94.72	83.86
2 CRUISE	10.00	50.88	99.33	4807.36	1747.95	1.4533	72.75	53.36	96.78	37.62	94.49	64.22
2 CRUISE	11.00	55.97	125.13	5240.19	2031.37	1.4533	72.75	61.57	96.73	45.33	95.15	92.19
2 CRUISE	12.00	61.05	143.03	5634.52	2361.29	1.4533	72.75	68.81	96.57	48.40	92.23	86.54
2 CRUISE	13.00	66.14	167.85	5940.48	2738.03	1.4533	72.75	75.51	96.30	53.66	90.57	88.34
2 CRUISE	14.00	71.23	194.65	6305.36	3156.38	1.4533	72.75	81.62	96.51	57.31	88.53	90.49
2 CRUISE	15.00	76.32	222.48	5593.23	3550.95	1.4533	72.75	87.15	96.42	61.13	86.39	92.95
2 CRUISE	16.00	81.40	254.27	6644.65	4195.57	1.4533	72.75	92.12	96.54	66.54	95.96	93.65
2 CRUISE	17.00	86.48	287.05	7255.57	4506.45	1.4533	72.75	96.54	95.23	67.57	81.70	98.64
2 CRUISE	18.00	91.56	321.62	7343.66	5453.09	1.4533	72.75	100.45	96.37	70.21	86.74	101.69

LF = FUEL BELOW MINIMUM REQUIRED RATE

HF = FUEL ABOVE MAXIMUM FUEL RATE

HS = TURBINE SPEED EXCESSIVE

HFS = TURBINE FUEL AND SPEED EXCESSIVE

C-40

## TWO CRUISE TURBINES

TURBINE CONFIG.	SPEED (KNOTS)	SHAFT RPM	SHFT. (TH-LB-FT)	TURBINE RPM	FUEL RATE	P/D RATIO	PROP. EFF.	TURBINE FOW	DRIVE EFF.	TOTAL EFF.	PERCENT FIELD	BUSS VOLTAGE	MOTOR AMPS
1 CRUISE	1.00	5.09	0.55	3502.53	720.00	1.4500	72.75	0.55	23.04	0.03	65.44	11.37	92.27
2 CRUISE	2.00	10.19	3.97	3419.57	720.00	1.4500	72.75	1.45	65.84	0.73	33.6.05	16.64	357.27
2 CRUISE	3.00	15.26	8.94	3172.57	720.00	1.4500	72.75	3.86	88.42	2.45	20.7.86	37.80	795.02
2 CRUISE	4.00	20.35	15.89	2483.51	720.00	1.4500	72.75	8.51	54.98	5.83	12.2.03	64.50	145.51
2 CRUISE	5.00	25.44	24.85	2183.32	804.46	1.4500	72.75	14.63	66.56	10.28	8.6.02	61.67	2168.74
2 CRUISE	6.00	30.53	35.76	2749.35	937.53	1.4500	72.75	21.66	56.71	15.24	9.0.03	27.72	50.09
2 CRUISE	7.00	35.61	43.67	3301.55	1094.90	1.4500	72.75	29.42	96.78	20.72	92.70	65.23	4273.42
2 CRUISE	8.00	40.70	63.57	3832.55	1270.49	1.4500	72.75	37.57	56.81	25.46	94.19	66.60	5574.83
2 CRUISE	9.00	45.79	80.45	4337.44	1494.60	1.4500	72.75	45.80	95.81	32.26	94.72	63.86	7049.07
2 CRUISE	10.00	50.88	97.33	4607.39	1743.90	1.4500	72.75	52.66	56.76	37.92	94.49	83.74	8596.01
2 CRUISE	11.00	55.97	120.18	5240.19	2031.39	1.4500	72.75	61.57	96.73	43.33	93.63	85.15	92.19
2 CRUISE	12.00	61.05	143.03	5634.52	2361.29	1.4500	72.75	68.61	66.67	48.40	92.29	96.54	100.65
2 CRUISE	13.00	66.14	167.86	5690.48	2738.08	1.4500	72.75	75.51	96.60	53.06	96.57	88.34	102.12
2 CRUISE	14.00	71.23	194.68	6509.36	3156.38	1.4500	72.75	81.62	56.51	57.31	80.56	90.49	117.61
2 CRUISE	15.00	76.32	223.48	6593.23	3650.96	1.4500	72.75	87.15	96.42	61.13	86.36	62.95	125.11
2 CRUISE	16.00	81.40	254.27	6844.65	4196.67	1.4500	72.75	92.12	96.31	64.54	84.06	95.68	134.63
2 CRUISE	17.00	86.49	287.05	7056.57	4808.45	1.4500	72.75	96.54	56.20	67.57	91.70	98.64	143.15
2 CRUISE	18.00	91.58	321.82	5493.09	1.4500	72.75	100.45	95.07	7C.21	80.74	100.00	151.69	28390.15 HS

LF = FUEL &amp; GELCO MINIMUM REQUIRED RATE

HF = FUEL ABOVE MAXIMUM FUEL RATE

HS = TURBINE SPEED EXCESSIVE

HFS = TURBINE FUEL AND SPEED EXCESSIVE

C-41

## ELECTRIC DRIVE SYSTEM

## MISSION PROFILE SUMMARY - ONE MAIN TURBINE

KTS	PCT.	P/D	TIME	SHAFT RPM	SPEED RATIO	EFFECTIVE HP	SHAFT HP	TURBINE HP	FUEL RATE (PPH)	RANGE (NM/TCN)	NAUT. MILES	TONS FUEL	TONS PER MILE	PER THOUSAND HOURS	
														NO. OF TURBINES	NO. OF CF
1	1-10	1-450		5-C9	251-10	1-40	1-92	11-27	1100-	2-036	11-	5-80	0-527	1	MAIN
2	1-20	1-450	10-18	145-40	11-20	15-39	24-96	1100-	4-073	24-	6-33	0-264	1	MAIN	
3	1-20	1-450	15-26	61-59	37-20	51-54	61-70	1100-	6-1C9	26-	6-33	0-176	1	MAIN	
4	1-20	1-450	20-35	61-81	86-60	123-20	132-90	1100-	8-145	48-	6-33	0-132	1	MAIN	
5	1-20	1-450	25-44	29-56	175-50	240-50	248-70	1102-	10-170	60-	6-34	0-106	1	MAIN	
6	1-20	1-450	30-53	31-24	302-40	415-70	425-40	1235-	12-360	72-	7-06	0-958	1	MAIN	
7	1-20	1-450	35-61	32-60	450-20	660-10	681-80	1395-	11-240	64-	7-91	0-354	1	MAIN	
8	1-20	1-450	40-70	33-57	71-6-80	985-30	1018-00	1576-	11-370	96-	8-88	0-392	1	MAIN	
9	1-20	1-450	45-79	34-23	1321-00	1403-00	1450-00	1763-	11-310	108-	9-99	0-392	1	MAIN	
10	1-20	1-450	50-86	34-52	1400-00	1524-00	1691-00	2018-	11-1C0	120-	11-25	0-394	1	MAIN	
11	6-30	1-420	-	55-97	57-79	1563-00	1652-00	2284-	10-790	693-	66-54	0-396	1	MAIN	
12	6-70	1-450	61-05	34-77	2419-00	3225-00	3446-00	2384-	10-4C0	604-	79-76	0-299	1	MAIN	
13	7-00	1-450	66-14	34-52	3675-00	4226-00	4335-00	2921-	9-969	410-	93-61	0-102	1	MAIN	
14	7-10	1-450	71-13	34-27	3942-00	5265-00	5462-00	3299-	9-5C6	994-	107-23	0-108	1	MAIN	
15	6-80	1-450	76-32	33-84	4725-00	6495-00	6750-00	3721-	9-029	1320-	115-50	0-113	1	MAIN	
16	6-10	1-450	81-40	33-33	5734-00	7582-00	8201-00	4191-	8-551	976-	116-50	0-119	1	MAIN	
17	6-52	1-450	86-49	32-75	6576-00	9454-00	9844-00	4713-	8-079	1122-	141-40	0-126	1	MAIN	
18	7-20	1-450	91-56	32-11	7165-00	11230-00	11700-00	5291-	7-521	1296-	172-60	0-133	1	MAIN	
19	7-70	1-450	96-67	31-44	8635-00	13206-00	13730-00	5928-	7-179	1463-	206-90	0-141	1	MAIN	
20	8-90	1-450	101-80	30-75	11290-30	15390-00	15100-00	6629-	6-758	1790-	267-00	0-150	1	MAIN	
21	7-50	1-450	106-30	30-54	12970-00	17820-00	18660-00	7398-	6-359	1575-	250-80	0-159	1	MAIN	
22	4-30	1-450	111-90	29-32	14910-00	20490-00	21480-00	9238-	5-982	946-	166-00	0-169	1	MAIN	

\* # INSUFFICIENT DATA FOR FULL MISSION PROFILE \*\*\*

## PERFORMANCE AVERAGES OVER MISSION PROFILE ( 941 HOURS )

SPEED ----- KNOTS  
 SPEED POWER 6250- HP  
 SHAFT POWER 8350- HP  
 TURBINE POWER 2663- HP  
 TURBINE FUEL 4329- LBS/HP  
 PROPULSION FUEL 4415- LBS/HP

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PERFORMANCE AVERAGES OVER MISSION PROFILE ( 941 HOURS )

AVERAGE ELECTRICAL LOAD  
 PROPULSION COOLING... 7. KW  
 GENERATOR LUBE SYSTEM 1. KW  
 HELIUM COMPRESSORS... 100. KW  
 TOTAL LOAD... 106. KW ( 26.4 LBS/HR )

## ONE MAIN TURBINE

REF. NO. 501-3

TURBINE CONFIG.	SPFED (KNOTS)	SHAFT RPM	SHIFT TRQ (Lb-Lb-FT)	TURBINE RPM	FUEL RATE	P/R	PROP. EFF.	TURBINE DRIVE EFF.	TOTAL EFF.	PERCENT FIELD VOLTAGE	MOTOR AMPS
1 MAIN	1.00	5.09	0.99	91.37	754.24	1.4500	72.75	0.11	91.21	17.96	100.00
1 MAIN	2.00	10.18	3.67	207.33	811.63	1.4500	72.75	0.75	94.36	20.38	88.32
1 MAIN	3.00	15.26	6.34	370.18	889.44	1.4500	72.75	0.32	95.94	24.25	74.32
1 MAIN	4.00	20.35	15.89	553.73	936.11	1.4500	72.75	4.94	96.50	2.47	66.37
1 MAIN	5.00	25.44	24.63	720.43	1101.81	1.4500	72.75	5.61	96.66	29.50	61.33
1 MAIN	6.00	30.53	35.76	954.41	1237.60	1.4500	72.75	13.23	95.73	9.32	31.26
1 MAIN	7.00	35.61	49.67	1160.97	1395.02	1.4500	72.75	18.64	95.31	13.13	32.60
1 MAIN	8.00	40.70	63.57	1366.30	1575.97	1.4500	72.75	24.64	96.73	17.35	33.57
1 MAIN	9.00	45.79	80.45	1567.29	1762.67	1.4500	72.75	31.03	96.73	21.84	34.23
1 MAIN	10.00	50.88	96.33	1761.52	2017.64	1.4500	72.75	37.63	95.57	26.46	34.62
1 MAIN	11.00	55.97	120.18	1947.11	2283.65	1.4500	72.75	44.29	95.59	21.12	34.79
1 MAIN	12.00	61.05	143.03	2122.72	2583.73	1.4500	72.75	50.85	95.31	35.71	34.77
1 MAIN	13.00	66.14	167.86	2281.45	2921.07	1.4500	72.75	57.25	95.42	41.16	34.58
1 MAIN	14.00	71.23	194.68	2440.81	3299.09	1.4500	72.75	63.38	95.32	44.41	34.27
1 MAIN	15.00	76.32	223.48	2582.63	3721.32	1.4500	72.75	69.13	95.22	46.43	33.84
1 MAIN	16.00	81.40	254.27	2713.02	4141.49	1.4500	72.75	74.63	95.11	52.18	33.33
1 MAIN	17.00	86.49	287.05	2812.28	4713.41	1.4500	72.75	79.69	95.30	55.66	32.75
1 MAIN	18.00	91.58	321.82	2940.92	5290.98	1.4500	72.75	84.37	95.39	56.66	32.11
1 MAIN	19.00	96.67	358.57	3039.53	5528.21	1.4500	72.75	89.67	95.77	61.78	31.44
1 MAIN	20.00	101.76	357.30	3128.76	6629.11	1.4500	72.75	92.62	95.55	64.44	30.75
1 MAIN	21.00	106.84	438.03	3209.33	7397.77	1.4500	72.75	96.13	95.53	66.64	30.04
1 MAIN	22.00	111.93	460.74	3281.95	8238.31	1.4500	72.75	99.44	95.40	69.01	29.32
1 MAIN	23.00	117.02	525.43	3347.31	9154.85	1.4500	72.75	102.39	95.27	70.56	28.60

LF = FUEL BELOW MINIMUM REQUIRED RATE  
 HF = FUEL ABOVE MAXIMUM FUEL RATE  
 HS = TURBINE SPEED EXCESSIVE  
 HFS = TURBINE FUEL AND SPEED EXCESSIVE

## ONE MAIN TURBINE

TURBINE CONFIG.	SPEED (KNOTS)	SHAFT RPM	SHIFT TRQ (TH-LB-FT)	TURBINE RPM	FUEL RATE	P/D RATIO	PROP. EFF.	TURBINE FOM	DRIVE EFF.	TOTAL EFF.	PERCENT FIELD	BUSS VOLTAGE	MOTOR AMPS
1 MAIN	1.00	5.00	0.99	1481.14	1100.00	1.4500	72.75	0.39	17.07	0.05	251.12	6.17	92.27
1 MAIN	2.00	10.00	10.18	1459.49	1100.00	1.4500	72.75	0.67	61.57	0.39	143.43	17.54	16.64
1 MAIN	3.00	15.00	15.26	1397.97	1100.00	1.4500	72.75	2.14	84.22	1.31	91.59	17.63	24.98
1 MAIN	4.00	20.00	20.35	15.89	1100.00	1.4500	72.75	4.61	92.68	3.11	61.81	26.21	33.34
1 MAIN	5.00	25.00	25.44	750.43	1101.81	1.4500	72.75	8.61	96.71	6.06	29.50	61.33	41.71
1 MAIN	6.00	30.00	30.53	954.41	1237.60	1.4500	72.75	13.23	96.79	9.32	31.26	57.57	50.09
1 MAIN	7.00	35.00	35.61	48.67	1160.97	1395.02	1.4500	72.75	18.64	96.81	13.12	32.60	58.48
1 MAIN	8.00	40.00	40.70	63.57	1356.30	1575.97	1.4500	72.75	24.64	96.78	17.35	33.57	56.19
1 MAIN	9.00	45.00	45.79	80.45	1567.29	1732.67	1.4500	72.75	31.03	96.72	21.84	34.23	53.25
1 MAIN	10.00	50.00	50.88	99.33	1761.52	2017.64	1.4500	72.75	37.63	96.67	26.46	34.62	52.73
1 MAIN	11.00	55.00	55.97	120.16	1947.11	2283.66	1.4500	72.75	44.29	96.59	31.12	34.79	52.57
1 MAIN	12.00	60.00	61.65	143.03	2122.72	2593.73	1.4500	72.75	50.56	96.51	35.71	34.77	52.70
1 MAIN	13.00	65.00	66.14	167.86	2287.45	2921.07	1.4500	72.75	57.25	96.42	40.16	34.58	53.05
1 MAIN	14.00	70.00	71.23	154.68	2440.21	3299.05	1.4500	72.75	62.38	96.32	44.41	34.27	53.67
1 MAIN	15.00	75.00	76.32	223.43	2582.63	3721.32	1.4500	72.75	65.18	96.22	48.43	32.84	54.44
1 MAIN	16.00	80.00	81.40	254.27	2713.02	4191.49	1.4500	72.75	74.63	96.11	52.18	33.33	55.38
1 MAIN	17.00	85.00	86.49	287.05	2832.28	4713.41	1.4500	72.75	79.69	96.00	55.66	32.75	56.47
1 MAIN	18.00	90.00	91.52	321.82	2940.92	5230.93	1.4500	72.75	84.37	95.89	58.86	32.11	57.63
1 MAIN	19.00	95.00	96.57	358.57	3039.53	5928.21	1.4500	72.75	89.67	95.77	61.78	31.44	59.02
1 MAIN	20.00	100.00	101.76	357.30	3128.76	6529.11	1.4500	72.75	92.60	95.65	64.44	30.75	60.46
1 MAIN	21.00	105.00	106.84	438.03	3209.33	7397.77	1.4500	72.75	96.18	95.53	66.94	30.04	62.00
1 MAIN	22.00	110.00	111.93	420.74	3281.95	8238.31	1.4500	72.75	99.44	95.40	69.01	26.32	52.63
1 MAIN	23.00	115.00	117.02	525.43	3347.31	9154.85	1.4500	72.75	102.39	95.27	70.96	28.60	45.34

L.F. = FUEL BELOW MINIMUM REQUIRED RATE  
 H.F. = FUEL ABOVE MAXIMUM FUEL RATE  
 H.S. = TURBINE SPEED EXCESSIVE  
 H.F.S. = TURBINE FUEL AND SPEED EXCESSIVE

## ELECTRIC DRIVE SYSTEM

## MISSION PROFILE SUMMARY - TWO MAIN TURBINES

KTS	PCT.	TIME	P/D	SHAFT RPM	SPEED RATIO	EFFECTIVE HP	SHAFT HP	TURBINE HP	FUEL RATE (PPH)	RANGE (NM/TQNS)	NAUT. MILES	TONS PER MILE	PER THOUSAND HOURS		
													TONS		
														FUEL	NO. OF TURBINES
1	1.10	1.450	5.09	251.40	1.40	1.92	20.53	2200.	1.018	11.	11.21	1.019	2	MAIN	
2	1.20	1.450	10.18	144.70	11.20	15.39	34.28	2400.	2.036	24.	12.22	0.509	2	MAIN	
3	1.20	1.450	15.25	54.50	37.90	51.96	71.05	2200.	3.055	36.	12.22	C.340	2	MAIN	
4	1.20	1.450	20.35	67.87	89.60	123.20	142.20	2200.	4.073	48.	12.22	C.255	2	MAIN	
5	1.20	1.450	25.44	49.74	175.00	240.50	259.10	2200.	5.091	60.	12.22	0.264	2	MAIN	
6	1.20	1.450	30.53	23.15	302.40	415.70	432.50	2200.	6.109	72.	12.22	C.170	2	MAIN	
7	1.20	1.450	35.61	24.21	480.20	650.10	675.20	2347.	6.680	84.	13.01	C.155	2	MAIN	
8	1.20	1.450	40.70	25.19	716.80	935.30	1013.00	2577.	6.953	96.	14.25	C.143	2	MAIN	
9	1.20	1.450	45.79	25.96	1321.00	1403.00	1442.00	2835.	7.111	108.	15.63	C.145	2	MAIN	
10	1.20	1.450	50.89	26.56	1400.00	1924.00	1978.00	3122.	7.174	120.	17.17	C.143	2	MAIN	
11	6.30	1.450	55.97	27.00	1863.00	2561.00	2632.00	3442.	7.159	693.	99.12	0.143	2	MAIN	
12	6.70	1.450	61.05	27.31	2419.00	3325.00	3418.00	3795.	7.082	804.	116.00	0.144	2	MAIN	
13	7.00	1.450	66.14	27.49	3076.00	4226.00	4346.00	4186.	6.957	910.	133.40	C.147	2	MAIN	
14	7.10	1.450	71.23	27.55	3842.00	5260.00	5430.00	4616.	6.753	994.	149.00	C.150	2	MAIN	
15	5.80	1.450	76.32	27.55	4725.00	4950.00	6680.00	5090.	6.602	1020.	157.10	C.154	2	MAIN	
16	6.10	1.450	81.40	27.45	5734.00	7832.00	8110.00	5609.	6.390	976.	155.10	0.159	2	MAIN	
17	5.60	1.450	86.49	27.23	6378.00	9454.00	9731.00	6177.	6.165	1122.	184.50	C.164	2	MAIN	
18	7.20	1.450	91.55	27.05	8165.00	11220.00	11560.00	6798.	5.932	1296.	221.30	0.171	2	MAIN	
19	7.70	1.450	96.67	25.77	5603.00	13200.00	13600.00	7474.	5.694	1463.	260.00	C.178	2	MAIN	
20	6.90	1.450	101.80	26.45	11200.00	15390.00	15870.00	8211.	5.456	1780.	222.80	C.185	2	MAIN	
21	7.50	1.450	106.80	26.09	12970.00	17820.00	18380.00	9011.	5.220	1575.	304.70	C.193	2	MAIN	
22	4.30	1.450	111.90	25.71	14910.00	20490.00	21140.00	9878.	4.989	946.	191.40	0.202	2	MAIN	
23	1.50	1.450	117.00	25.30	17030.00	23410.00	24170.00	10620.	4.763	345.	73.05	C.212	2	MAIN	
24	1.30	1.450	122.10	24.86	19150.00	26600.00	27470.00	11830.	4.545	312.	69.20	C.222	2	MAIN	
25	0.70	1.450	127.20	24.44	21970.00	30070.00	31070.00	12920.	4.334	175.	40.68	0.232	2	MAIN	
26	0.50	1.450	132.30	24.00	24610.00	33820.00	34970.00	14090.	4.132	130.	31.68	C.244	2	MAIN	
27	0.40	1.450	137.40	23.55	27560.00	37880.00	39190.00	15350.	3.939	108.	27.60	0.256	2	MAIN	

\*\*\* INSUFFICIENT DATA FOR FULL MISSION PROFILE \*\*\*

PERFORMANCE AVERAGES OVER MISSION PROFILE ( 985 HOURS )

SPEED..... KNOTS  
 EFFECTIVE POWER..... HP  
 SHAFT POWER..... HP  
 TURBINE POWER..... HP  
 TURBINE FUEL..... LBS/HR  
 PROPULSION FUEL..... LBS/HR

15.54  
 6378.  
 9453.  
 9741.  
 5999.  
 6085.

NO. OF TURBINES  
 2  
 2  
 2  
 2  
 2  
 2

AVERAGE ELECTRICAL LOAD  
 PROPULSION COOLING..... KW  
 GENERATOR LUBE SYSTEM..... KW  
 HELIUM COMPRESSORS..... 100.  
 TOTAL LOAD... 108. KW ( 36.1 LBS/HR )

## TWO MAIN TURBINES

TURBINE CONFIG.	SPEED (KNOTS)	SHAFT RPM	SHIFT TFO (TH-1R-FTI)	TURBINE RPM	FUEL RATE	P/D RATE	PROP. EFF.	TURBINE EFF.	DRIVE EFF.	TOTAL EFF.	SPEED RATIO	PERCENT FIELD	BUSS VOLTAGE
2 MAIN	1.00	5.09	0.99	91.29	1495.34	1.4500	72.75	0.05	82.13	0.04	17.94	100.00	8.31
2 MAIN	2.00	10.18	3.97	182.76	1573.07	1.4500	72.75	0.43	94.39	0.27	17.96	100.00	16.64
2 MAIN	3.00	15.26	8.64	274.41	1577.85	1.4500	72.75	1.23	95.79	0.86	17.96	100.00	24.73
2 MAIN	4.00	20.35	15.89	460.79	1809.38	1.4500	72.75	2.69	96.47	1.69	19.69	91.38	33.34
2 MAIN	5.00	25.44	24.93	547.29	1964.54	1.4500	72.75	4.82	96.35	3.40	21.51	63.74	41.71
2 MAIN	6.00	30.53	35.76	702.10	2143.54	1.4500	72.75	7.62	97.05	5.28	23.00	76.41	50.09
2 MAIN	7.00	35.61	48.67	862.24	2347.31	1.4500	72.75	11.04	97.13	7.80	24.21	74.56	58.48
2 MAIN	8.00	40.70	63.57	1025.17	2577.21	1.4500	72.75	14.93	97.25	10.61	25.19	71.74	66.87
2 MAIN	9.00	45.79	80.45	1168.79	2834.89	1.4500	72.75	19.43	97.23	13.73	25.95	69.57	75.31
2 MAIN	10.00	50.83	99.33	1361.25	3122.31	1.4500	72.75	24.15	97.33	17.10	26.56	69.17	83.74
2 MAIN	11.00	55.97	120.18	1511.12	3441.56	1.4500	72.75	29.17	97.39	20.65	27.03	67.42	92.19
2 MAIN	12.00	61.05	143.03	1667.07	3795.35	1.4203	72.75	34.35	97.22	24.31	27.31	66.44	100.55
2 MAIN	13.00	66.14	167.86	1816.08	4185.99	1.4500	72.75	39.50	97.27	28.02	27.49	66.06	109.07
2 MAIN	14.00	71.23	194.68	1963.37	4516.40	1.4500	72.75	44.86	97.25	31.74	27.56	65.55	117.61
2 MAIN	15.00	76.32	223.43	2102.30	5089.55	1.4500	72.75	50.03	97.22	35.41	27.55	66.05	126.11
2 MAIN	16.00	81.43	254.27	2234.45	5608.59	1.4500	72.75	55.15	97.19	39.20	27.45	66.36	134.63
2 MAIN	17.00	86.49	287.05	2359.53	6176.77	1.4500	72.75	60.39	97.15	42.47	27.23	66.83	143.21
2 MAIN	18.00	91.56	321.62	2437.40	6797.51	1.4500	72.75	64.84	97.12	45.61	27.05	67.46	151.69
2 MAIN	19.00	96.67	358.57	2548.05	7474.32	1.4500	72.75	69.33	97.33	49.03	26.77	66.24	150.25
2 MAIN	20.00	101.76	397.30	2691.53	8210.82	1.4500	72.75	73.73	97.23	52.03	26.45	69.13	153.82
2 MAIN	21.00	106.84	438.03	2788.03	9010.63	1.4503	72.75	77.73	96.99	54.88	26.09	70.15	143.25
2 MAIN	22.00	111.93	480.74	2877.75	9877.70	1.4503	72.75	81.62	96.94	57.56	25.71	71.27	155.99
2 MAIN	23.00	117.02	525.43	2960.98	10815.57	1.4503	72.75	85.22	96.39	60.07	25.30	72.45	154.60
2 MAIN	24.00	122.11	572.17	3036.03	11828.47	1.4500	72.75	88.53	96.33	62.49	24.38	73.79	203.22
2 MAIN	25.00	127.19	626.16	3104.22	12619.95	1.4500	72.75	91.72	95.73	64.58	24.44	75.15	54.29
2 MAIN	26.00	132.28	671.44	3174.92	14094.15	1.4500	72.75	94.63	96.72	66.59	24.39	76.50	220.50
2 MAIN	27.00	137.37	724.09	3235.45	15354.91	1.4500	72.75	97.34	96.56	68.45	23.55	78.17	229.16
2 MAIN	28.00	143.62	811.51	3315.97	17377.27	1.4500	72.36	100.95	95.53	70.52	23.06	79.94	240.05

C-46

LF = FUEL BELOW MINIMUM REQUIRED RATE  
 HF = FUEL ABOVE MAXIMUM FUEL RATE  
 HS = TURBINE SPEED EXCESSIVE  
 HFS = TURBINE FUEL AND SPEED EXCESSIVE

## TWO MAIN TURBINES

TURBINE CONFIG.	SPEED (KNOTS)	SHAFT RPM	SHFT TRQ (THLB-FT)	TURBINE RPM	FUEL RATE	P/D RATIO	PROP. EFF.	TURBINE FDN	DRIVE EFF.	TOTAL EFF.	PERCENT BUSS FIELD	MOTOR AMP
2 MAIN	5.09	0.99	1482.72	2200.00	1.4500	72.75	0.36	9.37	0.02	291.43	6.16	8.31
2 MAIN	10.18	3.97	1471.61	2200.00	1.4500	72.75	0.55	44.91	0.15	144.65	12.42	16.64
2 MAIN	15.26	8.94	1442.35	2200.00	1.4500	72.75	1.23	72.12	0.66	94.50	19.02	24.98
2 MAIN	20.35	15.89	1381.24	2200.00	1.4500	72.75	2.47	85.59	1.95	67.87	26.52	33.34
2 MAIN	25.44	24.83	1265.34	2200.00	1.4500	72.75	4.49	92.83	3.03	49.74	36.22	41.71
2 MAIN	30.53	35.76	1011.99	2200.00	1.4500	72.75	7.50	96.11	5.24	33.15	54.40	50.09
2 MAIN	35.61	48.67	862.24	2347.31	1.4500	72.75	11.04	97.18	7.80	24.21	74.56	58.48
2 MAIN	40.70	63.57	1025.17	2577.21	1.4500	72.75	14.95	97.25	16.61	25.19	71.74	66.89
2 MAIN	45.79	80.45	1188.79	2934.89	1.4500	72.75	19.40	97.28	13.73	25.96	69.67	75.31
2 MAIN	50.88	99.33	1351.28	3122.31	1.4500	72.75	24.16	97.30	17.10	26.55	63.17	83.74
2 MAIN	55.97	120.18	1511.12	3441.66	1.4500	72.75	29.17	97.30	20.65	27.00	67.12	92.19
2 MAIN	61.05	143.03	1667.07	3795.35	1.4500	72.75	34.35	97.29	24.31	27.31	66.44	106.55
2 MAIN	66.14	167.85	1818.08	4185.99	1.4500	72.75	39.60	97.27	23.02	27.49	66.36	109.12
2 MAIN	71.23	194.68	1963.37	4616.40	1.4500	72.75	44.86	97.25	31.74	27.56	65.95	117.61
2 MAIN	76.32	223.49	2102.30	5089.56	1.4500	72.75	50.05	97.22	35.41	27.55	66.05	126.11
2 MAIN	81.40	254.27	2234.45	5608.59	1.4500	72.75	55.15	97.19	39.00	27.45	66.36	134.63
2 MAIN	86.49	287.65	2359.53	6176.77	1.4500	72.75	60.05	97.16	42.47	27.28	66.93	143.15
2 MAIN	91.58	321.62	2477.40	6797.51	1.4500	72.75	64.84	97.12	45.81	27.05	67.46	151.69
2 MAIN	96.63	358.57	2596.05	7474.32	1.4500	72.75	69.38	97.08	49.00	26.77	63.24	160.25
2 MAIN	101.76	357.30	2691.53	8210.82	1.4500	72.75	73.70	97.03	52.02	26.45	65.13	168.82
2 MAIN	106.84	438.03	2788.03	9010.68	1.4500	72.75	77.78	96.99	54.88	26.09	70.15	177.60
2 MAIN	111.93	480.74	2877.75	9877.70	1.4500	72.75	81.62	96.94	57.56	25.71	71.27	185.79
2 MAIN	117.02	525.43	2960.93	10815.67	1.4500	72.75	85.22	96.85	60.07	25.30	72.43	194.60
2 MAIN	122.11	572.12	3036.03	11828.47	1.4500	72.75	88.58	96.83	62.40	24.86	73.79	203.22
2 MAIN	127.19	523.79	3109.22	12919.98	1.4500	72.75	91.72	96.78	64.58	24.44	75.18	211.85
2 MAIN	132.28	671.46	3174.52	14094.15	1.4500	72.75	94.63	96.72	66.59	24.03	76.64	220.50
2 MAIN	137.37	724.99	3235.46	15354.91	1.4500	72.75	97.34	96.66	63.45	23.55	78.18	229.16
2 MAIN	142.48	811.51	3315.97	17377.27	1.4500	72.36	100.96	96.53	70.52	23.08	79.64	240.05

LF = FUEL BELOW MINIMUM REQUIRED RATE

HF = FUEL ABOVE MAXIMUM FUEL RATE

HS = TURBINE SPEED EXCESSIVE

HFS = TURBINE FUEL AND SPEED EXCESSIVE

## ELECTRIC DRIVE SYSTEM

## MISSION PROFILE SUMMARY - THREE MAIN TURBINES

PER THOUSAND HOURS

KTS	PCT. TIME	P/O RATIO	SHAFT RPM	SPEED RATIO	EFFECTIVE HP	SHAFT HP	TURBINE HP	FUEL RATE (PPH)	RANGE (NM/TCN)	NAUT. MILES	TONS FUEL	TONS PER MILE	NO. OF TURBINES
1	1.10	1.450	5-C9	291.50	1.4C	1.92	26.80	3300.	0.679	11.	16.61	1.510	3 MAIN
2	1.20	1.450	1C-18	145.10	11.20	15.39	43.62	3300.	1.358	24.	18.12	1.755	3 MAIN
3	1.20	1.450	15-26	95.42	37.80	51.96	80.54	3300.	2.036	36.	18.12	0.5C3	3 MAIN
4	1.20	1.450	20-35	69.63	99.50	123.20	151.90	3300.	2.715	48.	18.12	0.378	3 MAIN
5	1.20	1.450	25-44	52.05	175.00	240.50	269.20	3300.	3.394	60.	18.12	0.302	3 MAIN
6	1.20	1.450	30-53	4C.07	302.40	415.70	443.50	3300.	4.073	72.	18.12	0.252	3 MAIN
7	1.20	1.450	35-61	25.75	450.20	650.10	595.20	3300.	4.752	84.	18.12	0.216	3 MAIN
8	1.20	1.450	40-70	21.16	716.90	995.30	1015.00	3518.	5-C54	96.	19.25	0.202	3 MAIN
9	1.20	1.450	45-79	21.62	1021.00	1403.00	1444.00	3517.	5-282	108.	20.89	0.193	3 MAIN
10	1.20	1.450	50-88	22.54	1400.00	1924.00	1981.00	4147.	5-4C1	120.	22.66	0.182	3 MAIN
11	6-30	1.450	55-97	23.04	1963.00	2561.00	2636.00	4511.	5-4.62	623.	129.20	0.186	3 MAIN
12	6-70	1.450	61-05	23.43	2419.00	3225.00	3423.00	4511.	5-473	804.	149.43	0.183	3 MAIN
13	7-00	1.450	66-14	23.72	3076.00	4228.00	4352.00	53-9.	5-444	910.	169.86	0.197	3 MAIN
14	7-10	1.450	71-23	23.92	3542.00	5230.00	5437.00	5827.	5-382	994.	187.49	0.189	3 MAIN
15	6-80	1.450	76-32	24.05	4725.00	6495.00	6639.00	6348.	5-293	1020.	195.30	0.191	3 MAIN
16	6-10	1.450	81-40	24.10	5734.30	7582.00	8121.00	6915.	5-183	976.	190.70	0.195	3 MAIN
17	6-60	1.450	86-49	24.09	6878.00	9454.00	9744.00	7532.	5-056	1122.	224.50	0.203	3 MAIN
18	7-20	1.450	91-58	24.03	9165.00	11220.00	11570.00	8200.	4-917	1296.	266.40	0-206	3 MAIN
19	7-70	1.450	96-67	23.92	9603.00	13200.00	13610.00	8524.	4-769	1463.	309.50	0-212	3 MAIN
20	8-90	1.450	1C1-8.0	23.77	11263.00	15395.00	15890.00	9707.	4-615	1780.	389.70	0-219	3 MAIN
21	7-50	1.450	1C5-10	23.57	12970.00	17620.00	18400.00	10550.	4-458	1575.	356.40	0-226	3 MAIN
22	4-30	1.450	111-9.3	23.35	14910.00	20490.00	21170.00	11430.	4-299	946.	221.80	0-235	3 MAIN
23	1-50	1.450	117-0.0	23.10	17030.00	23410.00	24200.00	12440.	4-140	345.	93.97	0-243	3 MAIN
24	1-20	1.450	122-1.0	22.83	19350.00	26600.00	27510.00	13500.	3-983	312.	78.50	0-253	3 MAIN
25	C-70	1.450	127-2.0	22.53	21870.00	30070.00	31110.00	14630.	3-828	1775.	46.03	0-263	3 MAIN
26	0-50	1.450	132-3.0	22.22	24610.00	33820.00	35010.00	15640.	3-676	130.	35.59	0-274	3 MAIN
27	C-40	1.450	137-4.0	21.91	27560.00	37860.00	39250.00	17140.	3-529	108.	30.79	0-285	3 MAIN
28	0-50	1.450	143-7.0	21.60	32130.00	44400.00	46050.00	19210.	3-265	140.	43.13	0-306	3 MAIN
29	0-50	1.450	150-1.0	21.25	37250.00	51750.00	53750.00	21570.	3-017	145.	48.31	0-333	3 MAIN
30	0-50	1.450	156.50	20.87	42950.00	6CC10.00	62410.00	24110.	2.787	150.	54.09	0.361	3 MAIN

## PERFORMANCE AVERAGES OVER MISSION PROFILE ( 1000 HOURS )

SPEED.....	15.74	KNOTS
EFFECTIVE POWER	7336.	HP
SHAFT POWER....	1C90.	HP
TURBINE POWER...	1C420.	HP
TURBINE FUEL....	7526.	LBS/HR ( 0.213 TONS/MILE )
PROPELLSION FUEL	7614.	LBS/HR ( 0.216 TONS/MILE )

AVERAGE ELECTRICAL LOAD	7. KW
PROPELLSION COOLING...	7. KW
GENERATOR LUBE SYSTEM	3. KW
HELIUM COMPRESSORS....	100. KW
TOTAL LOAD..	110. KW ( 87.6 LBS/HR )

## THREE MAIN TURBINES

TURBINE CONFIG.	SPEED (KNOTS)	SHAFT RPM	SHFT TRQ (LBS-IR-FT)	TURBINE RPM	FUEL RATE	P/D RATE	PROP. EFF.	TURBINE FWD	DRIVE EFF.	TOTAL EFF.	SPEED FIELD	PERCENT FIELD	BUSS VOLTAGE	MOTOR AMPS
3 MAIN	1.50	5.09	0.99	91.29	2236.45	1.4500	.72.75	0.27	92.24	10.32	92.27	LF	8.31	10.31
3 MAIN	2.00	10.12	3.67	182.76	2333.94	1.4500	72.75	0.18	17.95	100.00	16.64	LF	357.27	16.64
3 MAIN	2.50	15.12	8.64	274.41	2459.00	1.4500	72.75	0.85	16.93	100.00	24.98	LF	357.27	24.98
3 MAIN	3.00	15.76	15.89	366.24	2512.64	1.4500	72.75	1.87	95.93	100.00	33.34	LF	1405.51	33.34
3 MAIN	4.00	20.35	8.00	458.26	2795.92	1.4500	72.75	3.40	90.20	100.00	41.71	LF	2168.74	41.71
3 MAIN	5.00	25.44	24.83	584.72	3008.71	1.4500	72.75	5.44	95.33	100.00	50.09	LF	3144.71	50.09
3 MAIN	6.00	30.53	35.76	584.72	3249.12	1.4500	72.75	7.95	96.58	100.00	58.43	LF	4273.42	58.43
3 MAIN	7.00	35.61	48.67	721.11	3518.03	1.4500	72.75	11.00	91.37	100.00	66.39	LF	5574.83	66.39
3 MAIN	8.00	40.70	63.57	361.32	3816.95	1.4500	72.75	14.43	97.15	100.00	7049.07	7049.07		
3 MAIN	9.00	45.75	80.45	1003.69	5826.80	1.4500	72.75	16.22	97.15	100.00	8696.31	8696.31		
3 MAIN	10.00	50.83	69.73	116.79	4147.48	1.4500	72.75	17.67	97.15	100.00	92.19	LF	10515.69	92.19
3 MAIN	11.00	55.97	120.18	126.35	4511.43	1.4500	72.75	22.29	97.16	100.00	100.65	LF	12508.11	100.65
3 MAIN	12.00	61.05	143.03	1450.34	4911.11	1.4500	72.75	26.53	97.16	100.00	109.38	LF	14573.26	109.38
3 MAIN	13.00	66.14	167.66	1568.80	5348.71	1.4500	72.75	31.03	97.14	100.00	117.61	LF	17011.17	117.61
3 MAIN	14.00	71.23	184.68	1703.93	5826.80	1.4500	72.75	35.59	97.12	100.00	125.11	LF	19521.93	125.11
3 MAIN	15.00	76.32	223.44	1832.24	6348.67	1.4500	72.75	40.19	97.09	100.00	134.63	LF	22205.21	134.63
3 MAIN	16.00	81.40	251.27	1962.05	6915.36	1.4500	72.75	44.79	97.08	100.00	143.15	LF	25001.31	143.15
3 MAIN	17.00	86.49	287.05	2084.01	7531.70	1.4500	72.75	49.34	97.03	100.00	151.69	LF	28090.15	151.69
3 MAIN	18.00	91.58	321.62	2204.42	8200.23	1.4500	72.75	53.82	96.93	100.00	160.25	LF	31241.82	160.25
3 MAIN	19.00	96.67	358.57	2312.28	8924.23	1.4500	72.75	58.19	96.95	100.00	176.36	LF	34666.17	176.36
3 MAIN	20.00	101.76	397.30	2418.26	9707.07	1.4500	72.75	62.42	96.91	100.00	194.40	LF	36213.25	194.40
3 MAIN	21.00	106.84	439.03	2513.70	10552.27	1.4500	72.75	66.50	96.83	100.00	212.49	LF	41933.10	212.49
3 MAIN	22.00	111.93	480.74	2613.81	11463.42	1.4500	72.75	70.42	96.76	100.00	23.35	LF	45025.68	23.35
3 MAIN	23.00	117.02	525.43	2703.39	12444.13	1.4500	72.75	74.16	96.76	100.00	25.10	LF	49590.99	25.10
3 MAIN	24.00	122.11	572.12	2787.22	13458.78	1.4500	72.75	77.72	96.71	100.00	26.83	LF	54129.05	26.83
3 MAIN	25.00	127.19	620.79	2860.18	14629.54	1.4500	72.75	81.10	96.66	100.00	22.53	LF	58571.85	22.53
3 MAIN	26.00	132.28	671.44	2940.13	15841.67	1.4500	72.75	84.23	95.50	100.00	22.33	LF	62050.50	22.33
3 MAIN	27.00	137.37	724.09	3009.28	17138.99	1.4500	72.75	87.33	95.35	100.00	21.91	LF	66447.16	21.91
3 MAIN	28.00	143.68	811.51	3102.30	19211.71	1.4500	72.36	91.42	95.42	100.00	21.60	LF	70732.75	21.60
3 MAIN	29.00	150.66	905.68	3188.44	21528.77	1.4500	71.97	95.22	95.22	100.00	20.87	HF	75929.25	20.87
3 MAIN	30.00	156.51	1008.66	3260.55	24113.36	1.4500	71.58	98.72	98.72	100.00	20.47	HF	87734.25	20.47
3 MAIN	31.00	163.03	1115.27	3337.52	25930.12	1.4500	71.19	101.92	101.92	100.00	90.03	HF	97169.25	90.03

C-49

LF = FUEL BELOW MINIMUM REQUIRED RATE  
 HF = FUEL ABOVE MAXIMUM FUEL RATE  
 HS = TURBINE SPEED EXCESSIVE  
 HFS = TURBINE FUEL AND SPEED EXCESSIVE

## THREE MAIN TURBINES

REF. NO. 501-5

TURBINE CONFIG.	SPEED (KNOTS)	SHAFT RPM	SHFT TRQ (TH-LB-FT)	TURBINE RPM	FUEL RATE	P/D RATIO	PROP. EFF.	TURBINE EFF.	DRIVE EFF.	TOTAL EFF.	PERCENT FIELD SPEED	BUSSE VOLTAGE	MOTOR AMPS	
3 MAIN	1.00	5.99	1483.25	3300.00	1.4500	72.75	C.34	6.46	0.02	231.53	6.31	92.27		
3 MAIN	2.00	10.18	1476.00	3300.00	1.4500	72.75	0.50	35.29	C.13	145.05	12.38	15.64	357.27	
3 MAIN	3.00	15.26	1456.46	3300.00	1.4500	72.75	C.93	64.51	0.44	95.42	13.84	24.93		
3 MAIN	4.00	20.35	1417.07	3300.00	1.4500	72.75	1.76	81.07	1.04	45.83	25.85	33.34	1405.51	
3 MAIN	5.00	25.44	1346.87	3300.00	1.4500	72.75	2.11	86.37	2.02	52.65	34.92	41.71	2138.74	
3 MAIN	6.00	30.53	1223.33	3300.00	1.4500	72.75	5.13	93.72	3.50	43.07	45.00	50.09	3144.71	
3 MAIN	7.00	35.61	952.73	3300.00	1.4500	72.75	7.92	96.32	5.55	26.75	57.47	56.48	4275.42	
3 MAIN	8.00	40.70	661.32	3516.08	1.4500	72.75	11.00	57.07	7.77	21.16	65.23	66.85	5574.83	
3 MAIN	9.00	45.79	60.45	1003.69	1.4500	72.75	14.43	97.13	10.20	21.92	82.51	75.31	7049.07	
3 MAIN	10.00	50.88	59.23	1146.79	4147.46	1.4500	72.75	18.22	97.13	12.87	22.54	80.32	83.74	6666.01
3 MAIN	11.00	55.97	122.16	1289.36	4511.48	1.4500	72.75	22.29	97.16	15.75	23.04	72.66	52.19	12515.69
3 MAIN	12.00	61.05	143.03	1430.34	4911.11	1.4500	72.75	26.58	97.16	18.79	23.43	77.43	66.65	12553.11
3 MAIN	13.00	66.14	167.86	1555.80	5348.71	1.4500	72.75	31.03	97.14	21.93	23.72	76.55	109.12	14673.26
3 MAIN	14.00	71.23	194.68	1703.98	5826.80	1.4500	72.75	35.59	97.12	25.12	25.52	75.98	117.51	17C1.17
3 MAIN	15.00	76.32	223.48	1835.24	6348.07	1.4500	72.75	40.15	97.09	28.39	24.05	75.65	126.11	19521.83
3 MAIN	16.00	81.40	254.27	1962.05	6915.36	1.4500	72.75	44.79	97.05	31.63	24.10	75.56	134.63	22305.21
3 MAIN	17.00	86.49	287.05	2084.01	7531.70	1.4500	72.75	49.34	97.02	34.83	24.09	75.66	142.15	25061.31
3 MAIN	18.00	91.58	321.22	2200.92	8200.23	1.4500	72.75	53.02	96.95	37.98	24.03	75.92	151.69	28090.16
3 MAIN	19.00	96.67	358.57	2312.28	8924.23	1.4500	72.75	58.15	96.95	41.04	22.92	76.35	160.25	31251.90
3 MAIN	20.00	101.76	397.30	2418.26	9707.07	1.4500	72.75	62.42	96.91	44.01	23.77	76.92	153.62	34566.17
3 MAIN	21.00	106.84	438.03	2518.70	10552.27	1.4500	72.75	66.50	96.85	46.86	23.57	77.04	177.40	35513.25
3 MAIN	22.00	111.93	480.74	2613.61	11463.42	1.4500	72.75	70.42	96.81	49.60	23.35	78.46	165.96	41537.10
3 MAIN	23.00	117.02	525.43	2703.09	12444.16	1.4500	72.75	74.16	96.76	52.21	23.10	79.35	194.50	455825.68
3 MAIN	24.00	122.11	572.12	2787.22	13498.28	1.4500	72.75	77.72	96.71	54.68	22.83	80.41	203.22	49850.99
3 MAIN	25.00	127.20	622.76	2866.18	14629.54	1.4500	72.75	81.10	96.66	57.03	22.53	81.54	211.85	54129.05
3 MAIN	26.00	132.28	671.44	2940.13	15841.82	1.4500	72.75	84.29	96.60	59.24	22.23	82.75	220.50	58539.85
3 MAIN	27.00	137.37	724.09	3009.28	17138.99	1.4500	72.75	87.30	96.55	61.32	21.91	84.04	229.16	63123.40
3 MAIN	28.00	143.68	811.51	3132.60	19211.71	1.4500	72.36	91.42	96.42	63.79	21.60	85.41	240.05	70732.75
3 MAIN	29.00	149.06	905.68	3168.44	21528.77	1.4500	71.97	95.22	96.25	65.95	21.25	86.97	251.10	78929.25
3 MAIN	30.00	155.51	1006.86	3266.55	24113.38	1.4500	71.58	98.72	97.94	2C.87	68.72	262.31	87734.25	
3 MAIN	31.00	163.03	1115.27	3337.52	26990.12	1.4500	71.19	101.92	96.00	69.55	2C.47	90.63	273.68	97169.25

LF = FUEL BELOW MINIMUM REQUIRED RATE

HF = FUEL ABOVE MAXIMUM FUEL RATE

HS = TURBINE SPEED EXCESSIVE

HFS = TURBINE FUEL AND SPEED EXCESSIVE

C C O

## ELECTRIC DRIVE SYSTEM

## MISSION PROFILE SUMMARY - FCUR MAIN TURBINES

KTS	PCT.	TIME	P/D RATIO	SHAFT RPM	SPEED RATIO	EFFECTIVE HP	SHAFT HP	TURBINE HP	FUEL RATE (PPH)	RANGE (NM/TON)	NAUT. MILES		TONS PER MILE	NO. OF TURBINES
											PER THOUSAND HOURS	TONS FUEL		
1	1.10	1.450	5.09	291.60	1.40	1.92	39.06	4400.	0.5C9	11.	22.02	2.002	4	MAIN
2	1.20	1.450	10.18	145.30	11.20	15.39	52.97	4400.	1.018	24.	24.02	1.001	4	MAIN
3	1.20	1.450	15.26	95.68	37.80	51.96	50.01	4400.	1.527	36.	24.02	3.667	4	MAIN
4	1.20	1.450	20.35	74.43	89.60	123.20	161.60	4400.	2.035	48.	24.02	2.002	4	MAIN
5	1.20	1.450	25.44	54.39	175.30	240.50	279.00	4400.	2.545	60.	24.02	2.402	4	MAIN
6	1.20	1.450	30.53	42.58	302.40	415.70	453.70	4400.	3.055	72.	24.02	0.334	4	MAIN
7	1.20	1.450	35.61	22.44	480.20	660.10	696.70	4400.	3.564	84.	24.02	0.256	4	MAIN
8	1.20	1.450	40.70	18.65	715.80	985.30	1016.00	4425.	4.055	96.	24.02	0.252	4	MAIN
9	1.20	1.450	45.79	19.37	1021.00	1403.00	1445.00	4759.	4.236	108.	25.94	0.240	4	MAIN
10	1.20	1.450	50.88	19.98	1400.00	1924.00	1982.00	5126.	4.370	120.	27.91	0.233	4	MAIN
11	6.30	1.450	55.97	20.49	1863.00	2561.00	2637.00	5328.	4.459	693.	157.80	0.228	4	MAIN
12	5.70	1.450	61.05	20.90	2179.00	3225.00	3243.00	5666.	4.505	804.	131.00	0.225	4	MAIN
13	7.30	1.450	66.14	21.24	3076.00	4226.00	4352.00	6444.	4.519	910.	204.20	0.224	4	MAIN
14	7.10	1.450	71.23	21.49	3842.00	5280.00	5437.00	6963.	4.504	994.	223.40	0.225	4	MAIN
15	6.80	1.450	76.32	21.68	4725.00	6495.00	6688.00	7526.	4.464	1020.	231.10	0.227	4	MAIN
16	6.10	1.450	81.40	21.81	5734.00	7882.00	8118.00	8135.	4.405	976.	223.90	0.229	4	MAIN
17	6.60	1.450	86.49	21.89	6878.00	9454.00	9746.00	6794.	4.330	1122.	261.70	0.233	4	MAIN
18	7.20	1.450	91.58	21.91	9165.00	11220.00	11570.00	9504.	4.242	1256.	308.30	0.233	4	MAIN
19	7.70	1.450	96.67	21.93	9603.00	13220.00	13610.00	10270.	4.144	1403.	356.10	0.243	4	MAIN
20	8.90	1.450	101.80	21.93	11200.00	15390.00	15880.00	11390.	4.028	1760.	444.40	0.250	4	MAIN
21	7.50	1.450	106.80	21.73	12570.00	17820.00	18380.00	11580.	3.927	1575.	404.20	0.257	4	MAIN
22	4.30	1.450	111.90	21.60	14910.00	20490.00	21150.00	12930.	3.811	946.	250.00	0.264	4	MAIN
23	1.50	1.450	117.00	21.44	17030.00	23410.00	24170.00	13950.	3.693	345.	94.05	0.273	4	MAIN
24	1.30	1.450	122.10	21.25	19350.00	26600.00	27480.00	15040.	3.574	312.	87.86	0.262	4	MAIN
25	0.70	1.450	127.20	21.05	21870.00	30070.00	31070.00	16210.	3.455	175.	50.96	0.261	4	MAIN
26	0.50	1.450	132.30	20.84	24610.00	33820.00	34970.00	17460.	3.336	130.	39.19	0.261	4	MAIN
27	0.40	1.450	137.40	20.60	27550.00	37880.00	39150.00	18790.	3.219	106.	23.73	0.212	4	MAIN
28	0.30	1.450	143.70	20.40	32130.00	44400.00	45570.00	20500.	3.001	84.	23.14	0.335	4	MAIN
29	0.30	1.450	20.16	150.10	37250.00	51750.00	53650.00	23260.	2.793	87.	31.31	0.360	4	MAIN
30	0.30	1.450	156.50	15.82	42950.00	60010.00	62260.00	25380.	2.596	90.	34.83	0.387	4	MAIN
31	0.30	1.450	163.00	19.57	49290.00	69240.00	71560.00	28790.	2.412	93.	36.73	0.416	4	MAIN
32	0.30	1.450	169.60	19.24	56300.00	79520.00	82760.00	32020.	2.239	96.	43.06	0.449	4	MAIN

## PERFORMANCE AVERAGES OVER MISSION PROFILE ( 1000 HOURS )

SPEED.....	15.76 KNOTS	AVERAGE ELECTRICAL LOAD
EFFECTIVE POWER.....	7423. HP	PROPELLION COOLING...
SHAFT POWER....	10230. HP	GENERATOR LUBE SYSTEM
TURBINE POWER...	10550. HP	HELIUM COMPRESSORS...
TURBINE FUEL...	88C9. LBS/HR	111. KW ( 88.4 LBS/HR )
PROPELLION FUEL	8997. LBS/HR	TOTAL LOAD.. 111. KW ( 88.4 LBS/HR )

## FOUR MAIN TURBINES

REF. NO. 501-6

TURBINE NUMBER	SPEED (RPM)	SHAFT (INCHES)	SHIFT TORQUE (TH.LR-FT)	TURBINE RPM	F/FU RATE	P/D RATE	PROP. EFF.	TURBINE DRIVE FOM	TOTAL SPEED RATIO	PERCENT FIELD VOLTAGE	BUS AMPS	MOTOR AMPS
4 MAIN	1,000	5.09	0.99	91.28	2977.57	1.4500	72.75	0.02	17.94	100.30	8.31	32.27
4 MAIN	2,000	10.18	3.57	182.72	3094.79	1.4500	72.75	0.21	91.33	0.14	17.96	16.64
4 MAIN	3,000	15.26	8.94	274.33	3240.03	1.4500	72.75	0.55	91.23	0.44	17.97	24.96
4 MAIN	4,000	20.35	15.39	366.10	3414.49	1.4500	72.75	1.44	95.39	1.00	17.99	100.30
4 MAIN	5,000	25.44	24.33	452.04	3513.05	1.4500	72.75	2.64	95.09	1.84	18.01	100.30
4 MAIN	6,000	30.53	35.76	550.14	3824.92	1.4500	72.75	4.26	95.53	2.02	18.02	100.30
4 MAIN	7,000	35.61	48.67	642.41	4123.23	1.4500	72.75	5.31	95.32	4.44	18.04	100.30
4 MAIN	8,000	40.70	63.57	759.05	4424.97	1.4500	72.75	8.76	95.97	6.13	18.65	6.89
4 MAIN	9,000	45.79	80.45	847.03	4758.72	1.4500	72.75	11.51	97.05	8.18	19.37	75.31
4 MAIN	10,000	50.88	98.33	1016.58	5125.73	1.4500	72.75	14.75	97.10	10.42	19.98	90.52
4 MAIN	11,000	55.97	120.18	1140.61	5527.58	1.4500	72.75	18.20	97.13	12.86	20.48	92.19
4 MAIN	12,000	61.05	143.03	1276.22	5968.48	1.4500	72.75	21.83	97.14	17.46	20.80	96.93
4 MAIN	13,000	66.14	167.86	1404.28	6444.25	1.4500	72.75	25.76	97.14	18.20	21.24	95.43
4 MAIN	14,000	71.23	194.68	1530.99	6963.32	1.4500	72.75	29.73	97.13	21.04	21.49	94.45
4 MAIN	15,000	76.32	223.48	1654.86	7526.13	1.4500	72.75	33.89	97.11	23.94	21.63	93.78
4 MAIN	16,000	81.40	254.27	1775.66	6135.34	1.4500	72.75	38.06	97.03	26.88	21.81	83.36
4 MAIN	17,000	86.49	287.05	1892.93	8793.72	1.4500	72.75	42.24	97.07	29.83	21.89	82.16
4 MAIN	18,000	91.58	321.82	2036.46	9504.23	1.4500	72.75	46.41	97.04	32.76	21.91	83.14
4 MAIN	19,000	96.67	355.57	2115.64	10259.91	1.4500	72.75	50.53	97.01	35.66	21.89	83.30
4 MAIN	20,000	101.76	397.30	2220.52	11093.96	1.4500	72.75	54.58	96.97	38.50	21.63	83.51
4 MAIN	21,000	106.84	438.03	2321.54	11979.65	1.4500	72.75	58.53	96.34	41.28	21.73	84.35
4 MAIN	22,000	111.93	480.74	2417.63	12930.45	1.4500	72.75	62.37	96.33	43.97	21.60	84.64
4 MAIN	23,000	117.02	525.43	2559.16	13494.79	1.4500	72.75	66.09	96.57	46.57	21.44	85.33
4 MAIN	24,000	122.11	572.17	2596.12	15041.30	1.4500	72.75	69.67	96.32	49.07	21.26	86.33
4 MAIN	25,000	127.19	620.76	2676.57	16208.59	1.4500	72.75	73.11	95.73	51.47	21.05	87.34
4 MAIN	26,000	132.26	671.44	2756.59	17455.42	1.4500	72.75	76.43	96.73	53.76	20.54	86.34
4 MAIN	27,000	137.37	724.29	2830.27	16785.59	1.4500	72.75	79.54	96.62	55.95	20.60	88.12
4 MAIN	28,000	143.46	811.51	2931.38	20903.07	1.4500	72.36	83.63	96.50	58.62	20.40	90.17
4 MAIN	29,000	150.06	925.65	3024.71	23261.31	1.4500	71.97	87.95	96.47	61.07	20.16	91.42
4 MAIN	30,000	156.51	1006.86	3111.26	25883.15	1.4500	71.58	91.73	96.33	63.30	19.83	92.86
4 MAIN	31,000	163.03	1115.27	3190.95	26792.72	1.4500	71.19	95.32	95.22	65.29	19.57	94.48
4 MAIN	32,000	169.62	1231.19	3264.05	32015.66	1.4500	70.80	98.59	96.09	67.07	19.24	96.25
4 MAIN	33,000	176.27	1354.65	3350.39	35578.89	1.4500	70.41	101.61	95.25	68.64	18.90	96.24

L = FUEL BELOW MINIMUM REQUIRED RATE  
 LF = FUEL ABOVE MAXIMUM FUEL RATE  
 HS = TURBINE SPEED EXCESSIVE  
 HFS = TURBINE FUEL AND SPEED EXCESSIVE

**FOUR MAIN TURBINES**

TURBINE CONFIG.	SPEED (KNOTS)	SHAFT RFY	SHIFT TRQ (TH.LB-FT)	TURBINE RPM	FUEL RATE	P/D RAT10	PRCP. EFF.	TURBINE FCN	DRIVE EFF.	TOTAL FIELD EFF.	PERCENT BUSS VOLTAGE	MOTOR AMPS
4 MAIN	1.00	5.CS	0.99	1463.51	4400.00	1.4500	72.75	0.34	4.93	0.01	291.58	92.27
4 MAIN	2.00	1C.16	3.97	1478.04	4400.00	1.4500	72.75	0.46	25.57	0.10	145.25	357.27
4 MAIN	3.00	15.26	8.94	1463.48	4400.00	1.4500	72.75	0.78	57.72	0.23	95.63	795.32
4 MAIN	4.00	20.35	15.85	1434.32	4400.00	1.4500	72.75	1.40	76.23	0.78	70.48	1405.51
4 MAIN	5.00	25.44	24.83	1383.69	4400.00	1.4500	72.75	2.42	86.21	1.52	54.39	2168.74
4 MAIN	6.00	30.53	35.76	1299.77	4400.00	1.4500	72.75	3.93	91.61	2.62	42.58	3144.71
4 MAIN	7.00	35.61	43.67	1155.21	4400.00	1.4500	72.75	6.44	94.73	4.16	32.44	58.43
4 MAIN	8.00	40.70	63.57	759.05	4424.97	1.4500	72.75	8.76	96.57	6.18	13.65	5574.83
4 MAIN	9.00	45.79	80.45	887.03	4758.72	1.4500	72.75	11.59	57.55	8.19	19.37	7049.97
4 MAIN	10.00	50.88	99.33	1015.58	5125.73	1.4500	72.75	14.75	57.10	10.42	15.98	8696.91
4 MAIN	11.00	55.97	120.18	1146.61	5527.68	1.4500	72.75	18.20	97.13	12.86	20.49	83.34
4 MAIN	12.00	61.05	143.03	1276.22	5966.48	1.4500	72.75	21.88	97.14	15.46	20.90	66.63
4 MAIN	13.00	66.14	167.86	1404.58	6444.46	1.4500	72.75	25.76	97.14	18.20	21.24	85.40
4 MAIN	14.00	71.23	154.68	1530.99	6953.32	1.4500	72.75	29.78	97.13	21.34	21.49	84.45
4 MAIN	15.00	76.32	223.32	1654.46	7526.13	1.4500	72.75	33.99	97.11	23.94	21.68	83.78
4 MAIN	16.00	81.40	254.27	1775.56	8135.34	1.4500	72.75	36.06	97.09	26.99	21.51	19521.83
4 MAIN	17.00	86.49	237.05	1692.98	8793.72	1.4500	72.75	42.24	97.07	29.63	21.89	100.65
4 MAIN	18.00	91.58	321.82	2005.46	9504.23	1.4500	72.75	46.41	97.04	32.76	21.91	14672.23
4 MAIN	19.00	96.67	352.57	2115.84	10269.91	1.4500	72.75	50.53	97.01	35.66	21.89	17C1.17
4 MAIN	20.00	101.76	397.30	2220.92	11093.96	1.4500	72.75	54.58	96.97	38.50	21.82	31291.80
4 MAIN	21.00	106.84	433.03	2321.54	11979.56	1.4500	72.75	58.53	96.94	41.28	21.72	34665.17
4 MAIN	22.00	111.92	483.74	2417.63	12930.45	1.4500	72.75	62.37	96.90	43.57	21.60	83.14
4 MAIN	23.00	117.02	525.43	2509.16	13349.79	1.4500	72.75	66.05	96.86	46.57	21.44	83.30
4 MAIN	24.00	122.11	572.12	2596.12	15041.30	1.4500	72.75	69.67	96.82	49.07	21.26	83.61
4 MAIN	25.00	127.19	620.79	2678.57	16208.59	1.4500	72.75	73.11	96.78	51.47	21.06	87.04
4 MAIN	26.00	132.28	671.44	2756.59	17455.42	1.4500	72.75	76.40	96.73	53.76	20.84	22.05
4 MAIN	27.00	137.37	724.09	2830.27	18785.59	1.4500	72.75	79.54	96.69	55.95	20.50	89.12
4 MAIN	28.00	142.68	811.51	2931.08	20503.02	1.4500	72.36	83.88	96.58	58.62	20.40	90.17
4 MAIN	29.00	150.36	905.68	3024.71	23261.31	1.4500	71.97	87.96	96.47	61.07	20.16	91.42
4 MAIN	30.00	156.51	1005.86	3111.26	25363.16	1.4500	71.58	91.78	96.35	62.30	15.38	54.129.05
4 MAIN	31.00	163.03	1115.27	3160.95	23792.72	1.4500	71.19	95.22	96.22	65.29	19.57	58.539.05
4 MAIN	32.00	169.62	1231.19	3264.05	32015.66	1.4500	70.80	96.59	96.09	67.07	19.24	97159.25
4 MAIN	33.00	176.27	1354.35	3330.89	355578.89	1.4500	70.41	101.61	95.95	68.64	18.90	118017.31

HF = FUEL BELOW MINIMUM REQUIRED RATE  
 LF = FUEL ABOVE MAXIMUM FUEL RATE  
 HS = TURBINE SPEED EXCESSIVE  
 HFS = TURBINE FUEL AND SPEED EXCESSIVE

**APPENDIX D**  
**DESCRIPTION OF ENGINE ROOM**  
**MODIFICATIONS**

*D-1*

Description of Engine Room Modifications

for Installation of High Efficiency

Propulsion Systems in Destroyer Type Hulls

Prepared for

Bradford Computer & Systems, Inc.

1700 Broadway

New York, New York 10019

Under Contract

N0014-74-C-0398

by

M. Rosenblatt & Sons, Inc.

350 Broadway

New York, New York 10013

BSDD-2870-05

D-16

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2. General
3. Modifications
  - 3.1 Addition of Cruise Turbines
  - 3.2 Addition of Crossover Alternators
  - 3.3 Substitution of Superconducting Electric Propulsion, Existing Engine Room Configuration
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- 3.2 Location of Cruise Turbine Modules
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- 4.1 Summary of Weight Changes, Addition of Cruise Turbine
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- 4.3 Summary of Weight Changes, Superconducting Electric Propulsion, Present Configuration
- 4.4 Summary of Weight Changes, Superconducting Electric Propulsion Reconfigured Engine Room

## LIST OF DRAWINGS

The following drawings, which are under separate cover, supplement this report.

MR&S DWG. NO.	TITLE
2870-01	Addition of 5000 HP Cruise Gas Turbine for DD's
2870-02	Addition of Crossover Alternator for DD's
2870-03	Superconducting Electric Propulsion for DD's, Existing Configuration
2870-04	Superconducting Electric Propulsion for DD's, Reconfigured Engine Room

## 1. Introduction

At the request of Bradford Computer and Systems, Inc. (15 July 1974, C-2870) M. Rosenblatt & Son, Inc. was to conduct a study, at a feasibility level, of modifying the propulsion system of a modern type destroyer in order to obtain a higher fuel efficiency during cruising and low speed operations.

Baseline information as to the system configuration for each modification was based on information furnished by Bradford. In those instances where information was not directly applicable to the propulsion systems under study, new definitions of equipment configuration were engineered or estimated. This work involved ascertaining equipment characteristics of possible candidate systems and investigating the feasibility of integrating each system into the configuration of a modern type destroyer.

In order to demonstrate the feasibility of adding new equipment to typical modern destroyer type ships, in conjunction with the study of the comparative performance of high efficiency ship propulsion systems, four arrangement drawings have been prepared. Each drawing shows the modifications to both forward and after engine rooms to accommodate the required equipment for each proposed propulsion system. The propulsion configuration of an existing destroyer type (DD263) was used as a baseline for the equipment arrangements in order to provide a real life basis for the study. The baseline propulsion system consists of four LM-2500 gas turbines (80,000 HP total), mechanically geared to two independent shafts (40,000 HP each) and is considered representative of modern destroyer type ships. The four possible modifications to this baseline system are summarized as follows:

- 1.1 Drawing No. 2870-01 shows the addition of two 5000 HP gas turbines, one to each engine room, to provide the capability for reduced power

cruising. Each new gas turbine is mechanically coupled to the existing main propulsion gear.

1.2 Drawing No.2870-02 shows the addition of a 10,000 HP alternator and its associated equipment to each engine room, to permit a single propulsion turbine to drive both shafts via an electrical crossover between port and starboard propulsion systems. During crossover operation, one alternator will be driven as a synchronous motor by the other alternator.

1.3 Drawing No.2870-03 shows the substitution of superconducting electric propulsion equipment for the existing mechanical reduction gearing, while retaining the existing machinery arrangement. This modification provides the main propulsion system with the capability of accepting connections to external 5000 HP cruise turbines and an electrical crossover connection, both of which provide for cruising at reduced power levels.

1.4 Drawing No.2870-04 shows the substitution of superconducting electric propulsion equipment for mechanical reduction gearing, as above, except that the existing machinery configuration has been optimized by elevating the propulsion gas turbines to reduce intake and exhaust ducting and by locating the propulsion motors aft to reduce shaft length.

## 2. General

All four engine room arrangement drawings show equipment currently under development. The arrangements shown are based on preliminary information and are, of course, subject to change as a result of future design developments and as additional information is made available. Engineering

judgement was often required in allowing for service access and interface requirements.

Of the four engine room arrangements outlined in the introduction, those showing the addition of high performance alternators and superconducting machinery have been based on data previously developed through prior propulsion studies primarily for a SWATH type ship, and additional information furnished by Bradford Computer and Systems, Inc.

Although there is a convenient similarity between the SWATH propulsion plant and that of the destroyer chosen as typical of modern destroyer types, (twin screw, 80,000 sub total), some modification of the SWATH propulsion plant was necessary for installation in the destroyer type hull. The SWATH was provided with a large single engine room containing both port and starboard propulsion plants. Many of the services for the superconducting machinery on both plants (i.e. helium, coolanol, etc.) had a common source.

Destroyers, on the other hand, are usually provided with two separate engine rooms, each intended to be as independent as is practical from the other. Thus, in the destroyer arrangement drawings, several of the SWATH systems have been modified to provide independent superconducting machinery support systems, such as helium and coolanol systems for each engine room, as shown in Figure 2-1. In addition, motor and generator bearing lube oil requirements have been provided from the existing main lube oil system, in lieu of providing each new machine with its own individual lube oil system, as was shown for the SWATH study.

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Subject

## FLUID SYSTEMS, EACH ENGINE ROOM

Ship or Project STUDY OF HIGH EFFICIENCY PROPULSION SYSTEMS FOR DD'S

Section

B-1010

Prepared by J. H. Shaeffer

Date 10/74 Checked \_\_\_\_\_

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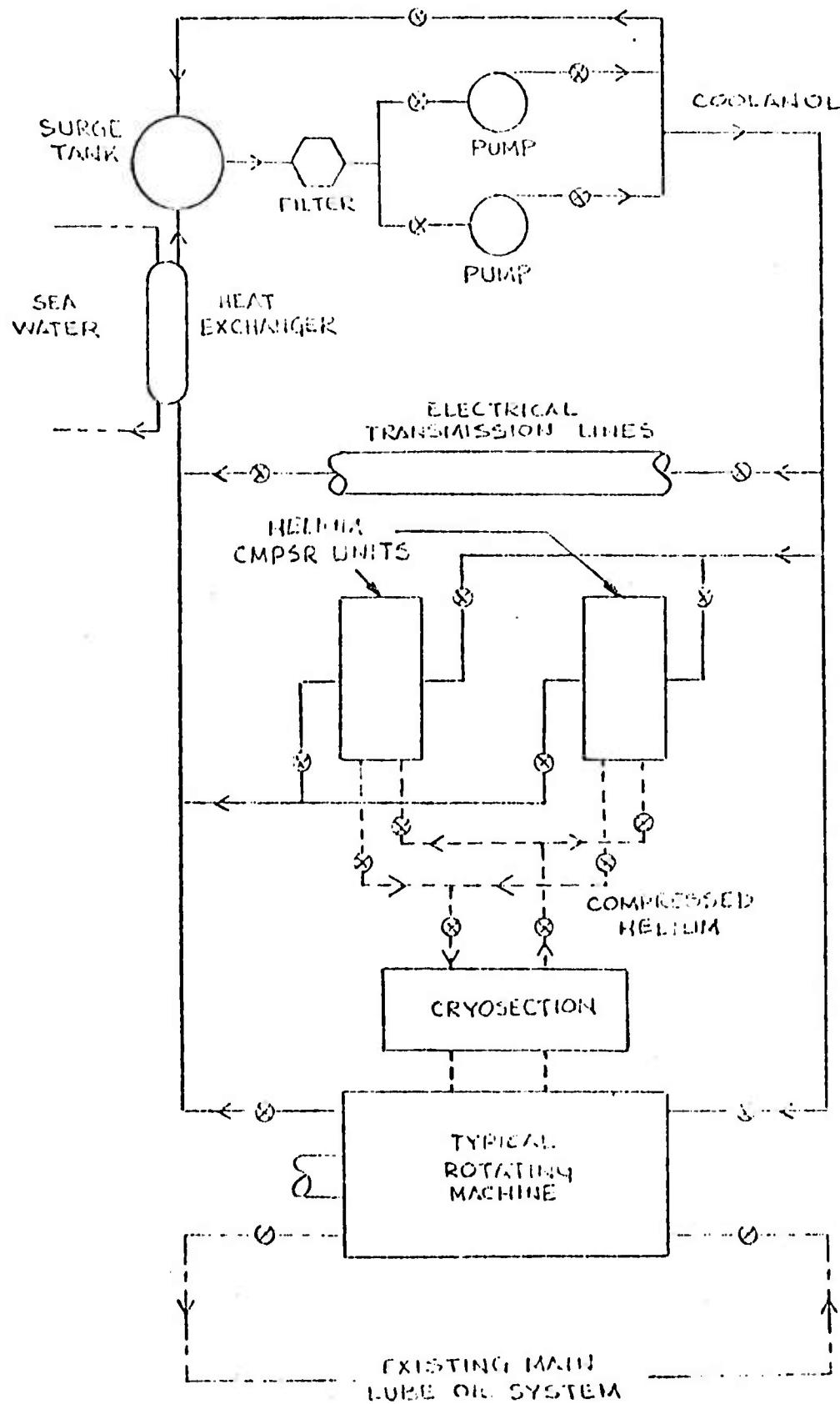


FIGURE 2-1 FLUID SYSTEMS SCHEMATIC  
DIAGRAM (EACH ENGINE ROOM)

### 3. Modifications

#### 3.1 Addition of Cruise Turbines (Drawing No. 2870-01)

The cruise turbine size shown was based on available information for modern marine gas turbines of approximately 5000 HP. The space shown will accommodate the Garrett GTPF990 engine, currently under development for the U.S. Navy. The cruise turbine output is mechanically coupled through angle gearing to the existing main reduction gear which must be modified to accept the cruise turbine input shaft.

Other modifications necessary to accept the cruise turbine, its gearing and its ductwork are as follows:

- a. The shaft turning gear was relocated to the opposite side of the reduction gear.
- b. The main lube oil cooler was relocated to the 7'-6" level, alongside the main reduction gear.
- c. Vertical ladders between the 24'-0" level and the 15'-0" level were relocated. In the forward engine room, this relocation placed the new vertical ladder close to the auxiliary boiler which normally would present a hazard to personnel. However, upgrading the boiler insulation in accordance with the recommendations of current Navy studies should eliminate any hazards due to heat from the boiler.
- d. The machinery platform at the 15'-0" level was extended to provide a turbine and gear service aisle.
- e. The auxiliary boiler exhaust duct was modified by the addition of a transition piece (from a circular to a

rectangular duct cross-section) to permit the new cruise turbine exhaust duct to be run under the existing boiler exhaust duct. In the aft engine room, the existing ship service generator intake duct was also re-routed to clear the new cruise turbine angle gearing.

- f. Several power panels, lighting panels, starting air flasks (forward engine room), and fire-fighting cylinders and hose reels were relocated to suit the new arrangements and ductwork.

### 3.2 Addition of Crossover Alternators (Drawing No. 2870-02)

The alternator size shown, and the service requirements for this alternator were estimated from existing machine data and from data on other alternator sizes supplied by Bradford Computer and Systems, Inc. The data used in preparing this arrangement is summarized in Table 3-1. Transmission line cooling was not considered necessary as it was assumed that the alternator would be arranged to operate at a higher voltage rating than the acyclic machines used in the SWATH study and that output currents could be transmitted via normally installed Navy 5KVTSAG cable.

The alternator is mounted alongside the existing reduction gear and mechanically coupled via a new transfer gear and a modification to the existing reduction gear. Few other modifications to the existing engine room arrangement are required to accommodate the new equipment. These modifications consist mainly of relocating a few minor items (air starting flasks, fire fighting hose reels and cylinders, etc.) and modifying existing gratings as shown on the drawing.

## DESIGN CALCULATION SHEET

Sheet 1 of 1

Subject 10,000 HP CROSSOVER ALTERNATOR

Ship or Project STUDY OF HIGH EFFICIENCY PROPULSION SYSTEMS FOR DD'S

Section BSDD Prepared by H. Springer Date 10/17/74 Checked

Reviewed

TABLE 3-1 SUMMARY OF CHARACTERISTICS  
FOR 10,000 HP ALTERNATORS

## 1. ALTERNATOR SIZE AND WEIGHT: (APPROX.)

O. D.	3.0 FT
LENGTH	6.0 FT
VOLUME	40. CU FT
WEIGHT	11,000 LBS
SPEED, AT FULL POWER	5,000 RPM

## 2. ESTIMATED LOSSES TO COOLANT: 149 KW

WITH COOLANT = SEA WATER TEMPERATURES AND  
PRESSURES AS SHOWN IN "SWATH" STUDY:

COOLANT FLOW = 63 GPM

SEA WATER FLOW = 66 GPM

COOLANT PUMP LOAD = 2 HP

HEAT EXCHANGER SIZE (APPROX) =

9" DIA X 100" LENGTH, 350 LBS.

### 3.3 Substitution of Superconducting Electric Propulsion, Existing Engine Room Configuration (Drawing No: 2870-03)

In this configuration a superconducting electric propulsion system similar to that planned for the SWATH is substituted for the existing main reduction gear in each engine room. One 20,000 HP propulsion generator is direct coupled to each propulsion gas turbine and one 40,000 HP propulsion motor is direct coupled to each propulsion shaft.

The controllable pitch propeller (CRP) is locked into a fixed position and the CRP hydraulic system is removed. Alternately, the CRP could be replaced by a fixed pitch propeller, however the change in efficiency is considered to be small. The difference in weight between the CRP and a fixed pitch propeller was not estimated.

The existing reduction gear lube oil system is retained to provide bearing lube oil to the new equipment. The existing gear driven lube oil pump is replaced by an additional motor driven lube oil pump. The existing main lube oil cooler is retained and relocated to the 7'-6" level to provide space for the new coolanol system. The existing thrust bearing is replaced by a new pedestal type thrust bearing at the after bulkhead in each engine room.

The new helium and coolanol systems are installed mostly on the 15'-0" level which has been extended into the space formerly occupied by the main reduction gear. A new uninterrupted power supply (UPS) power panel and automatic bus transfer switch (ABT) are also installed on the 15'-0" level. Generator disconnect and

crossover switches are located at the 24'-0" level except for the forward engine room, where the crossover switch is located at the 15'-0" level.

With the exception of the air starting flasks in the forward engine room, almost no other modifications are required to the existing engine room equipment.

The 5000 HP cruise turbine, if used, can be modularized as shown in Figure 3.1 and installed on top of the deck house adjacent to the machinery casing as shown in Figure 3.2. Electrical transmission lines and service piping will be run within the machinery casing between the cruise turbine module and the engine room with disconnect devices in the engine room in the event of damage to the module. Separate disconnect devices are also provided in each engine room to isolate the electrical cross-connect between engine rooms in the event of damage. It should be noted that the cruise turbine module can be easily installed within a standard 8'x8'x20' shipping container.

### **3.4 Substitution of Superconducting Electric Propulsion, Reconfigured Engine Room (Drawing No. 2870-04)**

This modification requires that the existing main reduction gear be replaced by superconducting electric propulsion, as does the previous modification. However, in this case an attempt is made to optimize the engine room arrangement by raising the main propulsion turbines and by relocating the main propulsion motors aft into the shaft alley area.

In this arrangement the propulsion gas turbines and the

## DESIGN CALCULATION SHEET

Subject

5000 HP CRUISE TURBINE MODULE

Ship or Project STUDY OF HIGH EFFICIENCY PROPULSION SYSTEMS FOR DD's

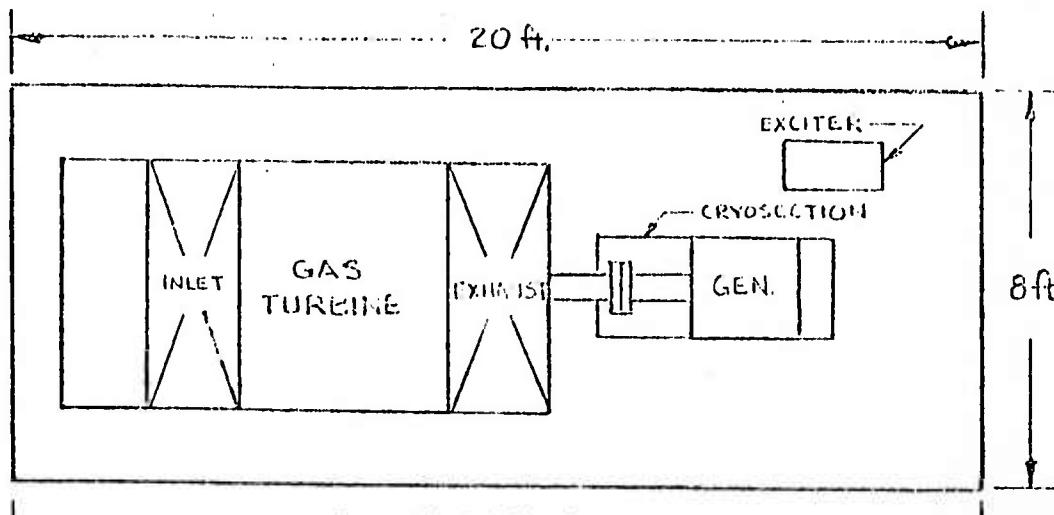
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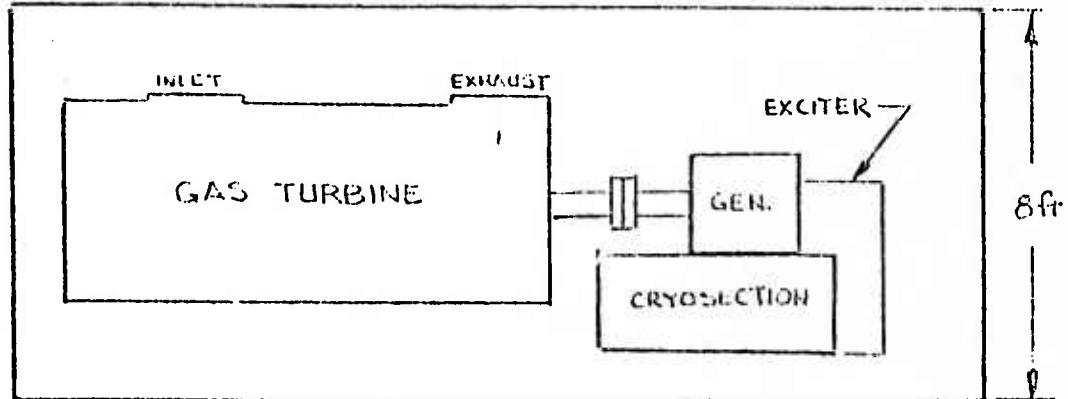
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PLAIN VIEW



ELEVATION

FIGURE 3-1

(10)

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## DESIGN CALCULATION SHEET

Subject LOCATION OF CRUISE TURBINE MODULES

Ship or Project STUDY OF HIGH-EFFICIENCY PROPULSION SYSTEMS FOR DD's

Section BSDP

Prepared by H. Rosenblatt

Date 10/74

Checked

Reviewed

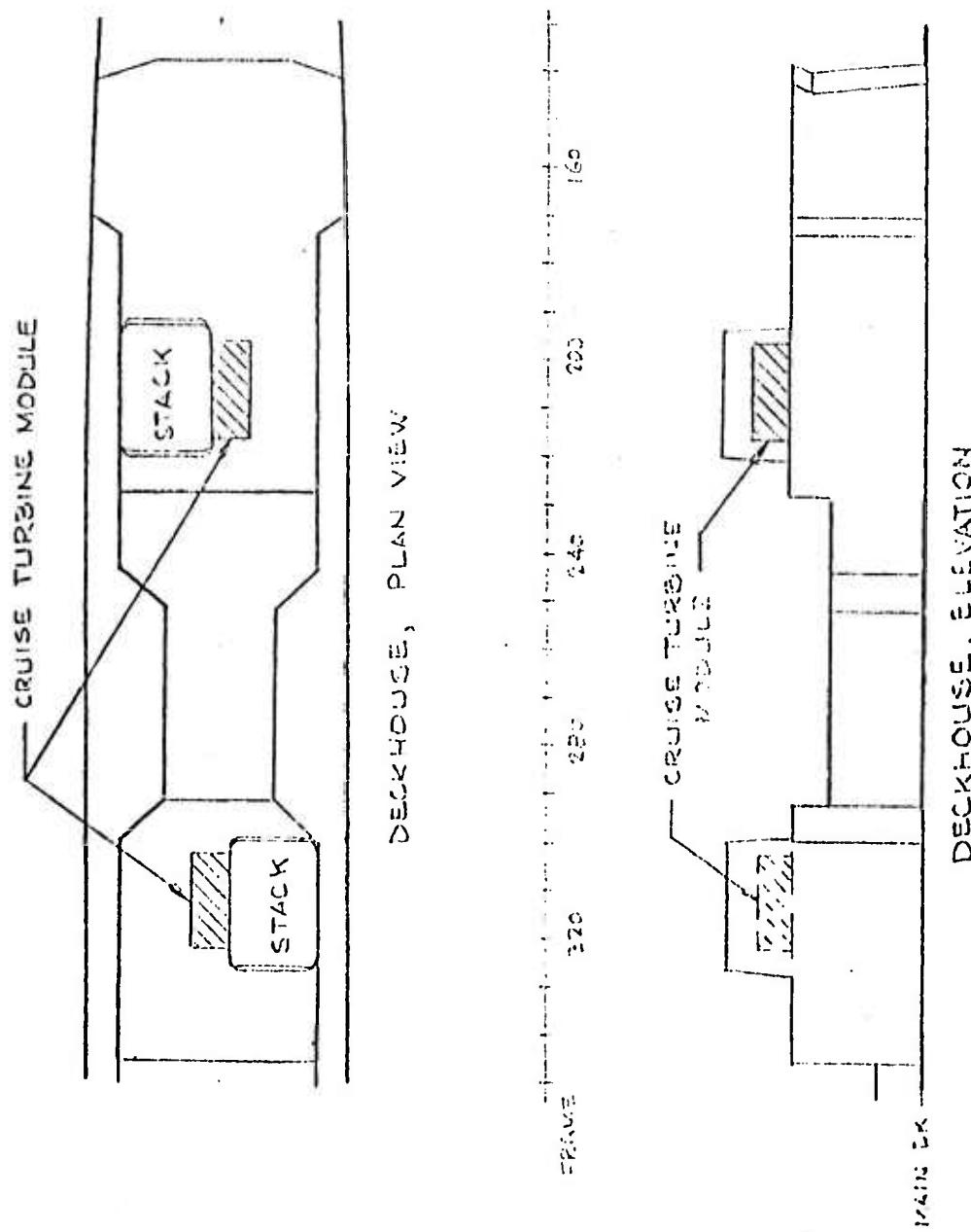


FIGURE 3-2

(11)

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20,000 HP propulsion generators are moved up onto the 24'-0" level.

In addition, the 24'-0" level is extended from the centerline to the shell to fill in the area formerly occupied by the gas turbine ductwork. The generator cryosections are located in the overhead of the 15'-0" level, directly under the propulsion generators.

The 15'-0" level is also extended from the centerline area to the shell. The helium and coolanol systems and the 20,000 HP generator disconnect switches are located on this level. The CRP system is locked in a fixed position as in the last arrangement (Section 3.3) and the existing attached lube oil pump is replaced by a new electrically driven lube oil pump. The main lube oil cooler is relocated to the 7'-6" level.

In this arrangement the existing lube oil storage and settling tanks are relocated from the 24'-0" level to the 15'0" level while the electronics cabinets on the 15'-0" level are moved to the 24'-0" level. This is to provide the inboard propulsion gas turbine on the 24'-0" level with a service access aisle. Several power panels, the fuel oil service heaters (aft engine room) and an air filter (forward engine room) were also relocated as part of this change.

With the 15'-0" level extended from the centerline area to the shell, there is no longer a need for two vertical access ladders and one of the ladders is eliminated in each engine room. It was necessary to relocate various fire fighting hose reels and cylinders, air starting cylinders (forward engine room) and vertical ladders from the 15'-0" level to the 7'6" level (forward engine room) and from the 15' -0" level to the 7' -6" level (forward engine room).

The location of the 5000 HP cruise turbines is as shown in Figure 3.2. Only one crossover switch is provided in the aft engine room, since both electric transmission lines must pass through this space.

The location of the propulsion motors is shown in Figure 3.3. The propulsion motors, in this location, appear to displace the shaft alley sewage treatment plant. However, the displaced equipment can be relocated to the space gained under the main propulsion turbines in one of the engine rooms. No attempt has been made at this time to optimize the shaft angles or relocate the shaft tubes. Additional studies are required into the serviceability of the propulsion motors in the location shown and into the possibility of providing a third set of helium-coolanol-tube oil service equipment in lieu of piping these services aft from the engine rooms.

#### 4. Estimate of Weight Changes

Tables 4-1, 4-2, 4-3 lists the equipment removed and added as a result of the modifications in Section 3 and the estimated weights for the various equipment. In many cases, weights and sizes shown have been estimated from available information on equipment, that is currently under development. Due to the preliminary nature of much of the available information, no attempt was made to estimate changes in structural weights or changes in various ship systems caused by these modifications.

**Subject**

## LOCATION OF PROPULSION MOTORS

**Ship or Project** STUDY OF HIGH EFFICIENCY PROPULSION SYSTEMS FOR DDGs

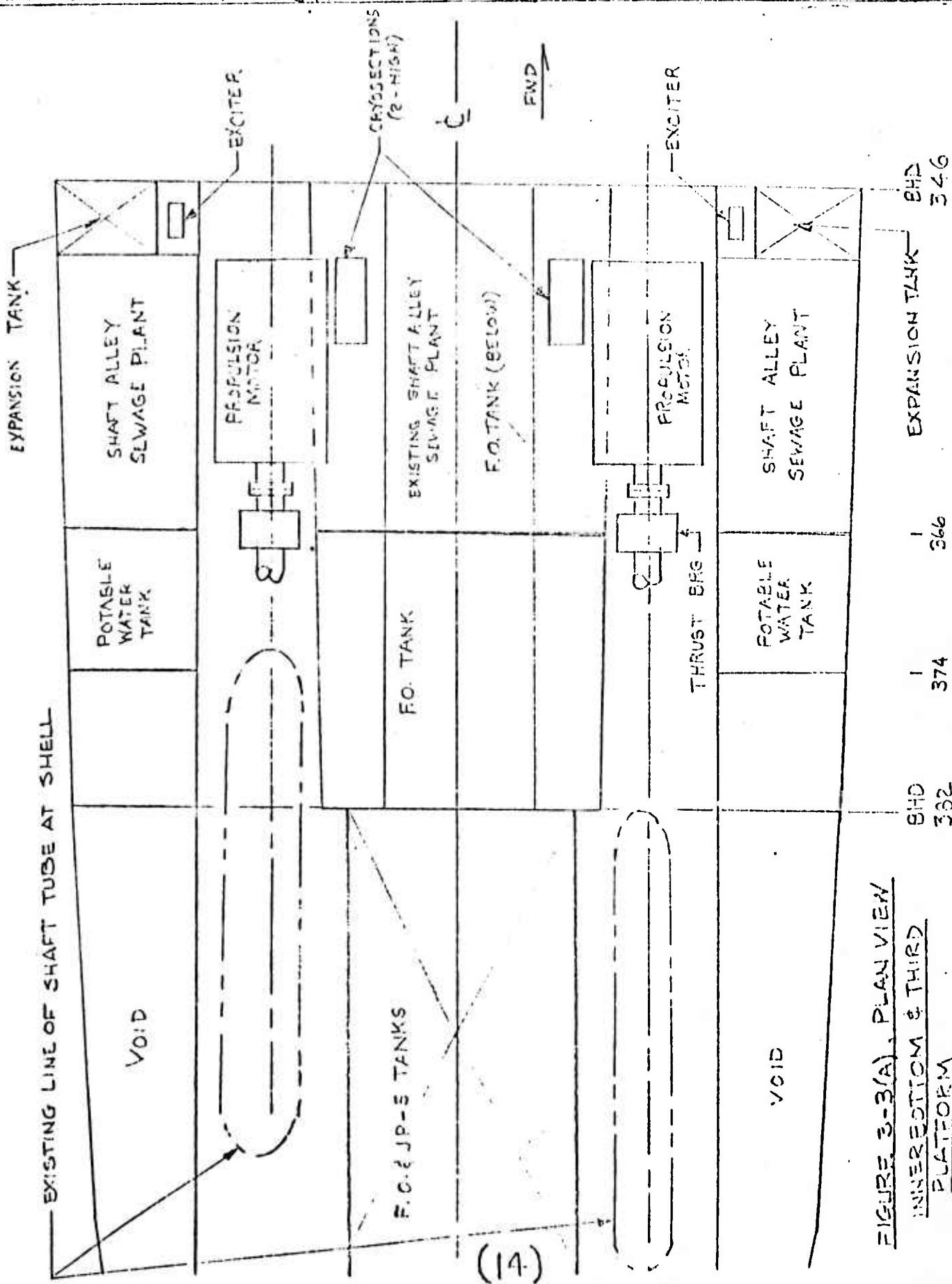
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Subject

LOCATION OF PROPULSION MOTORS

Ship or Project

STUDY OF HIGH EFFICIENCY PROPULSION SYSTEMS FOR DDG's

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Prepared by J.P.

Date 10/74

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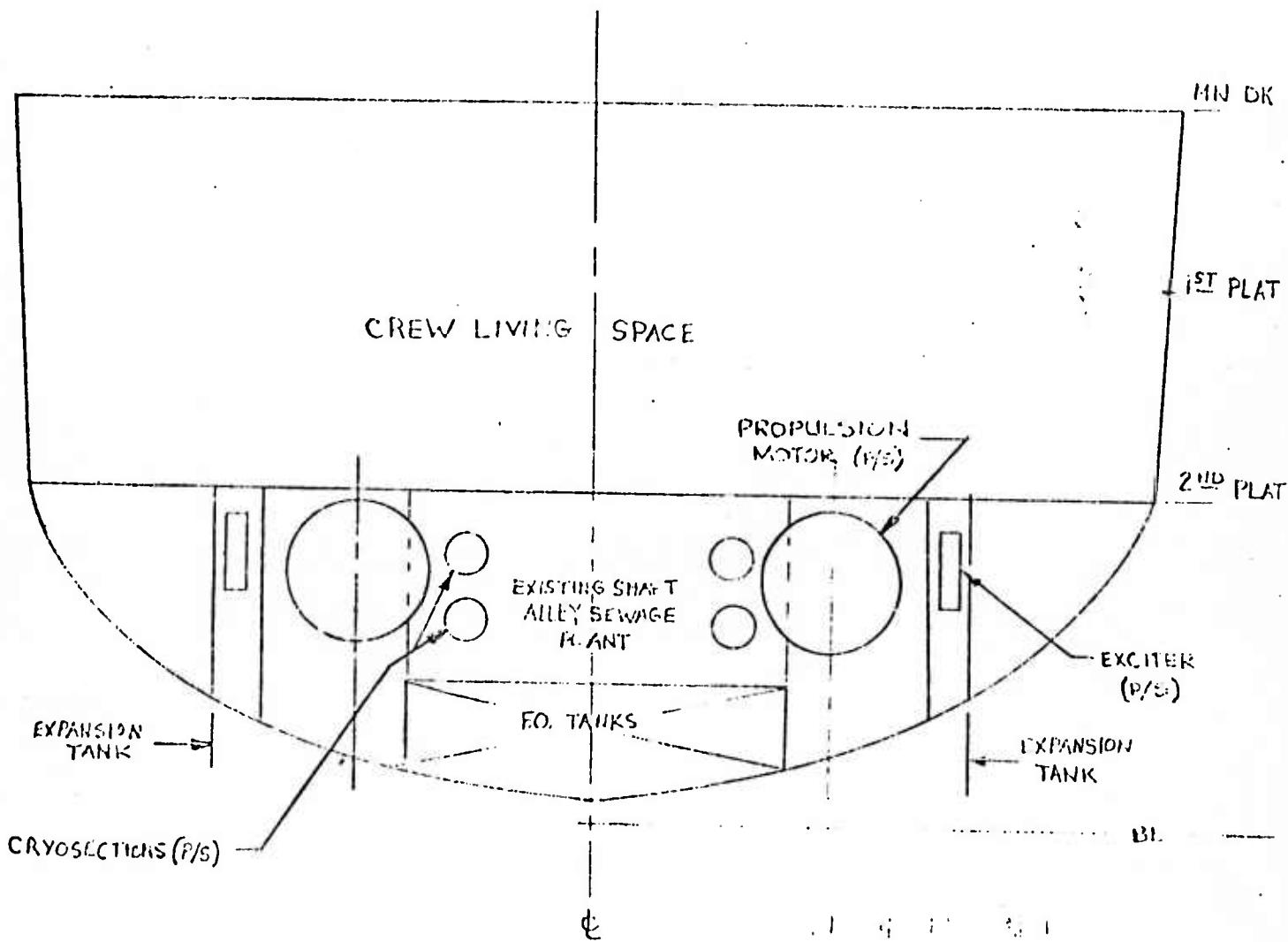


FIGURE 3-3 (B)  
ELEVATION, FR 346, LOOKING AFT

(15)

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TABLE 4 - 1

SUMMARY OF WEIGHT CHANGESADDITION OF CRUISE TURBINE

<u>LINE</u>		<u>QTY</u>	<u>UNIT WT (LBS)</u>	<u>UNIT SIZE</u>	<u>TOTAL WEIGHT</u>
1.	5,000 hp Gas Turbine	2	5,000	4'x5'x10'	10,000 lbs
2.	Transfer Gear & Clutch	2	6,000	4'x4'x4' 85'x5'x4.5'	12,000
TOTAL					22,000 lbs

NOTES

1. Above quantities include equipment for both forward and aft engine rooms.
2. There is no equipment removed as a result of this modification.
3. Additional omitted weights:
  - a. Modification to main reduction gear
  - b. Ductwork and new service piping and cables for new cruise turbine

TABLE 4 - 2

SUMMARY OF WEIGHT CHANGESADDITION OF CROSSOVER ALTERNATOR

<u>LINE</u>		<u>QTY</u>	<u>UNIT WT (LBS)</u>	<u>UNIT SIZE</u>	<u>TOTAL WEIGHT</u>
1.	10,000 hp Alternator	2	11,000	3' D x 6'	22,000 lbs
2.	Transfer Gear	2	12,000	8'x6'x3'	24,000
3.	Service Module	2	1,500		3,000
TOTAL					49,000 lbs

NOTES

1. Above quantities include equipment for both forward and aft engine rooms.
2. There is no equipment removed as a result of this modification.
3. Weight added as a result of modification to existing main reduction gear is omitted.

TABLE 4 - 3

SUMMARY OF WEIGHT CHANGESSUPERCONDUCTING ELECTRIC PROPULSION  
EXISTING ENGINE ROOM CONFIGURATION

LINE NOS.	ITEM	WEIGHT CHANGE IN LBS.
1 - 10	Fwd and Aft Engine Rooms - Weights Removed	(390,000)
11 - 37	Aft Engine Room - Weights Added	223,023
38 - 64	Fwd Engine Room - Weights Added	224,664
65	Crossover Between Engine Rooms - Weights Added	9,360
	TOTAL CHANGE IN WEIGHT	67,047

NOTES

1. Quantities for equipment removed includes equipment in both forward and aft engine rooms.
2. Weights for CRP hydraulic and Coolanol Systems considered to be even exchange except for new coolanol heat exchanges.
3. Additional study is required to confirm whether or not the high impedance element (25,000 lbs.) is required.

TABLE 4 - 3.1  
FWD & AFT ENGINE ROOM WEIGHTS REMOVED

SUPERCONDUCTING ELECTRIC PROPULSION  
-EXISTING ENGINE ROOM CONFIGURATION

<u>LINE</u>	<u>ITEM</u>	<u>QTY</u>	<u>UNIT WT (LBS)</u>	<u>UNIT SIZE</u>	<u>TOTAL WEIGHT (LBS)</u>
1.	Main Reduction Gear	2	170,000		340,000
2.	High Impedance Element (See Note 3)	2	35,000		50,000
3.	Attached Mn L.O. Pump		(Included in line 1)		
4.	" CRP Hyd Pump	"	" "	" "	
5.	" Oil Dist. Box	"	" "	" "	
6.	" Shaft Turn Gear	"	" "	" "	
7.	Control "Shaft Turn Gear		(Misc.)		
8.	CRP Head Tank		(See Note 2)		
9.	CRP Sump Tank	"	" "	" "	
10.	CRP Hydr. Module	"	" "	" "	
			TOTAL REMOVED		(390,000)

TABLE 4 - 3.1

## AFT ENGINE ROOM WEIGHTS ADDED

 SUPERCONDUCTING ELECTRIC PROPULSION  
 EXISTING ENGINE ROOM CONFIGURATION

<u>LINE</u>	<u>ITEM</u>	<u>QTY</u>	<u>UNIT WT (LBS)</u>	<u>UNIT SIZE</u>	<u>TOTAL WEIGHT (LBS)</u>
11.	Coolanol Pump (20hp)	2	(See Note 2)		
12.	Cont - Coolanol Pump	2	" " "		
13.	Coolanol Surge Tank	1	" " "		
14.	Coolanol Filter	1	" " "		
15.	Coolanol Heat Exchanger	1	4,000	1.5' Dx12'	4,000
16.	Thrust Bearing	1	12,70	3.8' Dx4'	12,000
17.	L.O. SVC Pump (50hp)	1	1,000		1,000
18.	Cont - L.O. SVC Pump (2 spd)	1	90		90
19.	Auto Bus Transfer SW	1	350	0.8'x2'x3'	350
20.	Power Panel	1	380	2'x1'x3.5'	380
21.	Uninterrupted Power Supply	1	1,275	2.7'x2'x3'	1,275
22.	Propulsion Motor (40 K hp)	1	136,500	6.5' Dx11.7'	136,500
23.	Propulsion Generators (70 K hp)	2	10,500	3.2' Dx4.2'	21,000
24.	Exciters	3	375	1'x2'x3.5'	1,125
25.	Gen. Polarity & Discon.	2	5,100	3.7'x4'x5.8'	10,200
26.	Transmission Lines:				
27.	Generator				2,027
28.	Motor				3,008
29.	Helium Compressors	2	3,250	2.6' Dx7.8'	6,500
30.	Cryosections	4	933	2.0' Dx5'	3,732
31.	Cryolines				<u>243</u>
			SUB-TOTAL		203,430
32.	Crossover Switch	1	1,300	2'x2.7'x3.8'	1,300
33.	Transmission Line				<u>1,584</u>
			SUB-TOTAL		2,884

TABLE 4 - 3.1  
AFT ENGINE ROOM WEIGHTS ADDED

SUPERCONDUCTING ELECTRIC PROPULSION  
EXISTING ENGINE ROOM CONFIGURATION

LINE	ITEM	QTY	UNIT WT (LBS)	UNIT SIZE	TOTAL WEIGHT (LBS)
34.	Cruise Turbine Module			8'x8'x20'	
a.	5,000 hp Gas Turbine	1	5,000		5,000
b.	5,000 hp Generator		3,850		3,850
c.	Cryosection	1	933		933
d.	Exciter	1	375		375
e.	Container Structure	1	3,500		3,500
35.	Transmission Line				1,813
36.	Cryoline				138
37.	Gen. Polarity & Disconnect Switch	1	1,100	2'x2.5'x3.5'	1,100
SUB-TOTAL					16,709
TOTAL, AFT ENGINE ROOM					223,023

TABLE 4 - 3.2  
FWD ENGINE ROOM WEIGHTS ADDED

SUPERCONDUCTING ELECTRIC PROPULSION  
-EXISTING ENGINE ROOM CONFIGURATION

LINE	ITEM	QTY	UNIT WT (LBS)	UNIT SIZE	TOTAL WEIGHT (LBS)
38.	Coolanol Pump (20hp)	2	(See Note 2)		
39.	Cont -Coolanol Pump	2	" " "		
40.	Coolanol Surge Tank	1	" " "		
41.	Coolanol Filter	1	" " "		
42.	Coolanol Heat Exchanger	1	4,000	1.5' Dx12'	4,000
43.	Thrust Bearing	1	12,000	3.8' Dx4'	12,000
44.	L.O. SVC Pump (50 hp)	1	1,000		1,000
45.	Cont -L.O. SVC Pump (2 spd)	1	90		90
46.	Auto Bus Transfer SW	1	350	0.8'x2'x3'	350
47.	Power Panel	1	380	2'x1'x3.5'	380
48.	Uninterrupted Power Supply	1	1,275	2.7'x2'x5'	1,275
49.	Propulsion Motor (40 K hp)	1	136,500	6.5' Dx11.7'	136,500
50.	Propulsion Generators (70 K hp)	2	10,500	3.2' Dx4.2'	21,000
51.	Exciters	3	375	1'x2'x3.5'	1,125
52.	Gen. Polarity & Discon.	2	5,100	3.7'x4'x5.8'	10,200
53.	Transmission Lines;				
54.	Generator				2,152
55.	Motor				3,008
56.	Helium Compressors	2	3,250	2.6' Dx7.8'	6,500
57.	Cryosections	4	933	2.0' Dx5'	3,732
58.	Cryolines				232
			SUB-TOTAL		203,444
59.	Crossover Switch	1	1,300	2'x2.7'x3.8'	1,300
60.	Transmission Line		SUB-TOTAL		360
					1,660

TABLE 4 - 3.2  
FWD ENGINE ROOM WEIGHTS ADDED

SUPERCONDUCTING ELECTRIC PROPULSION  
-EXISTING ENGINE ROOM CONFIGURATION

<u>LINE</u>	<u>ITEM</u>	<u>QTY</u>	<u>UNIT WT (LBS)</u>	<u>UNIT SIZE</u>	<u>TOTAL WEIGHT (LBS)</u>
61.	Cruise Turbine Module			8'x8'x20'	
a.	5,000 hp Gas Turbine	1	5,000		5,000
b.	5,000 hp Generator	1	3,850		3,850
c.	Cryosection	1	933		933
d.	Exciter	1	375		375
e.	Container Structure	1	3,500		3,500
62.	Transmission Line				4,018
63.	Cryoline				184
64.	Gen. Polarity & Disconnect Switch	1	1,100	2'x2.5'x3.5'	1,100
					—
			SUB-TOTAL		18,960
				TOTAL, FWD ENGINE ROOM	224,064

TABLE 4 - 3.3

SUPERCONDUCTING ELECTRIC PROPULSION  
-EXISTING ENGINE ROOM CONFIGURATION

<u>LINE</u>	<u>ITEM</u>	<u>QTY</u>	<u>UNIT WT (LBS)</u>	<u>UNIT SIZE</u>	<u>TOTAL WEIGHT (LBS)</u>
65.	Transmission Line				9,360
				TOTAL	9,360

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*D-26*

TABLE 4 - 4  
SUMMARY OF WEIGHT CHANGES

SUPERCONDUCTING ELECTRIC PROPULSION  
-RECONFIGURED ENGINE ROOM

<u>ITEM NOS.</u>	<u>LOCATION</u>	<u>WEIGHT CHANGE IN LBS.</u>
1 - 11	Fwd and Aft Engine Rooms - Weights Removed	(538,200)
12 - 39	Aft Engine Room - Weights Added	74,620
40 - 58	Fwd Engine Room - Weights Added	86,667
59 - 62	Propulsion Motor Space - Weights Added	301,482
	TOTAL CHANGE IN WEIGHT	(75,431)

NOTES

1. Quantities for equipment removed included equipment in both forward and aft engine rooms.
2. Weights for CRP hydraulic and Coolanol Systems considered to be even exchange except for new coolanol heat exchanges.
3. Additional study is required to confirm that high impedance element can be removed.

TABLE 4 - 4.1  
FWD & AFT ENGINE ROOM WEIGHTS REMOVED

<u>SUPERCONDUCTING ELECTRIC PROPULSION</u> <u>-RECONFIGURED ENGINE ROOM</u>					
<u>LINE</u>	<u>ITEM</u>	<u>QTY</u>	<u>UNIT WT (LBS)</u>	<u>UNIT SIZE</u>	<u>TOTAL WEIGHT (LBS)</u>
1.	Main Reduction Gear	2	170,000		340,000
2.	High Impedance Element (See Note 3)	2	25,000		50,000
3.	Attached Mn L.O. Pump		(Included in line 1)		
4.	CRP Hyd Pump	"	" " "		
5.	Oil Dist. Box	"	" " "		
6.	Shaft Turn Gear	"	" " "		
7.	Control Shaft Turn Gear		(Misc.)		
8.	CRP Head Tank		(See Note 2)		
9.	CRP Sump Tank	"	" " "		
10.	CRP Hydr. Module	"	" " "		
11.	Main Propulsion Shafting	650 lb/ft		228" x 18"	148,200
					538,200

TABLE 4 - 4.2  
AFT ENGINE ROOM WEIGHTS ADDED

SUPERCONDUCTING ELECTRIC PROPULSION  
-RECONFIGURED ENGINE ROOM

LINE	ITEM	QTY	UNIT WT (LBS)	UNIT SIZE	TOTAL WEIGHT (LBS)
12.	Coolanol Pump (30 hp)	2	(See Note 2)		
13.	Cont Coolanol Pump	2	(See Note 2)		
14.	Coolanol Surge Tank	1	(See Note 2)		
15.	Coolanol Filter	1	(See Note 2)		
16.	Coolanol Heat Exchanger	1	4,000	1.5' Dx12'	4,000
17.	(Not used)				
18.	L.O. SVC Pump (50 hp)	1	1,000		1,000
19.	Cont - L.O. SVC Pump (2SP0)	1	90		90
20.	Auto Bus Transfer SW	1	350	0.8'x2'x3'	350
21.	Power Panel	1	380	2'x1'x3.5'	380
22.	Uninterrupted Power Supply	1	1,275	2.7'x2'x5'	1,275
23.	(Not used)				
24.	Propulsion Generators (70K hp)	2	10,500	3.2' Dx4.2'	21,000
25.	Exciters	2	375	1'x2'x3.5'	375
26.	Gen. Polarity & Discon	2	5,100	3.7'x4'x5.8'	10,200
27.	Transmission Lines:				3,126
28.	Generator				1,892
29.	Motor				
30.	(Not used)				
31.	Helium Compressors	2	3,250	2.8' Cx7'	6,500
32.	Cryosections	2	933	2.0' Dx5'	1,866
33.	Cryolines				322
			SUBTOTAL		52,751

TABLE 4 - 4.2  
AFT ENGINE ROOM WEIGHTS ADDED

SUPERCONDUCTING ELECTRIC PROPULSION  
-RECONFIGURED ENGINE ROOM

LINE	ITEM	QTY	UNIT WT (LBS)	UNIT SIZE	TOTAL WEIGHT (LBS)
34.	Crossover Switch	1	1,300	2'x2.7'x3.8'	1,300
35.	Transmission Line				<u>3,034</u>
			SUBTOTAL		4,334
36.	Cruise Turbine Module			8.x8.x10'	
a.	5,000 hp Gas Turbine	1	5,000		5,000
b.	5,000 hp Generator	1	3,850		3,850
c.	Cryosection	1	933		933
d.	Exciter	1	375		375
e.	Container Structure	1	3,500		3,500
37.	Transmission Line				2,627
38.	Cryoline				150
39.	Gen. Polarity & Disconnect Switch	1	1,100	2'x2.5'x3.5'	1,100
			SUB-TOTAL		17,535
			TOTAL, AFT ENGINE ROOM		74,620

TABLE 4 - 4.3  
FWD ENGINE ROOM WEIGHTS ADDED

SUPERCONDUCTING ELECTRIC PROPULSION RECONFIGURED ENGINE ROOM					
LINE	ITEM	QTY	UNIT WT (LBS)	UNIT SIZE	TOTAL WEIGHT (LBS)
40.	Coolanol Pump (20 hp)	2	(See Note 2)		
41.	Cont - Coolanol Pump	2	" " "		
42.	Coolanol Surge Tank	1	" " "		
43.	Coolanol Filter	1	" " "		
44.	Coolanol Heat Exchanger	1	2,000	1.5' Dx12'	4,000
45.	L.O. SVC Pump (50 hp)	1	1,000		1,000
46.	Cont - L.O. SVC Pump (2 spd)	1	90		90
47.	Auto Bus Transfer SW	1	350	0.8'x2'x3'	350
48.	Power Panel	1	380	2'x1'x3.5'	380
49.	Uninterrupted Power Supply	1	1,275	2.7'x2'x5'	1,275
50.	Propulsion Generators (70 K hp)	2	10,500	3.2' Dx4.2'	21,000
51.	Exciters	2	375	1'x2'x3.5'	750
52.	Gen. Polarity & Discon. SW	2	5,100	3.7'x4'x5.8'	10,200
53.	Transmission Lines:				
54.	Generator				2,469
55.	Motor				16,104
56.	Helium Compressors	2	3,250	2.8' Dx5'	6,500
57.	Cryosections	2	933	2.0' Dx5'	1,866
58.	Cryolines				752
			SUB-TOTAL		66,736

TABLE 4 - 4.3

FWD ENGINE ROOM WEIGHTS ADDEDSUPERCONDUCTING ELECTRIC PROPULSION  
RECONFIGURED ENGINE ROOM

LINE	ITEM	QTY	UNIT WT (LBS)	UNIT SIZE	TOTAL WEIGHT (LBS)
59	Cruise Turbine Module			8x8x10'	
a.	5,000 hp Gas Turbine	1	5,000		5,000
b.	5,000 hp Generator	1	3,850		3,850
c.	Cryosection	1	933		933
d.	Exciter	1	375		375
e.	Container Structure	1	3,500		3,500
60.	Transmission Line				4,998
61.	Cryoline				175
62.	Gen. Polarity & Disconnect Switch	1	1,100	2'x2' 5'x3.5'	1,100
			SUB-TOTAL		19,931
			TOTAL, FWD ENGINE ROOM		86,667

TABLE 4 - 4.4

PROPULSION MOTOR SPACE WEIGHTS ADDED

LINE	ITEM	QTY	UNIT WT (LBS)	UNIT SIZE	TOTAL WEIGHT (LBS)
63.	Propulsion Motors	2	136,500	6.5' Dx11.7'	273,000
64.	Thrust Bearings	2	12,000	3.8' Dx4'	24,000
65.	Exciters	2	375	1'x2'x3.5'	750
66.	Cryosections	4	933	2' Dx5'	3,732
					301,482